

### DIO5833 Dual H-Bridge Motor Driver

### **Features**

- Dual H-Bridge Motor Driver With Current Control
  - 1 or 2 DC Motors or 1 Stepper Motor
  - Low On-Resistance: HS + LS = 850mΩ (Typical, 25°C)
- Output Current Capability (at V<sub>M</sub>=5V, 25°C)
  - PWP (HTSSOP) Package
    - 0.7A RMS, 1A Peak per H-Bridge
    - 1.4A RMS in Parallel Mode
  - RTE (QFN) Package
    - 0.6A RMS, 1A Peak per H-Bridge
    - 1.2A RMS in Parallel Mode
- Wide Power Supply Voltage Range
  - 2.7 to 15V
- Integrated Current Regulation
- Easy Pulse-Width-Modulation (PWM) Interface
- 1.6µA Low-Current Sleep Mode (at 5V)
- Small Package and Footprint
  - EP-TSSOP16
  - QFN 3\*3-16
- Protection Features
  - VM Undervoltage Lockout (UVLO)
  - Overcurrent Protection (OCP)
  - Thermal Shutdown (TSD)
  - Fault Indication Pin (nFAULT)

### Descriptions

The DIO5833 provides a dual-bridge motor driver solution for toys, printers, and other mechatronic applications.

The device has two H-bridges and can drive two DC brushed motors, a bipolar stepper motor, solenoids, or other inductive loads.

Each H-bridge output consists of a pair of N-channel and P-channel MOSFETs, with circuitry that regulates the winding current. With proper PCB design, each H-bridge of the DIO5833 can drive up to 700mA RMS (or DC) continuously, at 25°C with a  $V_M$  supply of 5V. The device can support peak currents of up to 1A per bridge. Current capability is reduced slightly at lower  $V_M$  voltages.

Internal shutdown functions with a fault output pi are provided for overcurrent protection, short-circuit protection, UVLO, and overtemperature. A low-power sleep mode is also provided.

### **Applications**

- Point-of –Sale Printers
- Video Security Cameras
- Office Automation Machines
- Gaming Machines
- Robotics
- Battery-Powered Toys

Order Part Number	Top Marking		T <sub>A</sub>	Package	
DIO5833XT16	DIO5833	Green	-40 to +85°C	EP-TSSOP16	Tape & Reel, 2500
DIO5833CL16	D5833	Green	-40 to +85°C	QFN3*3-16	Tape & Reel, 5000

### **Ordering Information**





www.dioo.com



### **Absolute Maximum Ratings**

Stresses beyond those listed under "Absolute Maximum Rating" may cause permanent damage to the device. These are stress ratings only and functional operation of the device at these or any other condition beyond those indicated in the operational sections of the specifications is not implied. Exposure to absolute maxim rating conditions for extended periods may affect device reliability.

Para	Rating	Unit	
Power supply (V <sub>M</sub> )		-0.3 to 16	V
Internal regulator (VINT)		-0.3 to 5.5	V
Control pins (AIN1, AIN2, BIN1, BIN2	2, nSLEEP, nFAULT)	-0.3 to 7	V
Voltage Continuous phase node pins	(AOUT1, AOUT2, BOUT1, BOUT2)	-0.3 to V <sub>M</sub> +0.5	V
Pulsed 10 µs phase node pins (AOU	-1 to V <sub>M</sub> +1	V	
Continuous shunt amplifier input pins (AISEN, BISEN)		-0.3 to 0.5	V
Pulsed 10 µs shunt amplifier input pins (AISEN, BISEN)		-1 to 1	V
Operating junction temperature (T <sub>J</sub> )		-40 to 150	°C
Storage temperature range $(T_{stg})$		-65 to 150	°C
Package Thermal Resistance	Θ <sub>JA</sub>	40.5	°C 10/
(EP-TSSOP16)	θ <sub>JC</sub>	32.9	C/W
Package Thermal Resistance	Θ <sub>JA</sub>	44.7	°CAN
(QFN-16)	θ <sub>JC</sub>	48.5	C/W
ESD	НВМ	±2000	V
	CDM	±1000	

## **Recommend Operating Conditions**

The Recommended Operating Conditions table defines the conditions for actual device operation. Recommended Operating conditions are specified to ensure optimal performance to the datasheet specifications. DIOO does not Recommend exceeding them or designing to Absolute Maximum Ratings.

Para	Rating	Unit	
Power supply voltage range		2.7 to 15	V
Logic level input voltage		0 to 5.5	V
Motor DMS ourrent	PWP package	0 to 0.7	А
	RTE package	0 to 0.6	А
Applied PWM signal to AIN1, AIN2, BIN1, or BIN2		0 to 200	kHz
Operating ambient temperature		-40 to 85	°C



### **Electrical Characteristics**

 $T_A$  = 25°C, unless otherwise specified.

Symbol	Parameter		Test Conditions	Min	Тур	Мах	Unit
POWER SU	JPPLIES (V <sub>M</sub> , V <sub>INT</sub> )						
V <sub>M</sub>	$V_M$ operating voltage			2.7		15	V
I <sub>VM</sub>	$V_M$ operating supply current		$V_M$ =5V, xINx low, nSLEEP high		1.7	3	mA
I <sub>VMQ</sub>	VMQ V <sub>M</sub> sleep mode supply current		$V_M$ =5V, nSLEEP low		1.6	4	μA
t <sub>SLEEP</sub>	Sleep time		nSLEEP low to sleep mode		10		μs
t <sub>WAKE</sub>	Wake-up time		nSLEEP high to output transition		110		μs
t <sub>ON</sub>	Turn-on time		$V_M > V_{UVLO}$ to output transition		100		μs
VINT	Internal regulator voltage		V <sub>M</sub> =5V	4	4.5	5	V
CONTROL	INPUTS (AIN1, AIN2, BIN1, BIN2, r	nSL	EEP)				
N			xINx	0		0.7	V
VIL			nSLEEP	0		0.5	V
N	V <sub>IH</sub> Input logic high voltage		xINx	2		5.5	N
VIH			nSLEEP	2.5		5.5	v
VHYS	Input logic hysteresis			350	400	650	mV
IIL	Input logic low current		$V_{IN} = 0 V$	-1		1	μA
ШН	Input logic high current		V <sub>IN</sub> = 5 V			50	μA
P			xINx	100	150	250	kO
RPD	Pulidown resistance		nSLEEP	380	500	750	K12
t <sub>DEG</sub>	Input deglitch time	2			575		ns
t <sub>PROP</sub>	Propagation delay INx to OUTx		V <sub>M</sub> = 5 V		1.2		μs
CONTROL	OUTPUTS (nFAULT)						
V <sub>OL</sub>	Output logic low voltage		l <sub>o</sub> = 5 mA			0.5	V
I <sub>OH</sub>	Output logic high leakage		$R_{PULLUP} = 1 k\Omega$ to 5 V	-1		1	μA
MOTOR DF	MOTOR DRIVER OUTPUTS (AOUT1, AOUT2, BOUT1, BOUT2)						
			V <sub>M</sub> = 5 V, I = 0.2 A, T <sub>A</sub> = 25°C		500		
Б	High oldo EET on registeres		V <sub>M</sub> = 5 V, I = 0.2 A, T <sub>A</sub> = 85°C		600	1475	
RDS(ON)	TIGH-SIDE FET ON-TESISIANCE		$V_{M} = 2.7 V, I = 0.2 A, T_{A} = 25^{\circ}C$		700		11122
			V <sub>M</sub> = 2.7 V, I = 0.2 A, T <sub>A</sub> = 85°C		800	1975	



		V <sub>M</sub> = 5 V, I = 0.2 A, T <sub>A</sub> = 25°C		350		
B		V <sub>M</sub> = 5 V, I = 0.2 A, T <sub>A</sub> = 85°C		400	705	
RDS(ON)	Low-side FET on-resistance	V <sub>M</sub> = 2.7 V, I = 0.2 A, T <sub>A</sub> = 25°C		450		11175
		V <sub>M</sub> = 2.7 V, I = 0.2 A, T <sub>A</sub> = 85°C		500	815	
I <sub>OFF</sub>	Off-state leakage current	V <sub>M</sub> = 5 V	-1		1	μA
t <sub>RISE</sub>	Output rise time	$V_{M}$ = 5 V; $R_{L}$ = 16 $\Omega$ to GND		70		ns
t <sub>FALL</sub>	Output fall time	$V_{M}$ = 5 V; $R_{L}$ = 16 $\Omega$ to $V_{M}$		80		ns
t <sub>DEAD</sub>	Output dead time	Internal dead time		450		ns
	RENT CONTROL (AISEN, BISEN)					
V <sub>TRIP</sub>	xISEN trip voltage		160	200	240	mV
t <sub>OFF</sub>	Current control constant off time	Internal PWM constant off time		20		μs
PROTECTI	ON CIRCUITS					
Manag		V <sub>M</sub> falling; UVLO report			2.6	V
VUVLO	V <sub>M</sub> undervoltage lockout	V <sub>M</sub> rising; UVLO recovery			2.7	v
V <sub>UVLO,HYS</sub>	$V_{\mbox{\scriptsize M}}$ undervoltage hysteresis	Rising to falling threshold		90		mV
I <sub>OCP</sub>	Overcurrent protection trip level		1			А
t <sub>DEG</sub>	Overcurrent deglitch time			2.3		μs
t <sub>OCP</sub>	Overcurrent protection period			1.4		ms
T <sub>TSD</sub>	Thermal shutdown temperature	Die temperature, T <sub>J</sub>	150			°C
T <sub>HYS</sub>	Thermal shutdown hysteresis	Die temperature, T <sub>J</sub>		20		°C

Specifications subject to change without notice.

**Dual H-Bridge Motor Driver** 



### Overview

The DIO5833 device is an integrated motor driver solution for brushed DC or bipolar stepper motors. The device integrates two PMOS + NMOS H-bridges and current regulation circuitry. The DIO5833 can be powered with a supply voltage from 2.7 to 15V and can provide an output current up to 700mA RMS.

A simple PWM interface allows easy interfacing to the controller circuit.

The current regulation is a 20-µs fixed off-time slow decay.

The device includes a low-power sleep mode, which lets the system save power when not driving the motor.

## **Functional Block Diagram**





### **Feature Description**

### **PWM Motor Drivers**

The DIO5833 contains drivers for two full H-bridges. Figure 3 shows a block diagram of the circuitry.



### Figure 3 H-Bridge and Current-Chopping Circuitry

### Bridge Control and Decay Modes

The AIN1 and AIN2 input pins control the state of the AOUT1 and AOUT2 outputs; similarly, the BIN1 and BIN2 input pins control the state of the BOUT1 and BOUT2 outputs (see Table 1).

xIN1	xIN2	xOUT1	xOUT2	FUNCTION
0	0	Z	Z	Coast/fast decay
0	1	L	Н	Reverse
1	0	Н	L	Forward
1	1	L	L	Brake/slow decay

#### Table 1 H-Bridge Logic

The inputs can also be used for PWM control of the motor speed. When controlling a winding with PWM and the drive current is interrupted, the inductive nature of the motor requires that the current must continue to flow (called recirculation current). To handle this recirculation current, the H-bridge can operate in two different states, fast decay or slow decay. In fast-decay mode, the H-bridge is disabled and recirculation current flows through the body diodes. In slow-decay mode, the motor winding is shorted by enabling both low-side FETs.

To externally pulse-width modulate the bridge in fast-decay mode, the PWM signal is applied to one xIN pin while the other is held low; to use slow-decay mode, one xIN pin is held high. See Table 2 for more information.



### Table 2 PWM Control of Motor Speed

xIN1	xIN2	FUNCTION
0	0	Forward PWM, fast decay
0	1	Forward PWM, slow decay
1	0	Reverse PWM, fast decay
1	1	Reverse PWM, slow decay

The internal current control is still enabled when applying external PWM to xIN. To disable the current control when applying external PWM, the xISEN pins should be connected directly to ground. Figure 4 show the current paths in different drive and decay modes.





### **Current Control**

The current through the motor windings may be limited, or controlled, by a 20µs constant off-time PWM current regulation, or current chopping. For DC motors, current control is used to limit the start-up and stall current of the motor. For stepper motors, current control is often used at all times.

When an H-bridge is enabled, current rises through the winding at a rate dependent on the DC voltage and inductance of the winding. If the current reaches the current chopping threshold, the bridge disables the current until the beginning of the next PWM cycle. Note that immediately after the output is enabled, the voltage on the xISEN pin is ignored for a fixed period of time before enabling the current sense circuitry. This blanking time is fixed at 3.75 µs.

The PWM chopping current is set by a comparator that compares the voltage across a current sense resistor connected to the xISEN pins with a reference voltage. The reference voltage,  $V_{TRIP}$ , is is fixed at 200 mV nominally.

The chopping current is calculated as in Equation 1.

$$I_{CHOP} = \frac{200mV}{R_{XISEN}}$$

(1)

Example: IF a 1 $\Omega$  sense resistor is used, the chopping current will be 200mV/1 $\Omega$ =200mA.



### **Delay Mode**

After the chopping current threshold is reached, the H-bridge switches to slow-decay mode. This state is held for  $t_{off}$  (20 µs) until the next cycle to turn on the high-side MOSFETs.

### Slow Decay

In slow-decay mode, the high-side MOSFETs are turned off and both of the low-side MOSFETs are turned on. The motor current decreases while flowing in the two low-side MOSFETs until reaching its fixed off time (typically 20 µs). After that, the high-side MOSFETs are enabled to increase the winding current again.





### Sleep Mode

Driving nSLEEP low puts the device into a low-power sleep state. In this state, the H-bridges are disabled, all internal logic is reset, and all internal clocks are stopped. All inputs are ignored until nSLEEP returns inactive high. When returning from sleep mode, some time,  $t_{WAKE}$ , needs to pass before the motor driver becomes fully operational. To make the board design simple, the nSLEEP can be pulled up to the supply (V<sub>M</sub>). TI recommends to use a pullup resistor when this is done. This resistor limits the current to the input in case V<sub>M</sub> is higher than 6.5V. Internally, the nSLEEP pin has a 500k $\Omega$  resistor to GND. It also has a clamping Zener diode that clamps the voltage at the pin at 6.5V. Currents greater than 250µA can cause damage to the input structure. Therefore, TI recommends a pullup resistor between 20 to 75k $\Omega$ .

#### Parallel Mode

The two H-bridges in the DIO5833 can be connected in parallel for double the current of a single H-bridge. The internal dead time in the DIO5833 prevents any risk of cross-conduction (shoot-through) between the two bridges due to timing differences between the two bridges. Figure 6 shows the connections.





Figure 6 Parallel Mode Schematic

### **Protection Circuits**

The DIO5833 is fully protected against overcurrent, overtemperature, and undervoltage events.

### **Overcurrent Protection (OCP)**

An analog current limit ( $I_{OCP}$ ) circuit on each FET limits the current through the FET by limiting the gate drive. If this analog current limit persists for longer than the OCP deglitch time ( $t_{DEG}$ ), all FETs in the H-bridge are disabled and the nFAULT pin is driven low. The driver is re-enabled after the OCP retry period ( $t_{OCP}$ ) has passed. nFAULT becomes high again after the retry time. If the fault condition is still present, the cycle repeats. If the fault is no longer present, normal operation resumes and nFAULT remains deasserted. Note that only the Hbridge in which the OCP is detected will be disabled while the other bridge functions normally.

Overcurrent conditions are detected independently on both high-side and low-side devices; a short to ground, supply, or across the motor winding all result in an overcurrent shutdown. Note that overcurrent protection does not use the current sense circuitry used for PWM current control, so it functions even without presence of the xISEN resistors.

### Thermal Shutdown (TSD)

If the die temperature exceeds safe limits, all FETs in the H-bridge are disabled and the nFAULT pin is driven low. After the die temperature has fallen below the specified hysteresis (T<sub>HYS</sub>), operation automatically resumes. The nFAULT pin is released after operation has resumed.

### UVLO

If at any time the voltage on the VM pin falls below the UVLO threshold voltage,  $V_{UVLO}$ , all circuitry in the device is disabled, and all internal logic is reset. Operation resumes when  $V_M$  rises above the UVLO threshold. The nFAULT pin is not driven low during an undervoltage condition.



### **Table 3 Device Protection**

Fault	Condition	Error Report	H-Bridge	Internal Circuits	Recovery
$V_M$ undervoltage (UVLO)	V <sub>M</sub> <2.6V	None	Disabled	Disabled	V <sub>M</sub> >2.7V
Overcurrent (OCP)	I <sub>OUT</sub> >I <sub>OCP</sub>	FAULTn	Disabled	Operating	OCP
Thermal Shutdown (TSD)	T <sub>J</sub> >T <sub>TSD</sub>	FAULTn	Disabled	Operating	$T_J < T_{TSD} - T_{HYS}$

### **Device Functional Modes**

The DIO5833 is active unless the nSLEEP pin is brought logic low. In sleep mode, the H-bridge FETs are disabled (Hi-Z). Note that  $t_{SLEEP}$  must elapse after a falling edge on the nSLEEP pin before the device is in sleep mode. The DIO5833 is brought out of sleep mode automatically if nSLEEP is brought logic high. Note that  $t_{WAKE}$  must elapse before the outputs change state after wake-up.

### Table 4 Modes of Operation

Fault	Condition	H-Bridge	Internal Circuits
Operating	nSLEEP pin high	Operating	Operating
Sleep mode	nSLEEP pin low	Disabled	Disabled
Fault encountered	Any fault condition met	Disabled	See Table 3

### Application and Implementation

#### **Application Information**

The DIO5833 is used in stepper or brushed DC motor control. The following design procedure can be used to configure the DIO5833 in a bipolar stepper motor application.

### **Typical Application**





### **Design Requirements**

Table 5 gives design input parameters for system design.

Design Parameter	Reference	Example Value
Supply voltage	V <sub>M</sub>	9V
Motor winding resistance	RL	12Ω/phase
Motor winding inductance	L	10mH/phase
Motor full step angle	Θ <sub>step</sub>	1.8°/step
Target stepping level	n <sub>m</sub>	2 (half-stepping)
Target motor speed	V	120rpm
Target chopping current	Існор	200mA
Sense resistor	RISEN	1Ω

### **Table 5 Design Parameters**

#### **Detailed Design Procedure**

#### **Stepper Motor Speed**

The first step in configuring the DIO5833 requires the desired motor speed and stepping level. The DIO5833 can support full- and half-stepping modes using the PWM interface.

If the target motor speed is too high, the motor does not spin. Ensure that the motor can support the target speed.

For a desired motor speed (v), microstepping level ( $n_m$ ), and motor full step angle ( $\theta_{step}$ ),









### Figure 8 Half-Step Mode

### **Current Regulation**

The chopping current ( $I_{CHOP}$ ) is the maximum current driven through either winding. This quantity depends on the sense resistor value ( $R_{XISEN}$ ).

$$I_{CHOP} = \frac{200mV}{R_{XISEN}}$$

 $I_{CHOP}$  is set by a comparator which compares the voltage across  $R_{XISEN}$  to a reference voltage. Note that  $I_{CHOP}$  must follow Equation 4 to avoid saturating the motor.

(3)

$$I_{FS}(A) < \frac{VM(V)}{R_L(\Omega) + R_{DS(ON)}HS(\Omega) + R_{DS(ON)}LS(\Omega)}$$

#### Where

- V<sub>M</sub> is the motor supply voltage.
- R<sub>L</sub> is the motor winding resistance.

#### Power Supply Recommendations

The DIO5833 is designed to operate from an input voltage supply ( $V_M$ ) range between 2.7 to 15 V. A 10 $\mu$ F ceramic capacitor rated for  $V_M$  must be placed as close to the DIO5833 as possible.

#### Sizing Bulk Capacitance for Motor Drive System

Bulk capacitance sizing is an important factor in motor drive system design. It depends on a variety of factors including:

- Type of power supply
- Acceptable supply voltage ripple
- Parasitic inductance in the power supply wiring
- Type of motor (brushed DC, brushless DC, stepper)

Motor startup current

### • Motor braking method

The inductance between the power supply and motor drive system limits the rate current can change from the power supply. If the local bulk capacitance is too small, the system responds to excessive current demands or dumps from the motor with a change in voltage. Size the bulk capacitance to meet acceptable voltage ripple levels.

The data sheet generally provides a recommended value, but system-level testing is required to determine the appropriate-sized bulk capacitor.



### Figure 9 Setup of Motor Drive System With External Power Supply

### Layout

### Layout Guidelines

Bypass the  $V_M$  terminal to GND using a low-ESR ceramic bypass capacitor with a recommended value of  $10\mu$ F rated for  $V_M$ . This capacitor should be placed as close to the  $V_M$  pin as possible with a thick trace or ground plane connection to the device GND pin and PowerPAD.

Bypass VINT to ground with a ceramic capacitor rated 6.3 V. Place this bypassing capacitor as close to the pin as possible.

### Layout Example





# Physical Dimensions:QFN3\*3-16







COMMON DIMENSIONS (UNITS OF MEASURE=MILLIMETER)						
Symbol	MIN	NOM	MAX			
А	2.9	3.0	3.1			
В	2.9	3.0	3.1			
С	0.70	0.75	0.80			
C1	0	0.025	0.05			
C2		0.203TYP				
D1		1.70 TYP				
D2		1.70TYP				
E	0.25TYP					
E1	0.50TYP					
F		0.40TYP				





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