

## MAX25512

# I<sup>2</sup>C-Controlled 4-Channel Low-Voltage 120mA LED Backlight Driver with Integrated Boost Converter

### General Description

The MAX25512 is a four-channel white LED backlight driver with an integrated current-mode boost converter which operates over a switching frequency range of 400kHz to 2.2MHz and incorporates spread spectrum. Phase-shifting of the output channels is included as an option to further reduce electromagnetic interference (EMI).

The device provides up to 120mA per channel and includes a control output for an external nMOS series switch. It is capable of operating down to 3V after startup.

The MAX25512 has an I<sup>2</sup>C interface to enable flexibility of control and detailed diagnostics.

The MAX25512 is available in a compact TQFN package and operates over the -40°C to +125°C temperature range.

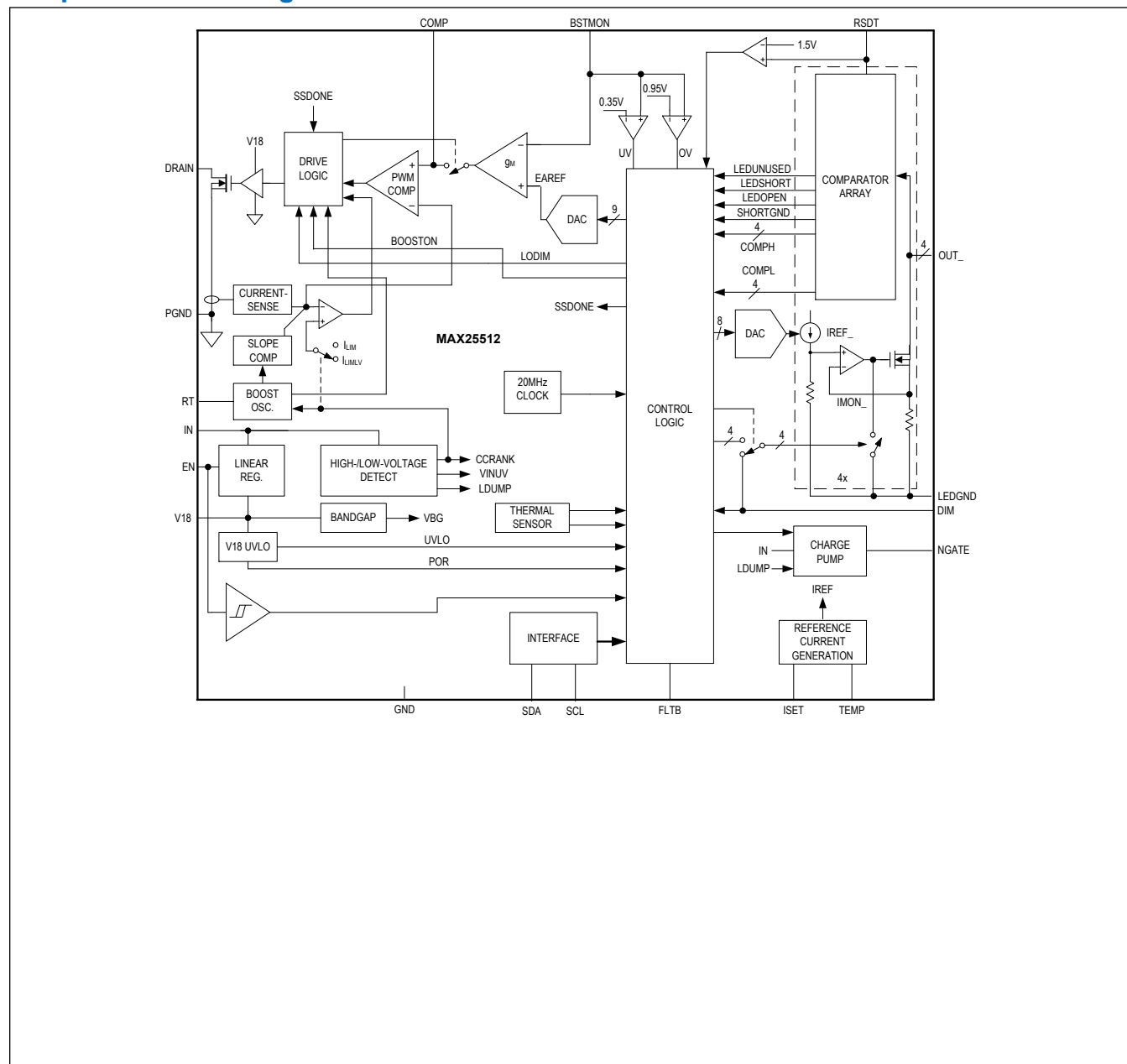
### Applications

- Automotive Instrument Clusters
- Automotive Central Information Displays
- Automotive Head-Up Displays

### Benefits and Features

- Operates Down to 3V on Battery Input after Startup
  - Wide Boost Duty Cycle to Support Low Input Voltage
- Boost or SEPIC Current-Mode DC-DC Controller
  - 400kHz to 2.2MHz Operating Frequency Range
  - Spread Spectrum Available
  - Ability to Synchronize to an External Clock
- LED Current Sinks
  - Up to 120mA Output Current per String
  - Low OUT<sub>REG</sub> Regulation Voltage for Best Efficiency
  - Optional Phase-Shifting of Outputs
- I<sup>2</sup>C Control for Enhanced Flexibility
- 16667:1 Dimming Ratio at 200Hz
- NTC Input for LED Current Foldback at High Temperature
- Hybrid Dimming Capable
- Built-in Programmable Automatic Fading Functionality
- Detailed Diagnostic Using I<sup>2</sup>C and FLTB Output
  - Shorted or Open LEDs
  - Thermal Shutdown
  - Output Undervoltage
- Compact, 4mm x 4mm TQFN Package
- AEC-Q100 Grade 1

## Simplified Block Diagram



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## Absolute Maximum Ratings

IN, EN to GND .....	-0.3V to +40V	PGND to GND.....	-0.3V to +0.3V
NGATE to IN.....	+6V	LEDGND to GND .....	-0.3V to +0.3V
NGATE to GND .....	-0.3V to +42V	DRAIN Current.....	±4.5A
OUT_ to LEDGND.....	-0.3V to +40V	OUT_ Continuous Current .....	±150mA
DRAIN to PGND .....	-0.3V to +40V	Continuous Power Dissipation (Multilayer Board) (T <sub>A</sub> = +70°C, derate 24.2mW/°C above +70°C.) .....	1938mW
V18, BSTMON to GND.....	-0.3V to +2.2V	Operating Temperature Range .....	-40°C to +125°C
SDA, SCL to GND .....	-0.3V to +6V	Junction Temperature .....	-40°C to +150°C
FLT, DIM to GND .....	-0.3V to +6V	Soldering Temperature (reflow) .....	+260°C
RT, COMP, ISET, TEMP, RSDT to GND .....	-0.3V to V18+0.3V		

Stresses beyond those listed under "Absolute Maximum Ratings" may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated in the operational sections of the specifications is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

## Package Information

### TQFN

Package Code	T2444+4C
Outline Number	<a href="#">21-0139</a>
Land Pattern Number	<a href="#">90-0022</a>
<b>Thermal Resistance, Single-Layer Board:</b>	
Junction to Ambient (θ <sub>JA</sub> )	48°C/W
Junction to Case (θ <sub>JC</sub> )	3°C/W
<b>Thermal Resistance, Four-Layer Board:</b>	
Junction to Ambient (θ <sub>JA</sub> )	36°C/W
Junction to Case (θ <sub>JC</sub> )	3°C/W

For the latest package outline information and land patterns (footprints), go to [www.maximintegrated.com/packages](http://www.maximintegrated.com/packages). Note that a "+", "#", or "-" in the package code indicates RoHS status only. Package drawings may show a different suffix character, but the drawing pertains to the package regardless of RoHS status.

Package thermal resistances were obtained using the method described in JEDEC specification JESD51-7, using a four-layer board. For detailed information on package thermal considerations, refer to [www.maximintegrated.com/thermal-tutorial](http://www.maximintegrated.com/thermal-tutorial).

## Electrical Characteristics

(V<sub>IN</sub> = V<sub>EN</sub> = 12V, T<sub>A</sub> = T<sub>J</sub> = -40°C to +125°C, unless otherwise noted. Typical values are at T<sub>A</sub> = +25°C, unless otherwise noted. ([Note 1](#)))

PARAMETER	SYMBOL	CONDITIONS	MIN	TYP	MAX	UNITS
<b>POWER SUPPLY</b>						
Operating Voltage Range	V <sub>IN</sub>		4.5		36	V
Operating Voltage Range after Start-Up		Maximum duration 100ms	3		36	V
Supply Current	I <sub>IN</sub>	No switching		1.3	1.8	mA
Shutdown Supply Current		V <sub>EN</sub> = 0V, +25°C		0.1	5	μA
IN Undervoltage Lockout, Rising	V <sub>INUVR</sub>		4.15	4.29	4.4	V
IN Undervoltage Lockout, Falling	V <sub>INUVF</sub>		2.77	2.9	2.95	V

**Electrical Characteristics (continued)**

( $V_{IN} = V_{EN} = 12V$ ,  $T_A = T_J = -40^{\circ}C$  to  $+125^{\circ}C$ , unless otherwise noted. Typical values are at  $T_A = +25^{\circ}C$ , unless otherwise noted. ([Note 1](#)))

PARAMETER	SYMBOL	CONDITIONS	MIN	TYP	MAX	UNITS
Threshold for Low-Voltage Operation Mode, Falling	$V_{LVF}$		5.4	5.5	5.7	V
Threshold for Low-Voltage Operation Mode, Rising	$V_{LVR}$		5.55	5.72	5.85	V
<b>V18 REGULATOR</b>						
V18 Voltage			1.75	1.8	1.85	V
V18 Undervoltage Lockout, Rising	$UVLOVCC_R$		1.6	1.65	1.69	V
V18 Undervoltage Lockout, Falling	$UVLOVCC_F$		1.54	1.575	1.61	V
V18 Short-Circuit Current Limit	$I_{SCV18}$	V18 shorted to GND		50		mA
<b>NGATE OUTPUT</b>						
NGATE Source Current			30	50		$\mu A$
NGATE Sink Current			0.5	1		mA
NGATE Output Voltage		Above $V_{IN}$ , $3V < V_{IN} < 33V$ , $I_{NGATE} = 0\mu A$	4.3	5.25	6.3	V
		Above $V_{IN}$ , $3V < V_{IN} < 33V$ , $I_{NGATE} = 10\mu A$	3.8	4.6	6	
NGATE Output Voltage at High Input Voltage		Above $V_{IN}$ , $V_{IN} > 35.5V$ , $I_{NGATE} = 1\mu A$	-0.05		0	V
$V_{IN}$ OV Comparator Threshold for NGATE, Rising	$V_{LDUMP\_TH}$		33		35.5	V
$V_{IN}$ OV Comparator Hysteresis for NGATE				0.7		V
NGATE Start Delay		Delay between NGATE charge-pump turning on and the boost converter starting		2	2.2	ms
<b>RT OSCILLATOR</b>						
Switching Frequency Range	$f_{SW}$	Frequency dithering disabled	400		2200	kHz
Oscillator Frequency Accuracy		$f_{SW} = 400kHz$ to $2200kHz$ , frequency dithering disabled	-10		10	%
Boost Converter Maximum Duty Cycle, High Frequency		1.3MHz to 2.2MHz	89	92	95	%
Boost Converter Maximum Duty Cycle, Low Frequency		$f_{SW} = 400kHz$ to 1.3MHz	94		98	%
Boost Minimum On-Time				60		ns



**Electrical Characteristics (continued)**

( $V_{IN} = V_{EN} = 12V$ ,  $T_A = T_J = -40^{\circ}C$  to  $+125^{\circ}C$ , unless otherwise noted. Typical values are at  $T_A = +25^{\circ}C$ , unless otherwise noted. ([Note 1](#)))

PARAMETER	SYMBOL	CONDITIONS		MIN	TYP	MAX	UNITS
Frequency Dither, High Setting		SSL = 0		+/-6			%
Frequency Dither, Low Setting	SS	SSL = 1		+/-4			%
RT Output Voltage	V <sub>RT</sub>	R <sub>RT</sub> = 65kΩ or R <sub>RT</sub> = 10kΩ		0.9			V
RT Out-of-Range Lower Limit				5	6.4		kΩ
RT Out-of-Range Upper Limit				90	111		kΩ
Sync Falling Threshold				0.77		0.84	V
Sync Frequency Duty-Cycle Range				50			%
Sync Frequency Range				400		2200	kHz
MOSFET							
DRAIN MOSFET R <sub>DS(ON)</sub>		I <sub>DRAIN</sub> = 1A		0.075	0.125		Ω
DRAIN Leakage Current		V <sub>DRAIN</sub> = 36V, T <sub>A</sub> = +25°C		0.03	1		μA
CURRENT-SENSE COMPARATOR							
Current-Limit Threshold at Low Input Voltage	I <sub>LIMLV</sub>			8.1	9.1	9.8	A
Current-Limit Threshold	I <sub>LIM</sub>			4.3	5.3	6	A
ERROR AMPLIFIER							
OUT_ Regulation High Threshold	V <sub>OUTH</sub>	V <sub>OUT_</sub> falling		0.825	0.85	0.875	V
OUT_ Regulation Low Threshold	V <sub>OUTL</sub>	V <sub>OUT_</sub> rising		0.55	0.58	0.61	V
Transconductance				410	630	890	μS
COMP Sink Current		V <sub>COMP</sub> = 1V		270	380	500	μA
COMP Source Current		V <sub>COMP</sub> = 1V		270	380	500	μA
LED CURRENT SINKS							
ISET Output Voltage	V <sub>ISET</sub>			0.75			V
OUT_ Output Current		R <sub>ISET</sub> = 12.5kΩ	120mA setting	116	120	124	mA
		R <sub>ISET</sub> = 15kΩ	100mA setting	97	100	103	
		R <sub>ISET</sub> = 30kΩ	50mA setting	48	50	52	
Channel-to-Channel Matching		I <sub>OUT_</sub> = 120mA		-2		2.2	%
		I <sub>OUT_</sub> = 50mA		-3.25		3.25	
Total OUT_ Leakage Current	I <sub>OUTLEAK</sub>	V <sub>OUT_</sub> = 36V, DIM = 0V, all OUT_ are shorted together		0.01		4	μA
OUT_ Minimum Pulse Width				300			ns
OUT_ Minimum Negative Pulse Width				90			ns

**Electrical Characteristics (continued)**

( $V_{IN} = V_{EN} = 12V$ ,  $T_A = T_J = -40^{\circ}C$  to  $+125^{\circ}C$ , unless otherwise noted. Typical values are at  $T_A = +25^{\circ}C$ , unless otherwise noted. ([Note 1](#)))

PARAMETER	SYMBOL	CONDITIONS	MIN	TYP	MAX	UNITS
OUT_ Current Rise Time		10% to 90% $I_{OUT\_}$ ( <a href="#">Note 2</a> )		150		ns
OUT_ Current Fall Time		90% to 10% $I_{OUT\_}$ ( <a href="#">Note 2</a> )		30		ns
<b>OVERVOLTAGE AND UNDERVOLTAGE PROTECTION</b>						
BSTMON Overvoltage Trip Threshold	$V_{BST\_OV}$	$V_{BSTMON}$ rising	0.93	0.95	0.97	V
BSTMON Hysteresis				50		mV
BSTMON Input Bias Current		$0 < V_{BSTMON} < 1.3V$	-1		+1	$\mu A$
BSTMON Undervoltage Detection Threshold, Rising	$V_{BST\_UVR,N}$	Normal soft-start	384	400	416	mV
	$V_{BST\_UVR,F}$	Fast soft-start	720	750	780	
BSTMON Undervoltage Detection Threshold, Falling	$V_{BST\_UVF}$	BSTMON falling, NGATE latched off	0.335	0.35	0.363	V
Boost Undervoltage Blanking Time, Standard Soft-Start		After EN pin taken high	49	53.25	57.5	ms
Boost Undervoltage Blanking Time, Fast Soft-Start		After EN pin taken high	26.18	28.46	30.74	ms
BSTMON Undervoltage Detection Delay	$t_{BST\_UV\_DEL}$	BSTMON falling	4	10	18	$\mu s$
<b>LED FAULT DETECTION</b>						
Maximum LED Short-Detection Threshold		$V_{RSDT} = 833mV$ rising	9.7	10	10.3	V
LED Short-Detection Threshold		$V_{RSDT} = 0.667V$	7.5	8	8.5	V
Minimum LED Short-Detection Threshold		$V_{RSDT} = 200mV$ rising	2.25	2.4	2.5	V
LED Short Disable Threshold		All active OUT_S rising	1.9	2	2.15	V
RSDT Pin Voltage Range			0.2		1	V
RSDT Disable/Switch-to-I <sup>2</sup> C Threshold			1.45	1.5	1.55	V
RSDT Pin Bias Current			-5		+5	$\mu A$
Short-Detection Comparator Delay	$t_{SD\_DEL}$			6.8		$\mu s$
OUT_ Check LED Source Current	$I_{CHKLED}$		50	60	70	$\mu A$
OUT_ Short to GND Detection Falling Threshold	$V_{TH\_SGND}$	Before boost converter start-up	230	250	270	mV

**Electrical Characteristics (continued)**

( $V_{IN} = V_{EN} = 12V$ ,  $T_A = T_J = -40^{\circ}C$  to  $+125^{\circ}C$ , unless otherwise noted. Typical values are at  $T_A = +25^{\circ}C$ , unless otherwise noted. ([Note 1](#)))

PARAMETER	SYMBOL	CONDITIONS	MIN	TYP	MAX	UNITS
OUT_ Unused Detection Threshold	$V_{TH\_UNUSED}$		0.775	0.85	0.925	V
OUT_ Open-LED Detection Threshold	$V_{OOL}$	During operation	230	250	270	mV
<b>LOGIC INPUT AND OUTPUTS</b>						
DIM, SDA, SCL Input Logic-High			1.6			V
DIM, SDA, SCL Input Logic-Low					0.4	V
DIM, SCL Input Leakage Current			-1		+1	$\mu A$
EN Input Logic-High			0.9			V
EN Input Logic-Low					0.6	V
EN Input Current		$V_{EN} = 5V$		0.01	1	$\mu A$
Minimum EN Pulse Width for Device Enable	$t_{EN\_ON}$		5			ms
EN Turn-Off Delay	$t_{EN\_OFF}$	Time between EN going low and complete device shutdown	11.5	12.8	14.1	ms
DIM Frequency Range			90		50000	Hz
DIM Sampling Frequency				20		MHz
FLTB Output Low Voltage		Sinking 3mA			0.4	V
FLTB Output Leakage Current		$V_{FLTB} = 5.5V$	-1		1	$\mu A$
SDA Output Leakage Current			-1		+1	$\mu A$
<b>TEMP PIN</b>						
TEMP Pin Voltage			180	200	220	mV
TEMP to ISET Gain		$V_{TEMP} < 250mV$	13.7	14.3	14.9	V/mA
TEMP Pin Disable Threshold				0.25		V
TEMP Pin Leakage Current		$+25^{\circ}C$		0.005	1	$\mu A$
ISET Voltage Threshold for LED Current Disable	$V_{TEMPD}$			150		mV
<b>THERMAL SHUTDOWN</b>						
Thermal-Shutdown Threshold	$T_{SHDN}$			160		$^{\circ}C$
Thermal-Shutdown Hysteresis				17		$^{\circ}C$
Thermal Warning Threshold	$T_{WARN}$	Temperature rising		125		$^{\circ}C$

**Electrical Characteristics (continued)**

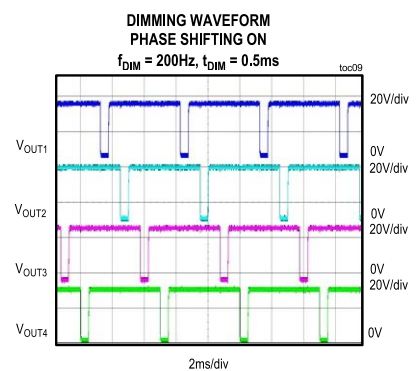
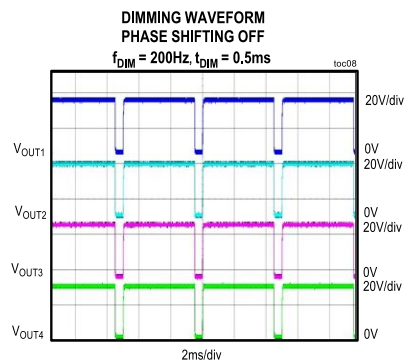
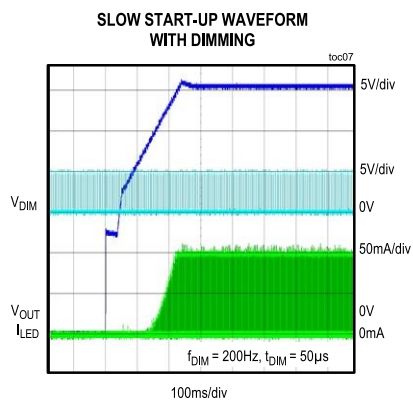
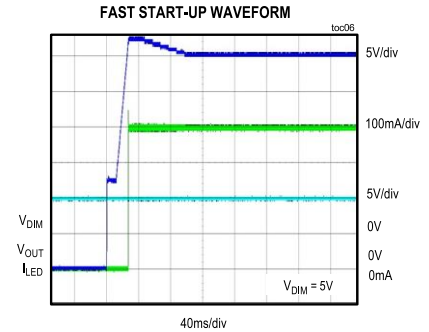
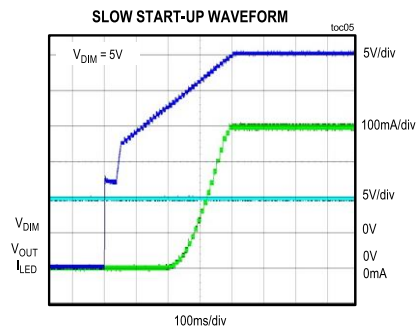
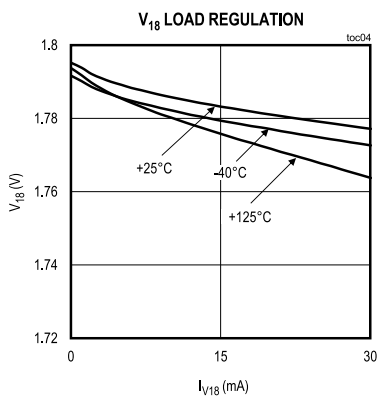
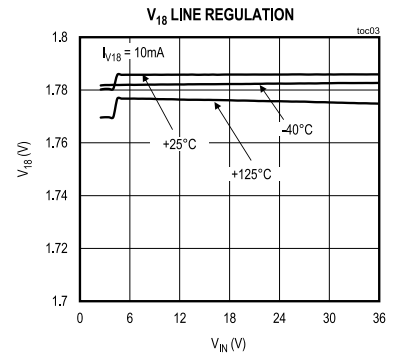
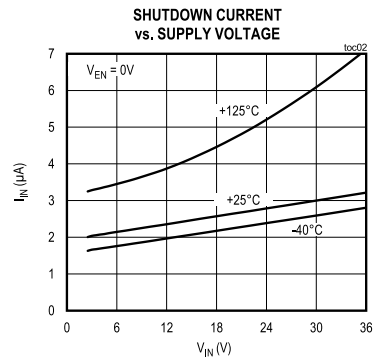
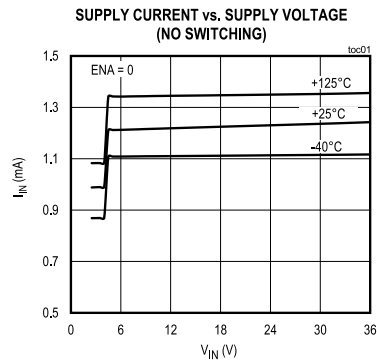
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PARAMETER	SYMBOL	CONDITIONS	MIN	TYP	MAX	UNITS
<b>I<sup>2</sup>C INTERFACE</b>						
Clock Frequency	$f_{SCL}$				0.4	MHz
Hold Time (Repeated) START	$t_{HD:STA}$		600			ns
SCL Low Time	$t_{LOW}$		1300			ns
SCL High Time	$t_{HIGH}$		600			ns
Setup Time (Repeated) START	$t_{SU:STA}$		600			ns
Data Hold Time	$t_{HD:DAT}$		0			ns
Data Setup Time	$t_{SU:DAT}$		100			ns
Setup Time for STOP Condition	$t_{SU:STO}$		600			ns
Spike Suppression				50		ns

**Note 1:** Limits are 100% tested at  $T_A = +25^{\circ}C$ ,  $T_A = +125^{\circ}C$ , and  $T_A = -40^{\circ}C$ . Limits over the operating temperature range and relevant supply voltage range are guaranteed by design and characterization.

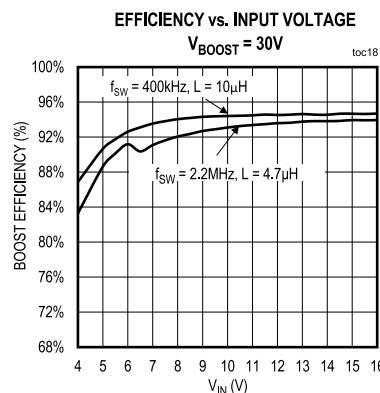
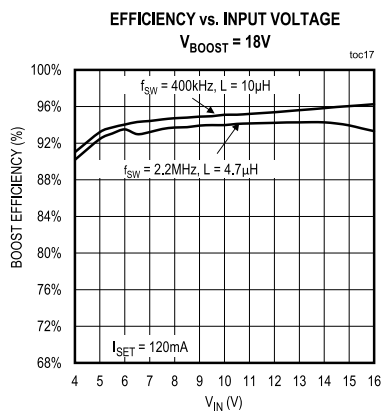
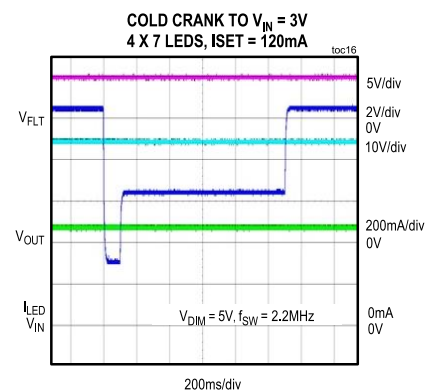
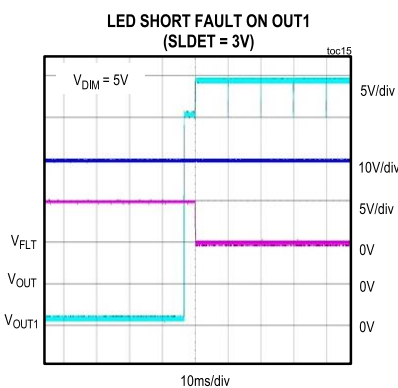
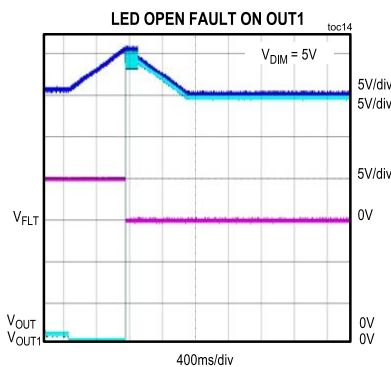
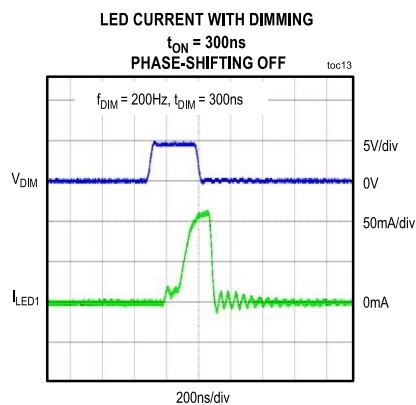
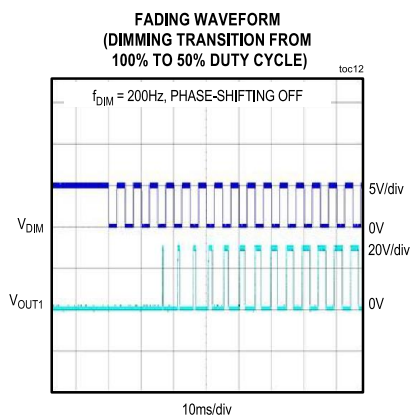
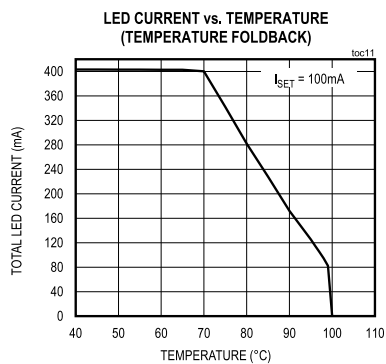
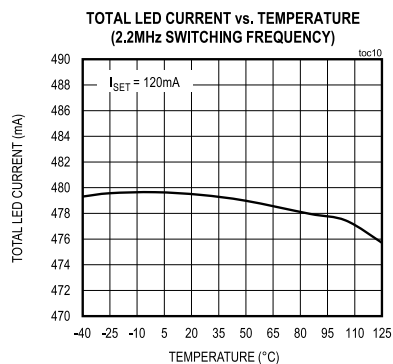
**Note 2:** Guaranteed by design.

## Typical Operating Characteristics

(V<sub>IN</sub> = V<sub>EN</sub> = 12V, 4x9 LED load at 100mA, f<sub>SW</sub> = 2.2MHz, T<sub>A</sub> = +25°C unless otherwise noted.)

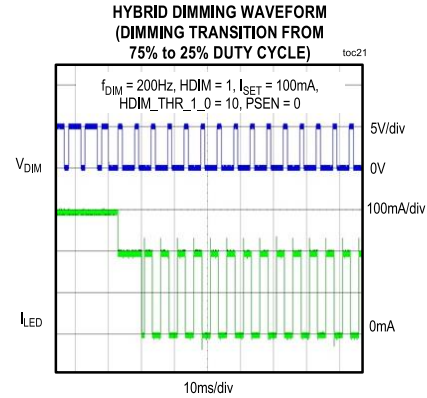
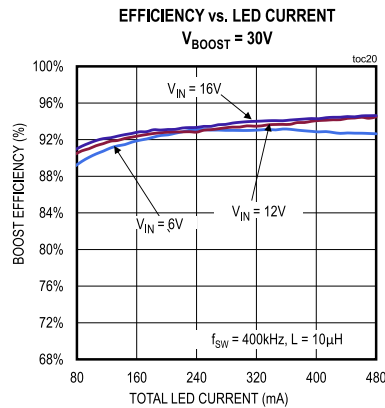
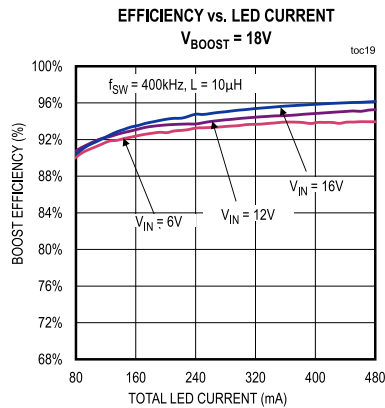
## Typical Operating Characteristics (continued)

( $V_{IN} = V_{EN} = 12V$ , 4x9 LED load at 100mA,  $f_{SW} = 2.2MHz$ ,  $T_A = +25^\circ C$  unless otherwise noted.)

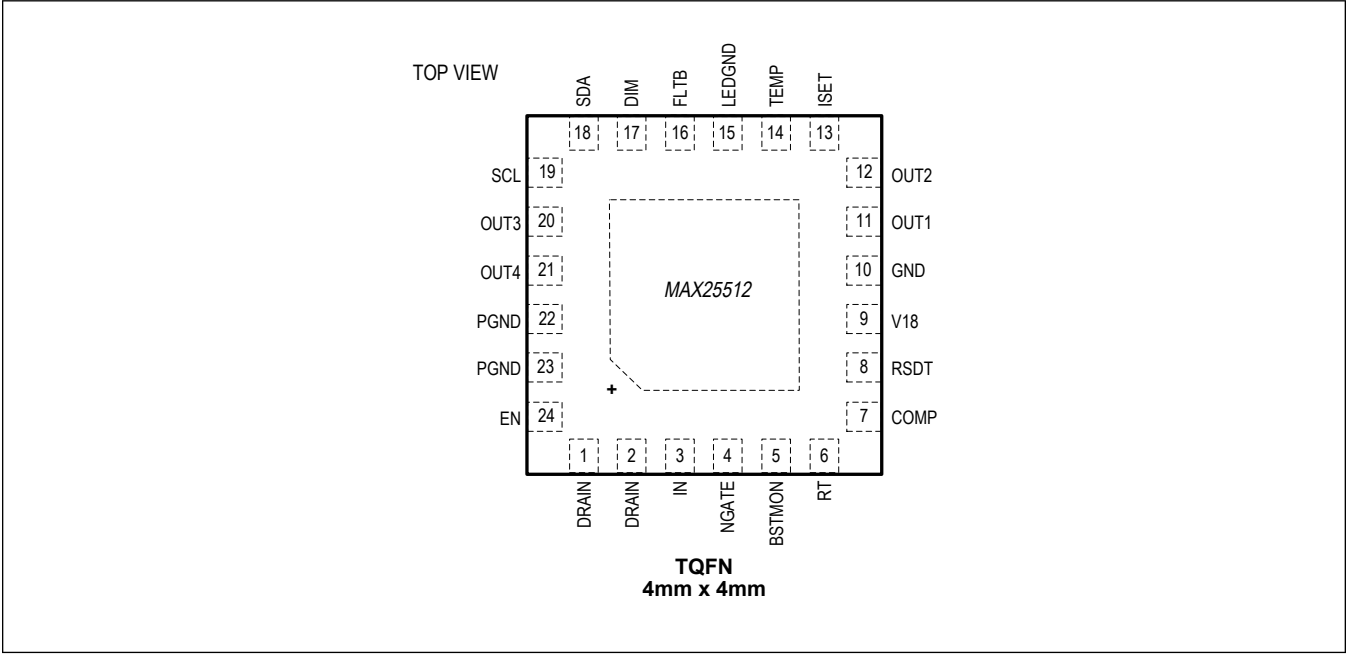


Typical Operating Characteristics (continued)

(V<sub>IN</sub> = V<sub>EN</sub> = 12V, 4x9 LED load at 100mA, f<sub>SW</sub> = 2.2MHz, T<sub>A</sub> = +25°C unless otherwise noted.)



Pin Configuration



Pin Description

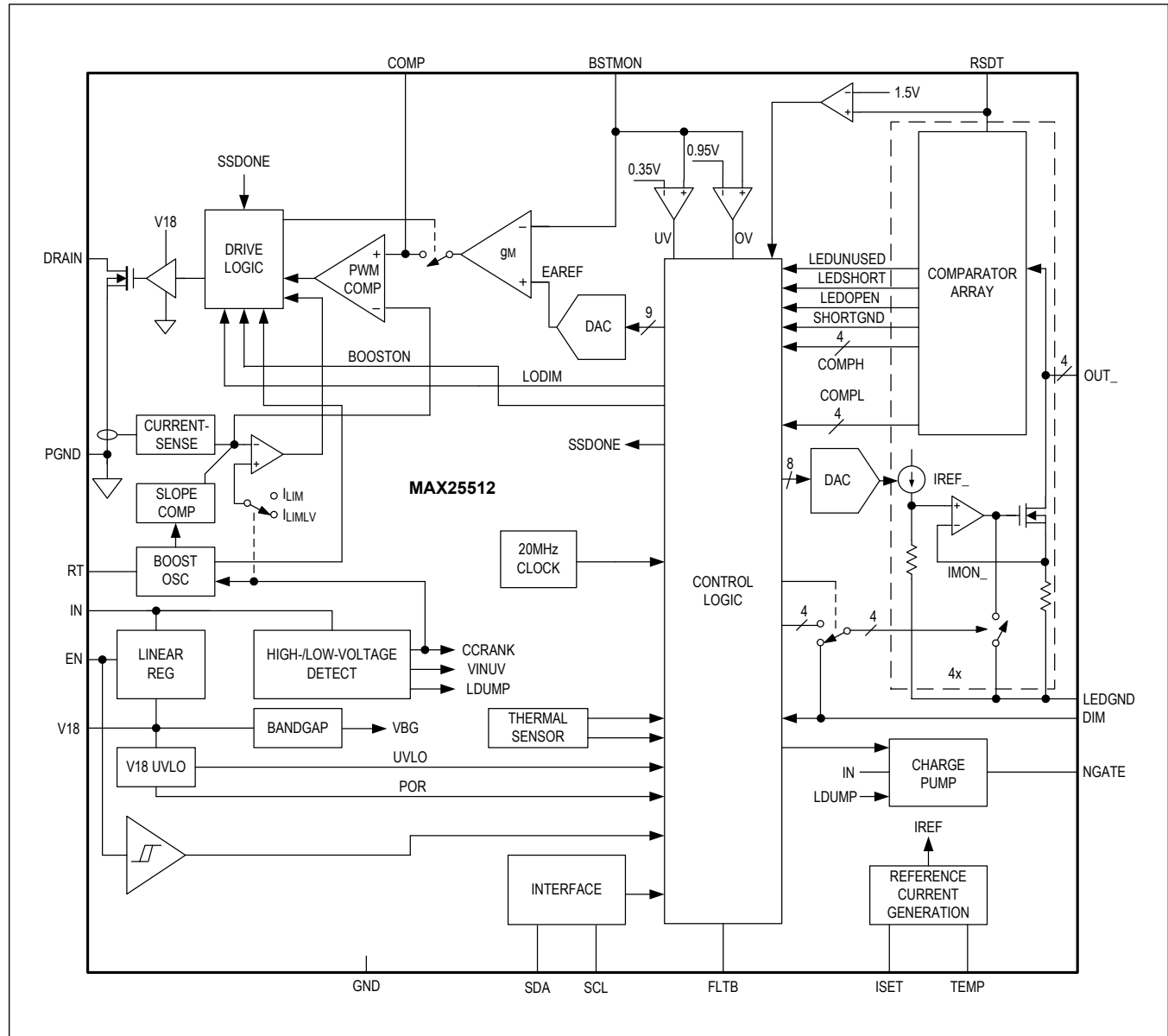
PIN	NAME	FUNCTION
1, 2	DRAIN	Drain Connection of Internal Switching Power nMOSFET. Connect to the external inductor and rectifier diode.
3	IN	Input Voltage. Connect to protected battery. Bypass IN with a minimum of 2.2µF in parallel with 0.1µF placed close to the pin.
4	NGATE	Gate Connection for External Series nMOSFET. Driven by the internal charge pump.

## Pin Description (continued)

PIN	NAME	FUNCTION
5	BSTMON	Boost Voltage Monitoring Input. Connect a resistor-divider from the boost converter output to GND with its midpoint connected to the BSTMON pin in order to set the maximum boost output voltage.
6	RT	Oscillator Timing Resistor Connection. Connect a timing resistor (RT) to GND to program the switching frequency. Apply an AC-coupled external clock at RT to synchronize the switching frequency with an external clock.
7	COMP	Switching Converter Compensation Input. Connect the compensation network from COMP to GND for current-mode control (see the <a href="#">Feedback Compensation</a> section).
8	RSDDT	LED Short Detection Threshold-Adjust Input. Connect a resistive divider from V18 to RSDDT and GND to program the LED short detection threshold. Connect RSDDT directly to V18 to disable LED short detection or when programming the threshold using the I <sup>2</sup> C interface.
9	V18	Output of Internal 1.8V Regulator. Connect 1μF and 0.1μF capacitors from V18 to GND with the 0.1μF capacitor placed closest to the pin.
10	GND	Signal GND. GND is the current return path connection for the low-noise analog signals. Connect GND, LEDGND, and PGND at a single point.
11	OUT1	LED String Cathode Connection 1. OUT1 is the open-drain output of the linear current sink that controls the current through the LED string connected to OUT1. OUT1 sinks up to 120mA.
12	OUT2	LED String Cathode Connection 2. OUT2 is the open-drain output of the linear current sink that controls the current through the LED string connected to OUT2. OUT2 sinks up to 120mA. If OUT2 is unused, connect a 10kΩ resistor from OUT2 to LEDGND.
13	ISSET	LED Current-Adjust Input. Connect a resistor (R <sub>ISSET</sub> ) from ISSET to GND to set the current through each LED string (I <sub>LED</sub> ), according to the formula $I_{LED} = 1500/R_{ISSET}$ . Place the resistor close to the pin to avoid parasitic capacitance.
14	TEMP	Temperature Sensor Input. To implement LED current reduction at high temperatures connect an NTC temperature sensor to GND with resistors from the NTC to TEMP and to V18. If unused, connect TEMP to V18.
15	LEDGND	LED Ground. LEDGND is the return path connection for the linear current sinks. Connect GND, LEDGND, and PGND at a single point.
16	FLTB	Open-Drain Fault Output. FLTB asserts low when a fault is detected. Connect a pull-up resistor from FLTB to a logic supply of 5V or lower.
17	DIM	Digital PWM Dimming Input. Apply a PWM signal to DIM for LED dimming control. Connect DIM to a logic supply of 5V or lower if dimming control is not used.
18	SDA	Bidirectional I <sup>2</sup> C Data Pin. Connect a pull-up resistor from this node to the logic supply voltage.
19	SCL	I <sup>2</sup> C Clock Input Pin. Connect a pull-up resistor from this node to the logic supply voltage.
20	OUT3	LED String Cathode Connection 3. OUT3 is the open-drain output of the linear current sink that controls the current through the LED string connected to OUT3. OUT3 sinks up to 120mA. If OUT3 is unused, connect a 10kΩ resistor from OUT3 to LEDGND.
21	OUT4	LED String Cathode Connection 4. OUT4 is the open-drain output of the linear current sink that controls the current through the LED string connected to OUT4. OUT4 sinks up to 120mA. If OUT4 is unused, connect a 10kΩ resistor from OUT4 to LEDGND.
22, 23	PGND	Power Ground. PGND is the DRAIN current return path connection. Connect GND, LEDGND, and PGND at a single point.
24	EN	Enable Input. Connect EN to logic-high for normal operation. When EN is taken low, the device is disabled after a delay of t <sub>EN_OFF</sub> . Do not leave the EN input open.



## Functional Diagrams



## Detailed Description

The MAX25512 is a 4-channel backlight driver IC with integrated boost converter for automotive displays. The integrated current outputs can each sink up to 120mA LED current. The device accepts a wide 3V to 36V input voltage range. The IC provides load-dump voltage protection up to 40V in automotive applications and incorporates three major blocks: a DC-DC converter with peak current-mode control to implement a boost or SEPIC-type switched-mode power supply, a 4-channel LED driver with up to 120mA constant-current sink capability per channel, and a logic control block.

The internal current-mode switching DC-DC converter supports boost or SEPIC topologies and operates in the 400kHz to 2.2MHz frequency range. Optional spread spectrum helps reduce EMI. An adaptive output-voltage-control scheme minimizes power dissipation in the LED current-sink paths.

The device tracks the external pulse-width-modulation (PWM) dimming input on DIM. The minimum pulse width is 300ns. Phase-shifted dimming of the strings is selectable for lower EMI.

Comprehensive diagnostic and protection features are implemented. The MAX25512 features an I<sup>2</sup>C interface for enhanced control and diagnostics.

### Enable

The internal regulator is enabled when the EN pin is high. To shut down the device, drive EN low. The current consumption reduces to  $\mu$ A levels.

The internal low dropout (LDO) regulator converts the input voltage at IN to a 1.8V output voltage at V18. The LDO regulator supplies current to the internal control circuitry and the gate driver.

### Undervoltage Lockout

The IC features two undervoltage lockouts (UVLOs) that monitor the input voltage at IN and the output of the internal LDO regulator at V18. The device turns on when EN is taken high, and the boost converter can be enabled if both IN and V18 are higher than their respective UVLO thresholds.

After startup, the device can operate down to 3V as described in the [Low-Voltage Operation](#) section.

### High-Voltage Operation

When the input voltage exceeds  $V_{LDUMP\_TH}$  the NGATE output follows the IN voltage and the external nMOSFET operates as a source follower. During this time, the power dissipation in the nMOSFET is higher than normal and is approximately  $V_t \times I_{LED(TOTAL)}$  where  $V_t$  is the threshold voltage of the external nMOSFET.

### Low-Voltage Operation

After the boost soft-start is complete, the MAX25512 continues to operate with IN voltages as low as 3V.

At very low input voltages, the efficiency of the boost converter reduces, and the input current can reach very high levels as a consequence. When the input voltage falls below  $V_{L\_VF}$ , the boost converter current limit is automatically increased to  $I_{LIMLV}$ , and the switching frequency is reduced if it is greater than 1.4MHz. In this mode, if the standard current limit ( $I_{LIM}$ ) is exceeded on four consecutive cycles, a 100ms timer is started. This returns the current limit to  $I_{LIM}$  when it expires. When the input voltage returns above  $V_{L\_VR}$ , operation at the normal switching frequency is resumed.

The external boost converter components must be selected for worst-case operation. An alternative is to reduce the output power at low input voltages.

If the voltage at IN drops below the undervoltage lockout level ( $V_{INUVF}$ ) at any time, the boost converter is disabled.

Operating Modes

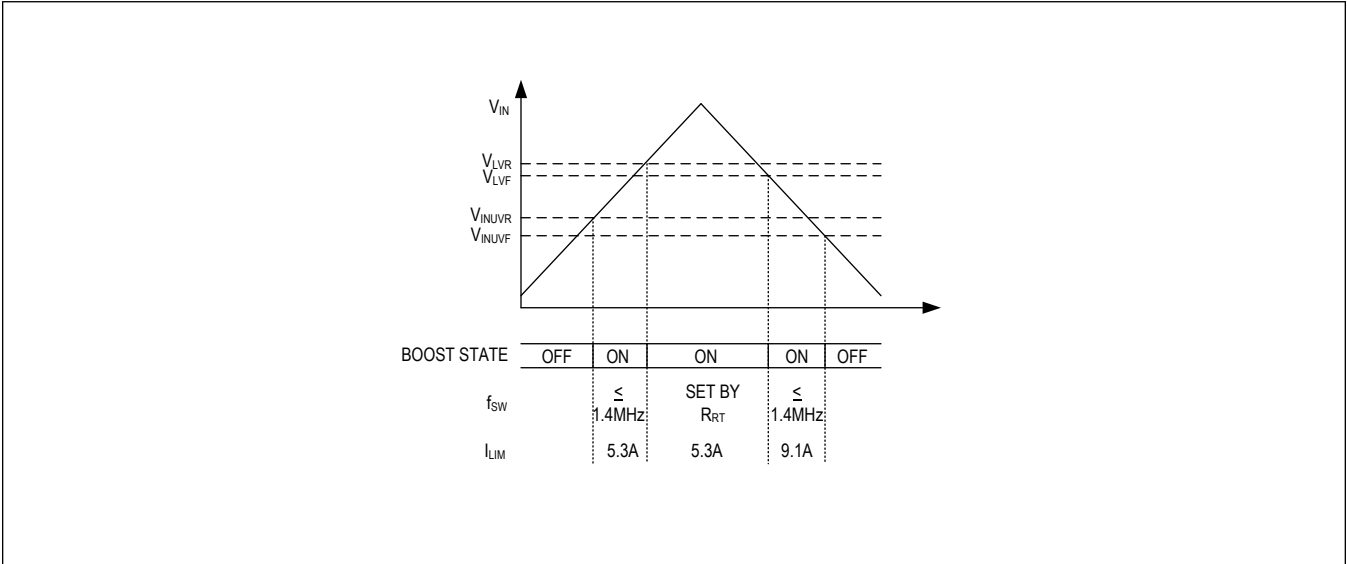


Figure 1. Boost Converter Operating Modes

Disabling Individual Strings

To disable an unused LED string, connect the unused OUT\_ to ground through a 10kΩ resistor, or set the corresponding DIS\_ bit to 1 in the DISABLE (0x13) register before the ENA bit is set. During startup, the device sources 60μA (typ) current through the OUT\_ pins and measures the corresponding voltage. For the string to be properly disabled, the OUT\_ voltage should measure between 270mV and 0.775V during this check. 270mV is the maximum threshold for the OUT\_ short-to-ground check, and 0.775V is the minimum unused string-detection threshold.

**Note:** When disabling unused strings, it is necessary to start by disabling the highest numbered current sinks first (e.g., if two strings need to be disabled, disable OUT4 and OUT3. Do not disable any two strings at random). During normal operation, strings can be selectively turned off by changing the corresponding TON\_ setting to 0. This is only possible when internal dimming is used, not when using the DIM input pin.

Current-Mode DC-DC Controller

The IC has a constant-frequency, current-mode controller designed to drive the LEDs in a boost or SEPIC configuration. The IC features multi-loop control to regulate the peak current in the inductor, as well as the voltage across the LED current sinks, to minimize power dissipation.

The internal MOSFET is turned on at the beginning of every switching cycle. The inductor current ramps up linearly until it is turned off at the peak current level set by the feedback loop. The peak inductor current is sensed internally, and slope compensation is added.

The IC features leading-edge blanking to suppress the MOSFET switching noise. A PWM comparator compares the current-sense voltage plus the slope-compensation signal with the output of the transconductance error amplifier. The controller turns off the MOSFET when the total current-sense voltage exceeds the error amplifier's output voltage, which is also the voltage on the COMP pin. This process repeats every switching cycle to achieve peak current-mode control.

In addition to the peak current-mode-control loop, the IC has two other feedback loops for control. The converter output voltage is sensed through the BSTMON input, which goes to the inverting input of the error amplifier. The other feedback comes from the OUT\_ current sinks. This loop controls the headroom of the current sinks to minimize total power dissipation while still ensuring accurate LED current matching. Each current sink has a window comparator with a low threshold of  $V_{OUTL}$  and a high threshold of  $V_{OUTH}$ . The outputs of these comparators control an up/down counter. The up/down counter is updated on every falling edge of the DIM input and drives a 9-bit DAC that sets the reference to the error amplifier. When dimming is set to 100%, the counter is updated at intervals of 10ms.

**9-Bit Digital-to-Analog Converter**

The error amplifier's reference input is controlled with an 9-bit digital-to-analog converter (DAC). The DAC output is ramped up slowly during startup to implement a soft-start function (see the [Startup Sequence](#) section). During normal operation, the DAC output range is limited to 0.48V to 1V. Because the DAC output is limited to no less than 0.48V during normal operation, the overvoltage threshold for the output should be set to a value less than twice the minimum LED forward voltage. The DAC LSB determines the minimum step in output voltage according to the equation:

$$V_{STEP\_MIN} = V_{DAC\_LSB} \times A_{OVP}$$

where,

$V_{STEP\_MIN}$  = Minimum output-voltage step

$V_{DAC\_LSB}$  = DAC least significant bit size (1.95mV)

$A_{OVP}$  = BSTMON resistor-divider gain (1 + R6/R7)

**LED Current Control**

The full-scale sink current for the outputs (OUT1–OUT4) is set using the resistor on the ISET pin. Use the following equation to calculate the resistor value:

$$R_{ISET} = \frac{1500}{I_{LED}}$$

where  $I_{LED}$  is the individual OUT\_ current.

If the  $R_{ISET}$  value is less than 11.9kΩ, the device may not operate.

When PWM dimming is used, the current in the OUT\_ channels switches between zero and the full-scale sink current at the set duty cycle.

**Analog Dimming**

By using the ADIM register, the OUT\_ current set by the resistor on the ISET pin can be reduced in 255 steps. Each step represents 0.4% of the ISET current. When ADIM is set to 0xFF, the full-scale current is provided.

**Dimming**

Dimming can be performed using an external PWM signal applied to the DIM pin or by writing to the TON\_ registers. The signal on the DIM pin is sampled with a 20MHz internal clock except when phase-shifting is disabled, in which case, the DIM signal controls the OUT\_ outputs directly.

The device tracks frequency changes in the external pulse-width-modulation (PWM) dimming input on DIM in phase-shift mode.

**Low-Dimming Mode**

The IC's operation changes at very narrow dimming pulses to ensure a consistent dimming response of the LEDs. If the dimming on-time is lower than 50μs (typ), the device enters low-dimming mode. In this state, the converter switches continuously, and LED short detection is disabled. When the DIM input is greater than 51μs (typ), the device goes back into normal operation, enabling the short-LED detection and switching the power FET only when the effective dimming signal is high.

By setting the BSTFORCE bit in the ISET\_REG register to 1, it is possible to force the boost converter to run continuously independent of the state of the DIM input.

**Phase-Shift Dimming**

When the PSEN bit in register 0x02 is set phase shifting of the LED strings is enabled. The device automatically sets the phase shift between strings to 90°, 120°, or 180° depending on the number of strings enabled.

**Automatic Fade-In/Fade-Out During Dimming**

The device can be configured to perform a smooth change in brightness, even when the DIM input duty cycle or TON\_ setting is suddenly changed by setting the FADE\_IN\_OUT bit in the FADING\_REG register to 1.

When using the fade function, it is important to maintain the DIM frequency constant while entering and leaving 100% duty cycle. This is necessary in order to avoid erroneous frequency measurement that can change the speed of the fade-in/out.

The step size in the dimming transition is either 6.25% or 12.5% depending on the setting of the FADE\_GAIN bit. The total transition time can be set by writing the TDIM field to a value between 0 to 5, where the value sets the update speed to once every 2<sup>TDIM</sup>. The transition time depends on the initial and final dimming values according to:

$$t = \frac{1}{f_{\text{DIM}}} \times 2^{\text{TDIM}} \times \frac{\ln(\text{DIM}_F) - \ln(\text{DIM}_i)}{\text{FADE\_GAIN}}$$

where  $f_{\text{DIM}}$  is the dimming frequency, TDIM is the TDIM register setting, DIM<sub>F</sub> is the final dimming setting, DIM<sub>i</sub> is the initial dimming setting, and FADE\_GAIN is either 0.0625 or 0.125. For this equation, DIM<sub>F</sub> should be larger than DIM<sub>i</sub> but, since the fading function is symmetrical, the values can be swapped if the final dimming ratio is lower than the initial one.

When transitioning to 100% dimming with fading enabled, do not change the input dimming from 100% until the complete fading transition to 100% is complete. Use the above equation to determine the transition time.

### Hybrid Dimming

In hybrid dimming mode, the external LEDs are dimmed by first reducing their current as the dimming duty-cycle decreases from 100% (see [Figure 2](#)). At the crossover level set by the HDIM\_THR\_1\_0[1:0] bits (50%, 25%, 12.5% or 6.25%), dimming transitions to PWM dimming where the LED current is chopped. To select hybrid dimming, set the HDIM bit in the IMODE (0x03) register. Select the desired crossover level between analog and PWM dimming using the HDIM\_THR\_1\_0[1:0] bits in the same register. Depending on the DIM\_EXT bit, the device functions in one of the following two ways:

1. (DIM\_EXT = 1) measures the duty cycle on the DIM pin and translates it into a combined LED current value and PWM setting.
2. (DIM\_EXT = 0) takes the 18-bit value from the TON1 register and translates it into a combined LED current value and PWM setting.

When hybrid dimming is used with an internal dimming setting (DIM\_EXT = 0), only the value TON1[17:0] is used. It is not possible to have individual dimming settings for each channel in this mode.

Note that when hybrid dimming is enabled, the ADIM register has no effect.

[Figure 3](#) illustrates the difference between standard and hybrid dimming with phase-shifting enabled.

Hybrid Dimming Operation

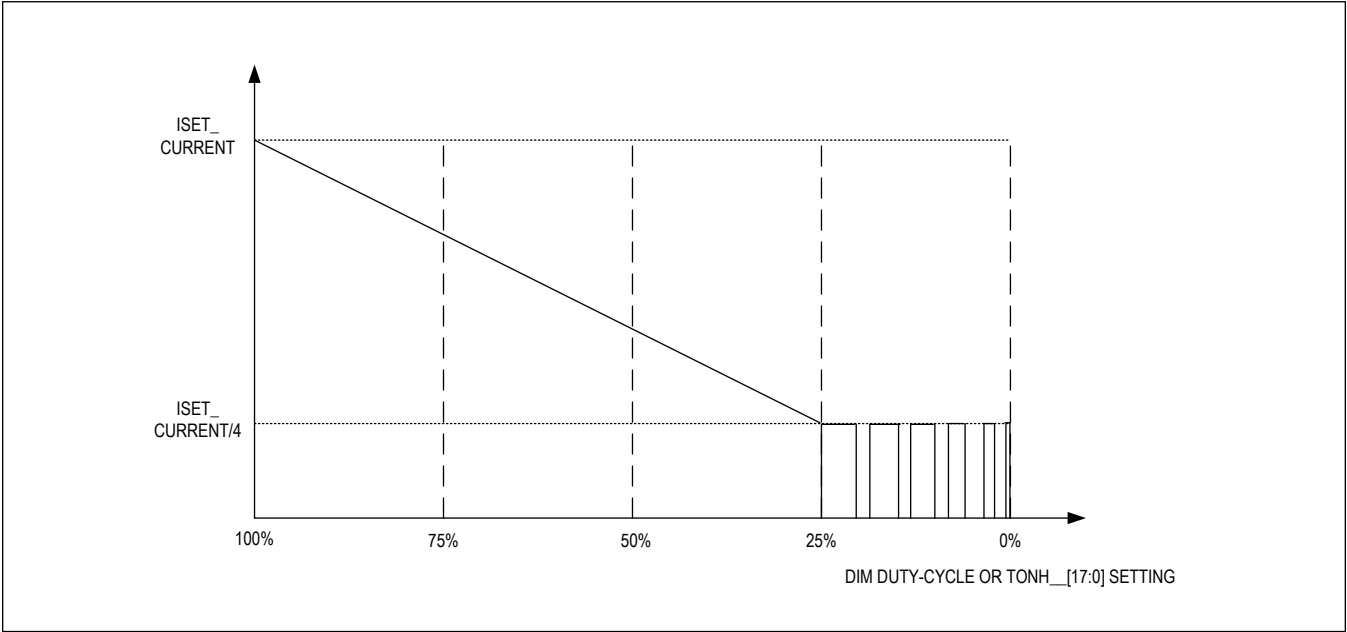


Figure 2. Hybrid Dimming Operation with HDIM[1:0] = 10 (25%)

Hybrid Dimming Operation Modes

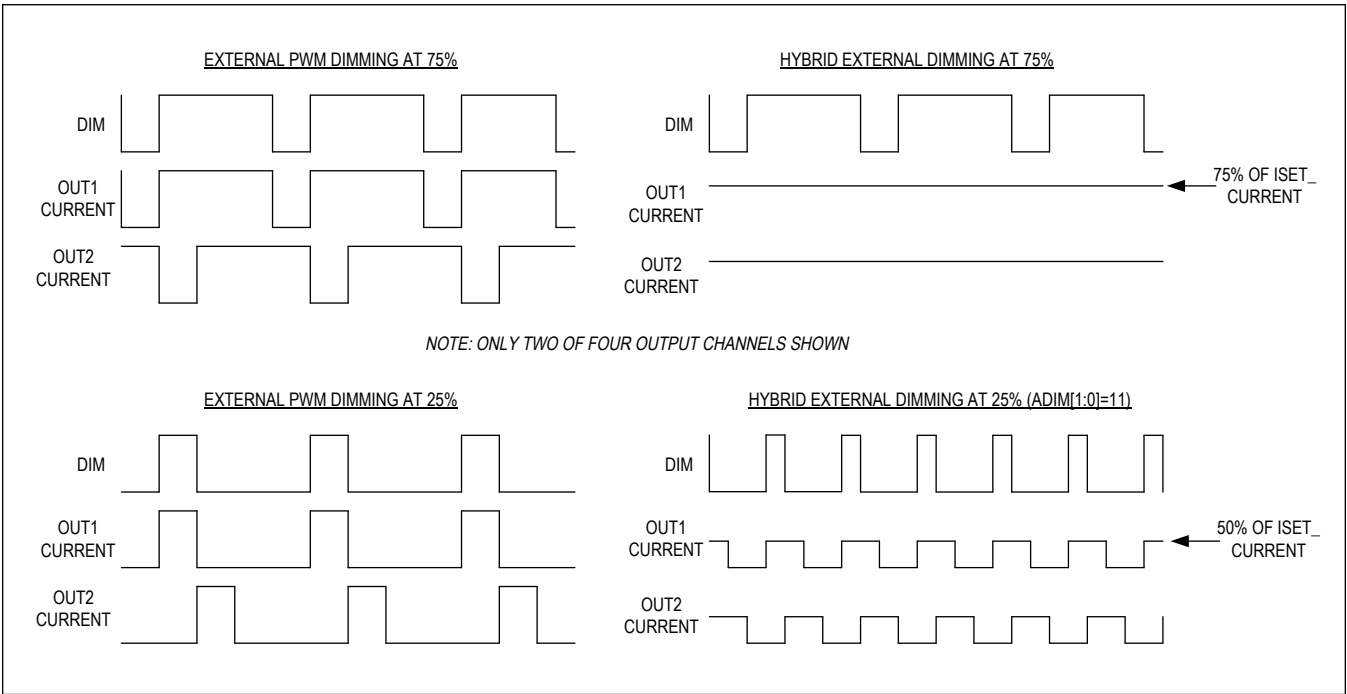


Figure 3. Hybrid Dimming Operation Modes

**Startup Sequence**

When the EN pin is taken high (assuming the IN voltage is above its undervoltage-lockout value), the internal regulator and the I<sup>2</sup>C interface are turned on. The total duration of this phase of the startup is 2ms (max). After this phase, the I<sup>2</sup>C interface can be used, and the device registers can be written. The ENA bit should be set to 1 to enable the boost and subsequently the OUT\_ current sinks. Before setting the ENA bit to 1, fast soft-start can be chosen by setting the FAST\_SS bit to 1. When the ENA bit is set high, the device checks the OUT\_ channels for short-circuits to GND. If any of the OUT\_ pins are detected as shorted to GND, the boost converter does not start. This avoids possible damage. The corresponding OUT\_SG bit(s) are set. The device also detects and disconnects any unused current-sink channels connected to GND by means of a 10kΩ resistor. Alternatively, individual channels can be disabled using the DIS[4:1] bits. The subsequent startup sequence occurs in three stages.

**Stage 1**

After the ENA bit is set high, the controller turns on the charge-pump for the external nMOSFET. The output current of the charge-pump charges the gate of the external nMOSFET to turn it on. After a 2ms timeout expires, stage 2 of the startup begins.

**Stage 2**

After the external nMOSFET is turned on, the converter starts switching, and the output begins to ramp. The DAC reference to the error amplifier is stepped up 1 bit at a time until the voltage at BSTMON reaches 480mV or 0.88V when fast soft-start is selected. This stage duration is fixed at approximately 50ms (typ) or 25ms (typ) when fast soft-start is selected. If the BSTMON voltage is greater than 480mV at the end of stage 2, the device transitions directly to stage 3. The BSTMON pin is sampled at the end of this stage. If its voltage is less than 350mV (typ), FLTB is asserted low, the power converter is turned off, the external nMOSFET on NGATE is turned off, and they all remain off until the ENA bit is toggled.

**Stage 3**

The third stage begins once stage 2 is complete, and the DIM input goes high. During stage 3, the output of the converter is adjusted until the minimum OUT\_ voltage falls between the V<sub>OUTH</sub> and V<sub>OUTL</sub> comparator limits. The output adjustment is again controlled by the DAC, which provides the reference for the error amplifier. The DAC output is updated on each rising edge of the DIM input pin. If the DIM input is at 100% duty cycle (DIM = high), the DAC output is updated once every 10ms.

The total soft-start time can be calculated using:

$$t_{SS} = 52\text{ms} + \frac{(V_{LED} + 0.715) - (0.48 \times A_{OVP})}{f_{DIM} \times 0.00975 \times A_{OVP}}$$

where,

$t_{SS}$  = Total soft-start time

52ms = Fixed stage 1 + stage 2 duration

$V_{LED}$  = Total forward voltage of the LED strings

0.715V = Midpoint of the window comparator

$f_{DIM}$  = Dimming frequency (use 100Hz for  $f_{DIM}$  when input duty cycle is 100%)

0.00975V = 5 times the 1.95mV LSB of the DAC

$A_{OVP}$  = Gain of the BSTMON resistor-divider or  $1 + R_6/R_7$ , and

0.48V = Voltage on BSTMON after stage 2

If fast soft-start is enabled, the soft-start is accelerated, and the final value of the voltage on the BSTMON pin is 0.88V. The equation for the total soft-start time then becomes:

$$t_{SS} = 27\text{ms} + \frac{(0.88 \times A_{OVP}) - (V_{LED} + 0.715)}{f_{DIM} \times 0.00975 \times A_{OVP}}$$

After the soft-start period, a fault is detected whenever the BSTMON pin falls below  $V_{BST\_UVF}$ .

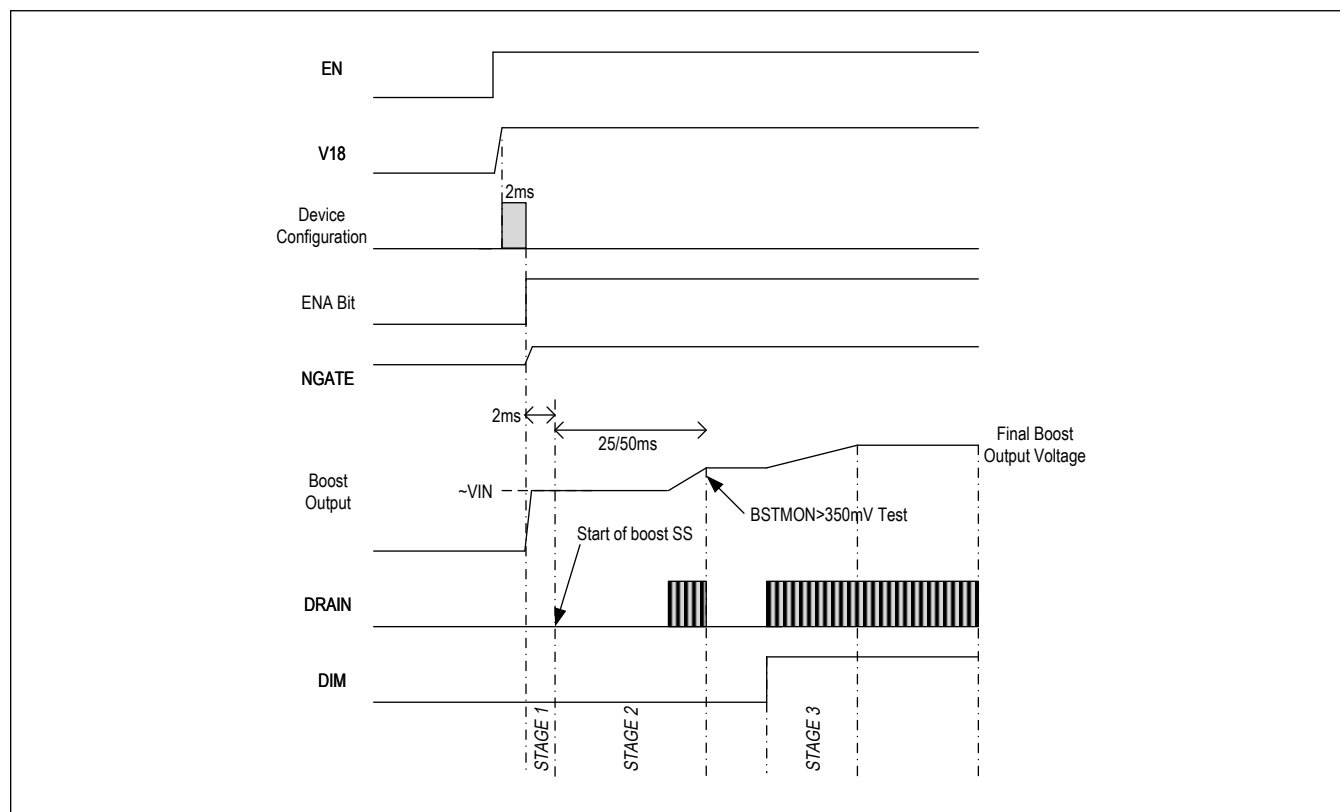
**Boost Startup**

Figure 4. Boost Startup Waveforms

**Oscillator Frequency/External Synchronization**

The internal oscillator frequency is programmable between 400kHz and 2.2MHz using a timing resistor ( $R_{RT}$ ) connected from the RT pin to GND. Use the following equation to calculate the value of  $R_{RT}$  for the desired switching frequency ( $f_{SW}$ ).

$$R_{RT} = \frac{26.4 \times 10^6}{f_{SW}} - 0.32$$

where  $R_{RT}$  is in k $\Omega$  and  $f_{SW}$  is in Hz. For example, a 12k $\Omega$  resistor on pin RT sets a switching frequency of 2.14MHz.

If the value of the RT resistor is out of range or the pin is shorted to GND, the boost converter cannot start when the ENA bit is set to 1; the RTOOR bit is set, and the FLTB pin goes low.

Synchronize the oscillator with an external clock by AC-coupling the external clock to the RT input. The value of the capacitor used for AC-coupling is  $C_{SYNC} = 10\text{pF}$ . The duty cycle of the external clock should be 50%. When synchronizing the converter, do not apply the synchronizing signal to the RT pin at start-up as this may cause the RT resistor value check to fail.

At low input voltages, and when the switching frequency is above 1.4MHz, the switching frequency is automatically reduced by 30% to enable high-duty-cycle operation and maintain output voltage regulation. This also applies when the device is synchronized to an external frequency.

**Spread Spectrum**

The IC includes spread spectrum that reduces peak electromagnetic interference (EMI) at the switching frequency and its harmonics. Spread spectrum can be enabled and disabled using the SS\_OFF bit in the register SETTING\_REG.



Spread spectrum uses a pseudorandom dithering technique where the switching frequency is varied in the range 94% to 106% or 96% to 104% of the programmed switching frequency set through the external resistor from RT to GND.

Spread spectrum is disabled if external synchronization is used.

### Fault Protection

Fault protection in the IC includes cycle-by-cycle current limiting in the PWM controller, DC-DC converter output-undervoltage protection, output-overvoltage protection, open-LED detection, short-LED detection and protection, and overtemperature shutdown. Thermal shutdown and shorted-LED faults are automatically cleared when the fault is removed; however, FLTB stays low until the relevant fault register is read. It is cleared when the fault condition is removed during thermal shutdown and when shorted LEDs are identified. FLTB is latched low for an open-LED and can be reset by cycling power or by toggling the EN pin.

### Open-LED Management and Overvoltage Protection

After the soft-start of the boost converter, the IC detects open-LED strings and disconnects any such strings from the internal minimum OUT\_ voltage detector. This keeps the DC-DC converter output voltage within safe limits and maintains high efficiency.

During normal operation, the DC-DC converter output-regulation loop uses the minimum OUT\_ voltage as the feedback input. If any LED string is open, the voltage at the opened OUT\_ goes to V<sub>LEDGND</sub>. The DC-DC converter output voltage then increases to the overvoltage-protection threshold set by the voltage-divider network connected between the converter output, the BSTMON input, and GND. The overvoltage-protection threshold at the DC-DC converter output is determined using the following equation:

$$V_{OUT\_BSTMON} = 0.95 \times \left(1 + \frac{R6}{R7}\right)$$

where 0.95V (typ) is the overvoltage threshold on BSTMON (see the [Functional Diagram](#)). Select V<sub>OUT\\_BSTMON</sub> according to the following formula:

$$1.1 \times (V_{LED\_MAX} + 0.875) < V_{OUT\_BSTMON} < 2 \times (V_{LED\_MIN} + 0.55)$$

where,

V<sub>LED\\_MAX</sub> = Maximum expected LED string voltage

V<sub>LED\\_MIN</sub> = Minimum expected LED string voltage

Select R6 and R7 so that the voltage at OUT\_ does not exceed the absolute maximum rating. As soon as the DC-DC converter output reaches the overvoltage-protection threshold, the internal MOSFET is switched off.

The overvoltage threshold should be set to less than twice the minimum LED voltage to ensure proper operation and so that the BSTMON minimum regulation point of 0.48V (typ) is not breached. When an open-LED overvoltage condition occurs, FLTB is latched low. Any current-sink output with V<sub>OUT\_</sub> < V<sub>OOL</sub> is permanently disconnected from the minimum voltage detector.

### OUT\_ Short-to-GND Detection

During device start-up, the OUT\_ pins are checked for short circuits to ground by sourcing a current I<sub>CHKLED</sub> into the OUT\_ pin and measuring the resultant voltage. If the voltage is below V<sub>TH\_SGND</sub>, the OUT\_ is considered shorted to ground and the boost converter does not start.

### Shorted-LED Detection

The IC checks for shorted LEDs after the current in any channel is turned on. A shorted-LED is detected at OUT\_ if the following condition is met.

$$V_{OUT\_} > V_{SLDET}$$

where V<sub>SLDET</sub> = 12x the voltage set on the RSDT pin or when the RSDT pin is connected to V18, the value set by the SLDET[1:0] bits in the SETTING (0x12) register.

If a short is detected on any of the strings, the affected LED strings are disconnected, and the FLTB output flag asserts low until the device detects that the shorts are removed. Disable short-LED detection by connecting RSDT to V18 with

SLDET[1:0] set to 0x0. Short-LED detection is disabled in low-dimming mode.

In external dimming mode with the DIM input connected continuously high, the OUT\_ pins are periodically scanned to detect shorted LEDs. The scan frequency is 100Hz. Similarly, when DIM\_EXT = 0 and internal dimming is used, shorted LEDs are still detected by periodically scanning the OUT\_ states at 100Hz.

**Thermal Warning**

If the junction temperature of the device reaches T<sub>WARN</sub> or if the TEMP pin reaches the voltage representing the temperature T1, the over-temperature warning (OTW) bit in the DIAG\_REG register is set. In addition, if the OTWMASK bit is 0 the FLTB pin is asserted low.

**Thermal Shutdown**

The IC includes thermal protection that operates at a temperature of T<sub>SHDN</sub>. When the thermal-shutdown temperature is reached, the device is immediately disabled so it can cool. When the junction temperature falls by 17°C, the device is re-enabled and the boost converter performs a soft-start. When a thermal shutdown occurs, the FLTB pin goes low.

**Temperature Foldback**

When an NTC temperature sensor is connected between GND and a resistor (RT1) connected to the V18 supply, with a further resistor (RT2) connected from the junction of the NTC and RT1 to the TEMP pin, temperature foldback is implemented. When the temperature reaches the temperature T1 (set by RT1), the current in the LEDs is reduced according to the linear scheme shown in [Figure 5](#). The slope of the current reduction is set nominally by RT2. The MAX25512 is designed to be used with the NTCLE100E3103\*B0 or a similar NTC device. [Table 1](#) illustrates some examples of values of RT1 and RT2 to obtain certain values of T1 and T<sub>DELTA</sub>.

**Table 1. Temperature Foldback Sample Resistor Values**

RT1	RT2	T1	T <sub>DELTA</sub>
20kΩ	2.7kΩ	+60°C	+40°C
14kΩ	2.1kΩ	+70°C	+30°C
10kΩ	1.78kΩ	+80°C	+25°C

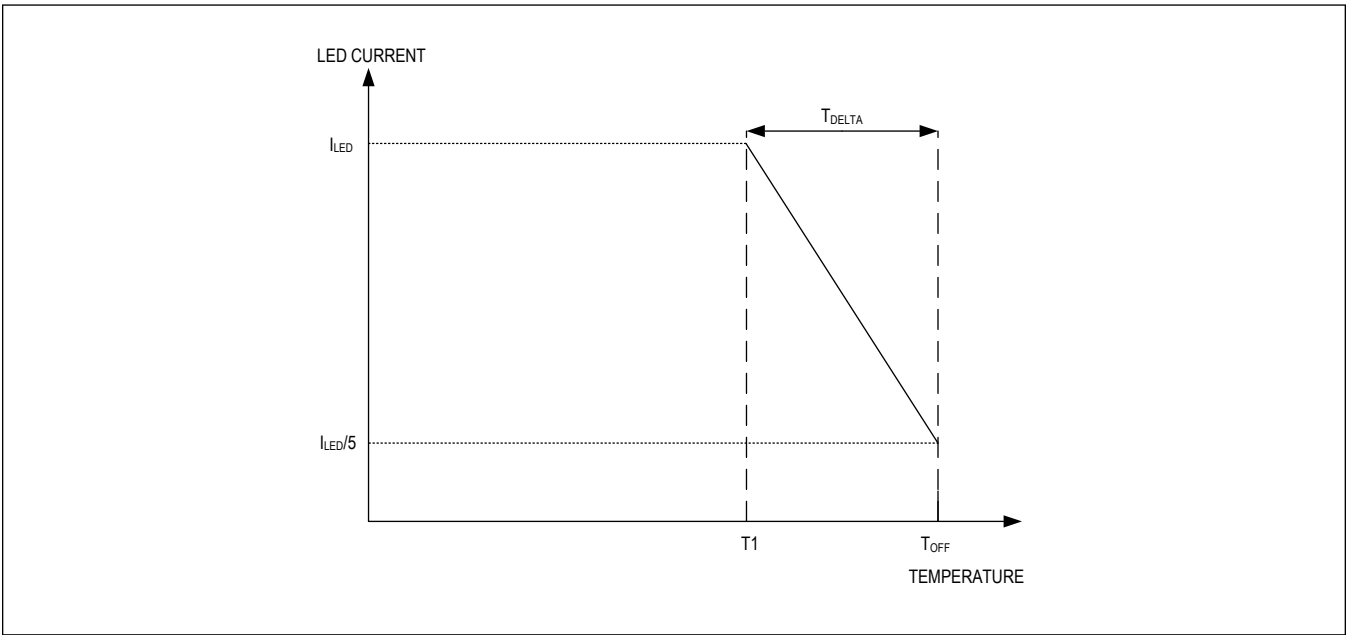


Figure 5. Temperature Foldback Curve

MAX25512

I<sup>2</sup>C-Controlled 4-Channel Low-Voltage 120mA  
LED Backlight Driver with Integrated Boost  
Converter

**Above Temperature T1**  
When the temperature reaches T1, the OTW bit in register DIAG\_REG is asserted. When the temperature reaches T<sub>OFF</sub>, the LED current is turned off and the FLTB pin asserts low.

**TEMP External Circuit**

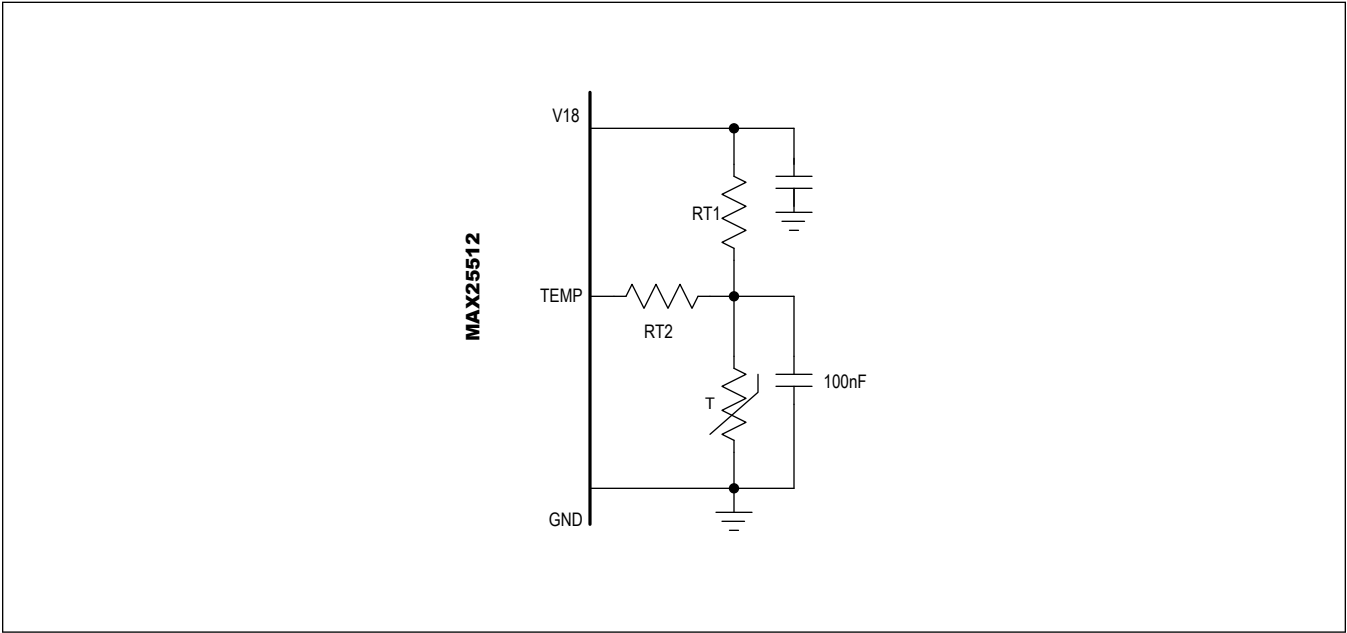


Figure 6. TEMP External Circuit

**I<sup>2</sup>C Interface**

**Slave Address**

**Table 2. I<sup>2</sup>C Slave Address**

	DEVICE ADDRESS							WRITE ADDRESS	READ ADDRESS
	A6	A5	A4	A3	A2	A1	A0		
MAX25512ATG	0	1	0	0	0	1	0	0x44	0x45

## Register Map

## MAX25512

ADDRESS	NAME	MSB							LSB
USER_REGISTERS									
0x00	<a href="#">DEV_ID_REG[7:0]</a>	DEV_ID[7:0]							
0x01	<a href="#">REV_ID_REG[7:0]</a>	—	—	—	—	REV_ID[3:0]			
0x02	<a href="#">ISET_REG[7:0]</a>	—	—	—	—	BSTFOR CE	FAST_S S	ENA	PSEN
0x03	<a href="#">IMODE_REG[7:0]</a>	LO_DIM 4	LO_DIM 3	LO_DIM 2	LO_DIM 1	DIM_EX T	HDIM	HDIM_THR_1_0[1:0]	
0x04	<a href="#">ADIM_REG[7:0]</a>	ADIM[7:0]							
0x05	<a href="#">TON1H_REG[7:0]</a>	TON1H[7:0]							
0x06	<a href="#">TON1L_REG[7:0]</a>	TON1L[7:0]							
0x07	<a href="#">TON2H_REG[7:0]</a>	TON2H[7:0]							
0x08	<a href="#">TON2L_REG[7:0]</a>	TON2L[7:0]							
0x09	<a href="#">TON3H_REG[7:0]</a>	TON3H[7:0]							
0x0A	<a href="#">TON3L_REG[7:0]</a>	TON3L[7:0]							
0x0B	<a href="#">TON4H_REG[7:0]</a>	TON4H[7:0]							
0x0C	<a href="#">TON4L_REG[7:0]</a>	TON4L[7:0]							
0x0D	<a href="#">TON1_4LSB_REG[7:0]</a>	TON4LSB[1:0]		TON3LSB[1:0]		TON2LSB[1:0]		TON1LSB[1:0]	
0x0E	<a href="#">SETTING_REG[7:0]</a>	—	FPWM[2:0]			SS_OFF	SSL	SLDET[1:0]	
0x0F	<a href="#">DISABLE_REG[7:0]</a>	—	—	CP_DIS	—	DIS4	DIS3	DIS2	DIS1
0x10	<a href="#">FADING_REG[7:0]</a>	—	—	—	FADE_G AIN	FADE_I N_OUT	TDIM[2:0]		
0x11	<a href="#">OPEN_REG[7:0]</a>	—	—	—	—	OUT4O	OUT3O	OUT2O	OUT1O
0x12	<a href="#">SHORTGND_REG[7:0]</a>	—	—	—	—	OUT4SG	OUT3SG	OUT2SG	OUT1SG
0x13	<a href="#">SHORTED_LED_REG[7:0]</a>	—	—	—	—	OUT4SL	OUT3SL	OUT2SL	OUT1SL
0x14	<a href="#">MASK_REG[7:0]</a>	—	—	—	BSTUVM ASK	OMASK	SGMAS K	OTWMA SK	SLMASK
0x15	<a href="#">DIAG_REG[7:0]</a>	RTOOR	—	ISETOO R	BSTUV	BSTOV	HW_RS T	OTW	OT

## Register Details

[DEV\\_ID\\_REG \(0x00\)](#)

BIT	7	6	5	4	3	2	1	0
Field	DEV_ID[7:0]							
Reset	0x28							
Access Type	Read Only							
BITFIELD		BITS		DESCRIPTION				
DEV_ID		7:0		Device ID 0x28.				

[REV\\_ID\\_REG \(0x01\)](#)

BIT	7	6	5	4	3	2	1	0
Field	–	–	–	–	REV_ID[3:0]			
Reset	–	–	–	–	0x02			
Access Type	–	–	–	–	Read Only			

BITFIELD	BITS	DESCRIPTION
REV_ID	3:0	Device revision ID.

[ISSET\\_REG \(0x02\)](#)

BIT	7	6	5	4	3	2	1	0
Field	–	–	–	–	BSTFORCE	FAST_SS	ENA	PSEN
Reset	–	–	–	–	0x0	0x0	0b0	0b1
Access Type	–	–	–	–	Write, Read	Write, Read	Write, Read	Write, Read

BITFIELD	BITS	DESCRIPTION
BSTFORCE	3	When 1, this bit forces the boost converter to run continuously and independent of the dimming signal.
FAST_SS	2	Selects slow or fast boost soft-start. Set to 1 for fast soft-start.
ENA	1	Boost converter and LED outputs enable bit. Set to 1 to enable the device.
PSEN	0	When 0, phase shifting is disabled. When 1, phase shifting is enabled.

[IMODE\\_REG \(0x03\)](#)

BIT	7	6	5	4	3	2	1	0
Field	LO_DIM4	LO_DIM3	LO_DIM2	LO_DIM1	DIM_EXT	HDIM	HDIM_THR_1_0[1:0]	
Reset	0x0	0x0	0x0	0x0	0b1	0b0	0b00	
Access Type	Read Only	Read Only	Read Only	Read Only	Write, Read	Write, Read	Write, Read	

BITFIELD	BITS	DESCRIPTION
LO_DIM4	7	When 1, indicates channel 4 is in low-dim mode.
LO_DIM3	6	When 1, indicates channel 3 is in low-dim mode.
LO_DIM2	5	When 1, indicates channel 2 is in low-dim mode.
LO_DIM1	4	When 1, indicates channel 1 is in low-dim mode.
DIM_EXT	3	When 1, dimming through the DIM pin is enabled. When 0, dimming is controlled using the TON__ registers.
HDIM	2	When 1, hybrid dimming is enabled. Default value is 0.
HDIM_THR_1_0	1:0	Set hybrid dimming threshold.
		00 6.25%
		10 12.5%
		10 25%
		11 50%

[ADIM\\_REG \(0x04\)](#)

BIT	7	6	5	4	3	2	1	0
Field	ADIM[7:0]							
Reset	0xFF							
Access Type	Write, Read							

BITFIELD	BITS	DESCRIPTION
ADIM	7:0	8-bit linear analog dimming value. 0xFF is full-scale current, and each bit represents a current step of 0.4%.

[TON1H\\_REG \(0x05\)](#)

On-time setting for channel 1 with 50ns resolution, high byte.

BIT	7	6	5	4	3	2	1	0
Field	TON1H[7:0]							
Reset	0xFF							
Access Type	Write, Read							

BITFIELD	BITS	DESCRIPTION
TON1H	7:0	High byte of 18-bit TON setting for channel 1.

[TON1L\\_REG \(0x06\)](#)

On-time setting for channel 1 with 50ns resolution, middle byte.

BIT	7	6	5	4	3	2	1	0
Field	TON1L[7:0]							
Reset	0xFF							
Access Type	Write, Read							

BITFIELD	BITS	DESCRIPTION
TON1L	7:0	Middle byte of 18-bit TON setting for channel 1.

[TON2H\\_REG \(0x07\)](#)

On-time setting for channel 2 with 50ns resolution2, high byte.

BIT	7	6	5	4	3	2	1	0
Field	TON2H[7:0]							
Reset	0xFF							
Access Type	Write, Read							

BITFIELD	BITS	DESCRIPTION
TON2H	7:0	High byte of 18-bit TON setting for channel 2.

[TON2L\\_REG \(0x08\)](#)

On-time setting for channel 2 with 50ns resolution, middle byte.

BIT	7	6	5	4	3	2	1	0
Field	TON2L[7:0]							
Reset	0xFF							
Access Type	Write, Read							
BITFIELD		BITS		DESCRIPTION				
TON2L		7:0		Middle byte of 18-bit TON setting for channel 2.				

[TON3H\\_REG \(0x09\)](#)

On-time setting for channel 3 with 50ns resolution, high byte.

BIT	7	6	5	4	3	2	1	0
Field	TON3H[7:0]							
Reset	0xFF							
Access Type	Write, Read							
BITFIELD		BITS		DESCRIPTION				
TON3H		7:0		High byte of 18-bit TON setting for channel 3.				

[TON3L\\_REG \(0x0A\)](#)

On-time setting for channel 3 with 50ns resolution, middle byte.

BIT	7	6	5	4	3	2	1	0
Field	TON3L[7:0]							
Reset	0xFF							
Access Type	Write, Read							
BITFIELD		BITS		DESCRIPTION				
TON3L		7:0		Middle byte of 18-bit TON setting for channel 3.				

[TON4H\\_REG \(0x0B\)](#)

On-time setting for channel 4 with 50ns resolution, high byte.

BIT	7	6	5	4	3	2	1	0
Field	TON4H[7:0]							
Reset	0xFF							
Access Type	Write, Read							
BITFIELD		BITS		DESCRIPTION				
TON4H		7:0		High byte of 18-bit TON setting for channel 4.				

[TON4L\\_REG \(0x0C\)](#)

On-time setting for channel 4 with 50ns resolution, middle byte.

BIT	7	6	5	4	3	2	1	0
Field	TON4L[7:0]							
Reset	0xFF							
Access Type	Write, Read							

BITFIELD	BITS	DESCRIPTION
TON4L	7:0	Middle byte of 18-bit TON setting for channel 4.

**TON1\_4LSB\_REG (0x0D)**

LSBs of on-time setting for all channels with 50ns resolution.

BIT	7	6	5	4	3	2	1	0
Field	TON4LSB[1:0]		TON3LSB[1:0]		TON2LSB[1:0]		TON1LSB[1:0]	
Reset	0b11		0b11		0b11		0b11	
Access Type	Write, Read		Write, Read		Write, Read		Write, Read	

BITFIELD	BITS	DESCRIPTION
TON4LSB	7:6	2 least significant bits of 18-bit TON setting for channel 4.
TON3LSB	5:4	2 least significant bits of 18-bit TON setting for channel 3.
TON2LSB	3:2	2 least significant bits of 18-bit TON setting for channel 2.
TON1LSB	1:0	2 least significant bits of 18-bit TON setting for channel 1.

**SETTING\_REG (0x0E)**

BIT	7	6	5	4	3	2	1	0
Field	–	FPWM[2:0]			SS_OFF	SSL	SLDET[1:0]	
Reset	–	0b001			0b0	0b0	0b00	
Access Type	–	Write, Read			Write, Read	Write, Read	Write, Read	

BITFIELD	BITS	DESCRIPTION																																				
FPWM	6:4	These bits set the PWM frequency in internal PWM mode.																																				
		<table><tr><th>FPWM2</th><th>FPWM1</th><th>FPWM0</th><th>PWM FREQUENCY (Hz)</th></tr><tr><td>0</td><td>0</td><td>0</td><td>153</td></tr><tr><td>0</td><td>0</td><td>1</td><td>203</td></tr><tr><td>0</td><td>1</td><td>0</td><td>305</td></tr><tr><td>0</td><td>1</td><td>1</td><td>610</td></tr><tr><td>1</td><td>0</td><td>0</td><td>980</td></tr><tr><td>1</td><td>0</td><td>1</td><td>1220</td></tr><tr><td>1</td><td>1</td><td>0</td><td>1401</td></tr><tr><td>1</td><td>1</td><td>1</td><td>1634</td></tr></table>	FPWM2	FPWM1	FPWM0	PWM FREQUENCY (Hz)	0	0	0	153	0	0	1	203	0	1	0	305	0	1	1	610	1	0	0	980	1	0	1	1220	1	1	0	1401	1	1	1	1634
		FPWM2	FPWM1	FPWM0	PWM FREQUENCY (Hz)																																	
		0	0	0	153																																	
		0	0	1	203																																	
		0	1	0	305																																	
		0	1	1	610																																	
		1	0	0	980																																	
		1	0	1	1220																																	
		1	1	0	1401																																	
1	1	1	1634																																			
SS_OFF	3	When 1, spread-spectrum switching is disabled. Default value is 0.																																				



BITFIELD	BITS	DESCRIPTION
SSL	2	When spread spectrum is enabled, the SSL bit chooses the amount of spread. When 0, the spread is nominally $\pm 6\%$ . When 1, the spread is $\pm 4\%$ . When changing the percentage, disable spread-spectrum using the SS_OFF bit first. Then, change the value of SSL. Finally, re-enable spread spectrum using SS_OFF.
SLDET	1:0	Shorted-LED-Threshold Settings.
		00 Disabled
		01 3V
		10 6V
		11 8V

**DISABLE\_REG (0x0F)**

Channel-disable bits.

BIT	7	6	5	4	3	2	1	0
Field	–	–	CP_DIS	–	DIS4	DIS3	DIS2	DIS1
Reset	–	–	0b0	–	0b0	0b0	0b0	0b0
Access Type	–	–	Write, Read	–	Write, Read	Write, Read	Write, Read	Write, Read

BITFIELD	BITS	DESCRIPTION
CP_DIS	5	When 1, this bit disables the internal charge pump, which drives the NGATE pin. Set to 1 when an external series switch is not used. Setting CP_DIS to zero during operation will cause complete shutdown of the device and is not recommended.
DIS4	3	Set bit to 1 to disable OUT4. This must be done before ENA is written to 1.
DIS3	2	Set bit to 1 to disable OUT3. This must be done before ENA is written to 1.
DIS2	1	Set bit to 1 to disable OUT2. This must be done before ENA is written to 1.
DIS1	0	Set bit to 1 to disable OUT1. This must be done before ENA is written to 1.

**FADING\_REG (0x10)**

BIT	7	6	5	4	3	2	1	0
Field	–	–	–	FADE_GAIN	FADE_IN_OUT	TDIM[2:0]		
Reset	–	–	–	0b0	0b0	0b000		
Access Type	–	–	–	Write, Read	Write, Read	Write, Read		

BITFIELD	BITS	DESCRIPTION	DECODE
FADE_GAIN	4	When this bit is set to 1, the fade-in-out function has a gain of 12.5%, otherwise 6.25%	
FADE_IN_OUT	3	When this bit is set to 1, the fade-in-out function for the LED dimming is enabled.	

BITFIELD	BITS	DESCRIPTION	DECODE
TDIM	2:0	Sets the fading update time interval according to 2 <sup>TDIM</sup> . TDIM can be between 0 and 5. When set to 0, fading is updated on every dimming cycle.	0x0: 1 0x1: 2 0x2: 4 0x3: 8 0x4: 16 0x5: 32 0x6: NA 0x7: NA

**OPEN\_REG (0x11)**

Open-string diagnostics.

BIT	7	6	5	4	3	2	1	0
Field	–	–	–	–	OUT4O	OUT3O	OUT2O	OUT1O
Reset	–	–	–	–	0b0	0b0	0b0	0b0
Access Type	–	–	–	–	Read Only	Read Only	Read Only	Read Only

BITFIELD	BITS	DESCRIPTION
OUT4O	3	If 1, an open is detected on channel 4.
OUT3O	2	If 1, an open is detected on channel 3.
OUT2O	1	If 1, an open is detected on channel 2.
OUT1O	0	If 1, an open is detected on channel 1.

**SHORTGND\_REG (0x12)**

Short-to-ground diagnostics.

BIT	7	6	5	4	3	2	1	0
Field	–	–	–	–	OUT4SG	OUT3SG	OUT2SG	OUT1SG
Reset	–	–	–	–	0b0	0b0	0b0	0b0
Access Type	–	–	–	–	Read Only	Read Only	Read Only	Read Only

BITFIELD	BITS	DESCRIPTION
OUT4SG	3	If 1, a short-to-ground is detected on channel 4 at startup.
OUT3SG	2	If 1, a short-to-ground is detected on channel 3 at startup.
OUT2SG	1	If 1, a short-to-ground is detected on channel 2 at startup.
OUT1SG	0	If 1, a short-to-ground is detected on channel 1 at startup.

**SHORTED\_LED\_REG (0x13)**

Shorted-LED diagnostics.

BIT	7	6	5	4	3	2	1	0
Field	–	–	–	–	OUT4SL	OUT3SL	OUT2SL	OUT1SL
Reset	–	–	–	–	0b0	0b0	0b0	0b0
Access Type	–	–	–	–	Read Only	Read Only	Read Only	Read Only

BITFIELD	BITS	DESCRIPTION
OUT4SL	3	If 1, a shorted-LED condition is detected on channel 4.

BITFIELD	BITS	DESCRIPTION
OUT3SL	2	If 1, a shorted-LED condition is detected on channel 3.
OUT2SL	1	If 1, a shorted-LED condition is detected on channel 2.
OUT1SL	0	If 1, a shorted-LED condition is detected on channel 1.

**MASK\_REG (0x14)**

Mask register for the FLTB pin.

BIT	7	6	5	4	3	2	1	0
Field	–	–	–	BSTUVMAS K	OMASK	SGMASK	OTWMASK	SLMASK
Reset	–	–	–	0b0	0b0	0b0	0b1	0b0
Access Type	–	–	–	Write, Read	Write, Read	Write, Read	Write, Read	Write, Read

BITFIELD	BITS	DESCRIPTION
BSTUVMASK	4	When 1, a boost undervoltage fault does not cause the FLTB pin to assert low.
OMASK	3	When 1, an open-LED fault does not cause the FLTB pin to assert low.
SGMASK	2	When 1, a short-to-ground LED fault does not cause the FLTB pin to assert low.
OTWMASK	1	When 1, an overtemperature warning does not cause the FLTB pin to assert low.
SLMASK	0	When 1, a shorted-LED fault does not cause the FLTB pin to assert low.

**DIAG\_REG (0x15)**

Boost state, overtemperature-warning/shutdown diagnostics.

BIT	7	6	5	4	3	2	1	0
Field	RTOOR	–	ISETOOR	BSTUV	BSTOV	HW_RST	OTW	OT
Reset	0b0	–	0b0	0b0	0b0	0b1	0b0	0b0
Access Type	Read Only	–	Read Only	Read Only	Read Only	Read Only	Read Only	Read Only

BITFIELD	BITS	DESCRIPTION
RTOOR	7	This bit is set to 1 if the resistor on the RT pin is out of the expected range. When this happens, the device cannot operate.
ISETOOR	5	When 1, this bit indicates that the ISET current is out of range. This is more than likely due to an incorrect resistor value on ISET. In this condition, the IC stops operation.
BSTUV	4	If 1, an undervoltage is detected on the boost output, and the boost is disabled.
BSTOV	3	If 1, the boost converter is at its overvoltage limit.
HW_RST	2	If 1, the device has just emerged from a hardware reset (power-up). This bit is reset after the first read from this register.
OTW	1	If 1, the junction temperature of the device is over T <sub>WARN</sub> , or the temperature foldback circuit has reached the temperature T <sub>1</sub> .
OT	0	If 1, the junction temperature of the device exceeds T <sub>SHDN</sub> , and the device is shut down.

## Applications Information

### DC-DC Converter

The MAX25512 DC-DC converters offer the capability to work with two different converter topologies that have the ground-referenced outputs necessary to use the constant-current sink drivers. If the LED string forward voltage is always greater than the input supply voltage range, use the boost-converter topology. If the LED string forward voltage falls within the supply voltage range, use the SEPIC topology.

The boost-converter topology provides the highest efficiency of these topologies. The SEPIC configuration requires either two inductors or a coupled inductor and a coupling capacitor.

### Power-Circuit Design

First, select a converter topology based on the factors listed above. Determine the required input supply voltage range, the maximum voltage needed to drive the LED strings including the minimum 0.875V across the constant LED current sink ( $V_{LED}$ ), and the total output current needed to drive the LED strings ( $I_{LED}$ ), as shown in the following equation:

$$I_{LED} = I_{STRING} \times N_{STRING}$$

where  $I_{STRING}$  is the current per string, and  $N_{STRING}$  is the number of strings used.

Next, calculate the maximum duty cycle ( $D_{MAX}$ ) using one of the following equations, depending on the configuration:

#### Boost Configuration:

$$D_{MAX} = \frac{(V_{LED} + V_{D1} - V_{IN\_MIN})}{(V_{LED} + V_{D1} - V_{DS} - 0.3)}$$

#### SEPIC Configuration:

$$D_{MAX} = \frac{V_{LED} + V_{D1}}{(V_{IN\_MIN} - V_{DS} - 0.3 + V_{LED} + V_{D1})}$$

where,

$V_{D1}$  = Forward drop of the rectifier diode in volts (approximately 0.6V)

$V_{IN\_MIN}$  = Minimum input supply voltage

$V_{DS}$  = Drain-to-source voltage of the internal MOSFET when it is on, given by  $I_{LAVG} \times R_{DS(ON)}$  where  $R_{DS(ON)} = 125m\Omega$

Select the switching frequency ( $f_{SW}$ ) depending on space, noise, and efficiency constraints.

### Boost Configuration

In the converter configurations, the average inductor current varies with the input voltage; the maximum average current occurs at the lowest input voltage. For the boost converter, the average inductor current is equal to the input current. Select the maximum peak-to-peak ripple on the inductor current ( $\Delta I_L$ ). The recommended maximum peak-to-peak ripple is 60% of the average inductor current, but lower and higher ripple values are also acceptable.

Use the following equations to calculate the maximum average inductor current ( $I_{LAVG}$ ) and peak inductor current ( $I_{LP}$ ) in amps (A).

$$I_{LAVG} = \frac{I_{LED}}{(1 - D_{MAX})}$$

Allowing the peak-to-peak inductor ripple ( $\Delta I_L$ ) to be  $\pm 30\%$  of the average inductor current:

$$\Delta I_L = I_{LAVG} \times 0.3 \times 2$$

and:

$$I_{LP} = I_{LAVG} + \frac{\Delta I_L}{2}$$

Calculate the minimum inductance value ( $L_{MIN}$ ) in henries (H) with the inductor current ripple set to the maximum value:

$$L_{MIN} = \frac{(V_{IN\_MIN} - V_{DS} - 0.3) \times D_{MAX}}{f_{SW} \times \Delta IL}$$

where  $V_{DS}$  is  $IL_{AVG} \times 0.125$ . Choose an inductor with a minimum inductance greater than the calculated  $L_{MIN}$  and current rating greater than  $IL_P$ . The recommended saturation current limit of the selected inductor is 10% higher than the inductor peak current.

### SEPIC Configuration

Power-circuit design for the SEPIC configuration is very similar to a conventional design with the output voltage referenced to the input supply voltage. For SEPIC, the output is referenced to ground and the inductor is split into two parts. One of the inductors ( $L_2$ ) takes LED current as the average current, and the other ( $L_1$ ) takes input current as the average current.

Use the following equations to calculate the average inductor currents ( $IL_{1AVG}$ ,  $IL_{2AVG}$ ) and peak inductor currents ( $IL_{1P}$ ,  $IL_{2P}$ ) in A.

$$IL_{1AVG} = \frac{I_{LED} \times D_{MAX} \times 1.1}{1 - D_{MAX}}$$

The factor 1.1 provides a margin of 10% to account for the converter losses.

$$IL_{2AVG} = I_{LED}$$

Assuming the peak-to-peak inductor ripple  $\Delta IL$  is  $\pm 30\%$  of the average inductor current:

$$\Delta IL_1 = IL_{1AVG} \times 0.3 \times 2$$

and:

$$IL_{1P} = IL_{1AVG} + \frac{\Delta IL_1}{2}$$

and:

$$\Delta IL_2 = IL_{2AVG} \times 0.3 \times 2$$

and:

$$IL_{2P} = IL_{2AVG} + \frac{\Delta IL_2}{2}$$

Calculate the minimum inductance values ( $L_{1MIN}$  and  $L_{2MIN}$ ) in H with the inductor current ripple set to the values previously calculated.

$$L_{1MIN} = \frac{(V_{IN\_MIN} - V_{DS} - 0.3) \times D_{MAX}}{f_{SW} \times \Delta IL_1}$$

$$L_{2MIN} = \frac{(V_{IN\_MIN} - V_{DS} - 0.3) \times D_{MAX}}{f_{SW} \times \Delta IL_2}$$

Choose inductors with a minimum inductance greater than the calculated  $L_{1MIN}$  and  $L_{2MIN}$  and current ratings of greater than  $IL_{1P}$  and  $IL_{2P}$ , respectively. The recommended saturation current limit of the selected inductor is 10% higher than the inductor peak current.

To simplify further calculations, consider a single inductor equivalent to  $L_1$  and  $L_2$  connected in parallel. The combined inductance value and current is calculated as follows:

$$L = \frac{L_1 \times L_2}{L_1 + L_2}$$

and:

$$IL_{AVG} = IL_{1AVG} + IL_{2AVG}$$

where  $IL_{AVG}$  represents the total average current through both of the inductors in the SEPIC configuration. Use these

values in the calculations in the following sections.

Select coupling-capacitor  $C_S$  so that its peak-to-peak ripple is less than 2% of the minimum input supply voltage. This ensures that the second-order effects created by the series-resonant circuit comprising  $L_1$ ,  $C_S$ , and  $L_2$  do not affect the normal operation of the converter. Use the following equation to calculate the minimum value of  $C_S$ :

$$C_S = \frac{I_{LED} \times D_{MAX}}{V_{IN\_MIN} \times 0.02 \times f_{SW}}$$

where,

$C_S$  = Minimum value of the coupling capacitor in farads (F)

0.02 = 2% ripple factor

### Output Capacitor Selection

The output capacitor supplies the load current when the main switch is on. The function of the output capacitor is to reduce the converter output ripple to acceptable levels. The entire output-voltage ripple appears across the constant-current sink outputs because the LED-string voltages are stable due to the constant current. For the MAX25512, limit peak-to-peak output-voltage ripple to 250mV to get stable output current.

The equivalent series resistance (ESR), equivalent series inductance (ESL), and bulk capacitance of the output capacitor contribute to the output ripple. In most applications, using low-ESR ceramic capacitors can dramatically reduce the output ESR and ESL effects. To reduce this, connect multiple ceramic capacitors in parallel to achieve the required bulk capacitance. To minimize audible noise during PWM dimming, the amount of ceramic capacitors on the output is usually minimized. In this case, an additional electrolytic or aluminum organic polymer capacitor can provide most of the bulk capacitance.

### Rectifier Diode Selection

Using a Schottky rectifier diode produces less forward drop and puts the least burden on the MOSFET during reverse recovery. Select a diode with low reverse-recovery losses to reduce the MOSFET switching losses and avoid increased EMI. The voltage rating of the diode should be 20% higher than the maximum boost-converter output voltage and its current rating greater than the following:

$$I_{L\_AVG} \times (1 - D_{MAX}) \times 1.2$$

### Feedback Compensation

During normal operation, the feedback control loop regulates the minimum  $OUT\_$  voltage to fall within the window comparator limits of  $V_{OUTL}$  and  $V_{OUTH}$  when LED string currents are enabled during PWM dimming. When LED currents are off during PWM dimming, the control loop turns off the converter (when  $BSTFORCE = 0$ ) and stores the previous boost output-voltage value for use during the next on cycle.

The switching converter small-signal-transfer function has a right-half plane (RHP) zero in the boost configuration if the inductor current is in continuous-conduction mode. The RHP zero adds a 20dB/decade gain together with a 90° phase lag, which is difficult to compensate.

**Worst-Case RHP Zero Frequency ( $f_{ZRHP}$ ):**

$$f_{ZRHP} = \frac{V_{LED} \times (1 - D_{MAX})^2}{2 \times \pi \times L \times I_{LED}}$$

**SEPIC Configuration:**

$$f_{ZRHP} = \frac{V_{LED} \times (1 - D_{MAX})^2}{2 \times \pi \times L \times I_{LED} \times D_{MAX}}$$

The standard way to avoid this zero is to roll off the loop gain to 0dB at a frequency of less than 1/5 of the RHP zero frequency with a -20dB/decade slope.

The switching converter small-signal transfer function also has an output pole. The effective output impedance, together

with the output filter capacitance, determines the output pole frequency ( $f_{P1}$ ) that is calculated for the boost configuration, as shown in the following equation:

$$f_{P1} = \frac{I_{LED}}{\pi \times V_{LED} \times C_{OUT}}$$

#### SEPIC Configuration:

$$f_{P1} = \frac{I_{LED} \times D_{MAX}}{\pi \times V_{LED} \times C_{OUT}}$$

Compensation components  $R_{COMP}$  and  $C_{COMP}$  perform two functions.  $C_{COMP}$  introduces a low-frequency pole that presents a -20dB/decade slope to the loop gain.  $R_{COMP}$  flattens the gain of the error amplifier for frequencies above the zero formed by  $R_{COMP}$  and  $C_{COMP}$ . For compensation, this zero is placed at  $f_{P1}$  to provide a -20dB/decade slope for frequencies above  $f_{P1}$  to the combined modulator and compensator response.

The value of  $R_{COMP}$  needed to fix the total loop gain at  $f_{P1}$  so the total loop gain crosses 0dB with -20dB/decade slope at 1/5 the RHP zero frequency is calculated for the boost configuration as follows:

$$R_{COMP} = \frac{f_{ZRHP} \times R_{CS} \times I_{LED} \times A_{OVP}}{5 \times f_{P1} \times GM_{COMP} \times V_{LED} \times (1 - D_{MAX})}$$

#### SEPIC Configuration:

$$R_{COMP} = \frac{f_{ZRHP} \times R_{CS} \times I_{LED} \times A_{OVP} \times D_{MAX}}{5 \times f_{P1} \times GM_{COMP} \times V_{LED} \times (1 - D_{MAX})}$$

where,

$R_{COMP}$  = Compensation resistor in  $\Omega$

$A_{OVP}$  = BSTMON resistor-divider gain (a value  $\gg 1$ )

$R_{CS}$  = Current-sense resistor of value 0.066 $\Omega$

$GM_{COMP}$  = Transconductance of the error amplifier (600 $\mu$ S)

The value of  $C_{COMP}$  is calculated as follows:

$$C_{COMP} = \frac{1}{2 \times \pi \times f_{Z1} \times R_{COMP}}$$

where  $f_{Z1}$  is the compensation zero placed at 1/5 the crossover frequency; in turn, it is set at 1/5 the  $f_{ZRHP}$ . If the output capacitors do not have low ESR, the ESR zero frequency can fall below the 0dB crossover frequency. An additional pole may be required to cancel out this zero placed at the same frequency. This can be added by connecting a capacitor from the COMP pin directly to GND with a value shown as follows:

$$C_{PAR} = GM_{COMP} \times R_{ESR} \times C_{OUT}$$

where,

$R_{ESR}$  = Capacitor ESR value

$C_{OUT}$  = Output-capacitor value

### External Disconnect MOSFET Selection

An external nMOSFET can be used to disconnect the boost output from the battery in the event of an output overload or short condition. There is no need for the nMOSFET in the case of the SEPIC or buck-boost, since this protection is not necessary. Leave the NGATE pin disconnected when an external nMOSFET is not used. If it is necessary to have output-short protection for the boost even at power-up, then the current through the nMOSFET must be sensed (refer to the MAX25512 evaluation kit (EV kit) for a reference circuit). Once the current-sense voltage exceeds a certain threshold, it should limit the input current to the programmed threshold. This threshold should be set at a sufficiently high level so it never trips at startup or under normal operating conditions. Check the safe operating area (SOA) of the nMOSFET to confirm that the current-limit-trip threshold and voltage on the MOSFET do not exceed the limits of the SOA curve of the nMOSFET at the highest operating temperature.

Ensure that the maximum value of the nMOSFET gate threshold voltage is lower than 4V for reliable operation.

### V<sub>OUT</sub> to OUT<sub>\_</sub> Bleed Resistors

The OUT<sub>\_</sub> pins have a leakage specification of 4μA (max) in cases where all OUT<sub>\_</sub> pins are shorted to 36V (see I<sub>OUTLEAK</sub> in the [Electrical Characteristics](#) table). This leakage current is dependent on the OUT<sub>\_</sub> voltage and is higher at higher voltages. Therefore, in cases where large numbers of LEDs are connected in series, a 100kΩ (or larger) bleed resistor can be placed in parallel with the LED string to prevent the OUT<sub>\_</sub> leakage current from turning on the LEDs dimly, even when the DIM signal is low (see resistors R8–R11 in the [Typical Application Circuit](#)).

### Thermal Considerations

The on-chip power dissipation of the MAX25512 comprises four main factors:

1. Current-sink power loss =  $0.875V \times I_{LED}$
2. Device operating current power loss =  $V_{IN} \times 1.3mA$
3. Power due to R<sub>DS(ON)</sub> of the internal MOSFET =  $BoostDutyCycle \times I_{LAVG}^2 \times 0.125$
4. Power due to switching losses in the internal MOSFET =  $0.5 \times V_{LED} \times I_{LED} \times t_{R/F} \times f_{SW}$  where  $t_{R/F}$  is the rise/fall time of the boost converter switching node approximated to 6ns.

Calculate the total power dissipation by adding the values calculated above. The junction temperature at the maximum ambient temperature can then be calculated as follows:

$$T_J = T_A + P_{TOT} \times \theta_{JA}$$

where,

T<sub>A</sub> = Ambient temperature

θ<sub>JA</sub> = Junction-to-ambient thermal resistance of the package (36°C/W on a four-layer board). Ensure that the junction temperature does not exceed +150°C.

As an example, consider an application with a minimum operating voltage of 9V, a total output current of 400mA at 28.7V and an average 1.5A inductor current. With a switching frequency of 400kHz, the total power dissipation is calculated in the following equation:

$$P_{TOT} = (0.875 \times 0.4) + (9 \times 0.0013) + \left(\frac{28.7}{28.7+9} \times 1.5^2 \times 0.125\right) + (0.5 \times 28.7 \times 0.4 \times 6E-9 \times 400000) = 0.59W$$

The maximum junction temperature at an ambient temperature of +85°C is shown in the following equation:

$$T_J = 85 + 0.59 \times 36 = +106^\circ C$$

### PCB Layout Considerations

LED driver circuits based on the MAX25512 use a high-frequency switching converter to generate the voltage for LED strings. Take proper care while laying out the circuit to ensure correct circuit operation. The switching-converter part of the circuit has nodes with fast voltage changes that can lead to undesirable effects on the sensitive parts of the circuit. Use the following guidelines to reduce noise as much as possible:

- Connect the bypass capacitors on V18 as close as possible to the device. Make the connections directly to the device's V18 and GND pins. Connect the GND pin of the device to the analog ground plane and to the exposed pad of the device. Place the analog ground plane on an inner layer.
- Place a power ground plane for the switching-converter power circuit under the power components (input filter capacitor, output filter capacitor, inductor, and rectifier diode). Connect the PGND pins to the power ground plane and to the exposed pad of the device. Connect all other ground connections to the power ground plane using vias close to the terminals.
- There are two loops in the power circuit that carry high-frequency switching currents. One loop exists when the internal MOSFET is on (from the input filter capacitor positive terminal, through the inductor and internal MOSFET, to the input capacitor negative terminal). The other loop exists when the MOSFET is off (from the input capacitor positive terminal, through the inductor, the rectifier diode, output filter capacitor, to the input capacitor negative terminal). Analyze these two loops in order to make the loop areas as small as possible. Wherever possible, have a return path on the power ground plane for the switching currents on the top-layer copper traces or through power components. This reduces the loop area considerably and provides a low-inductance path for the switching currents. Reducing the loop area also

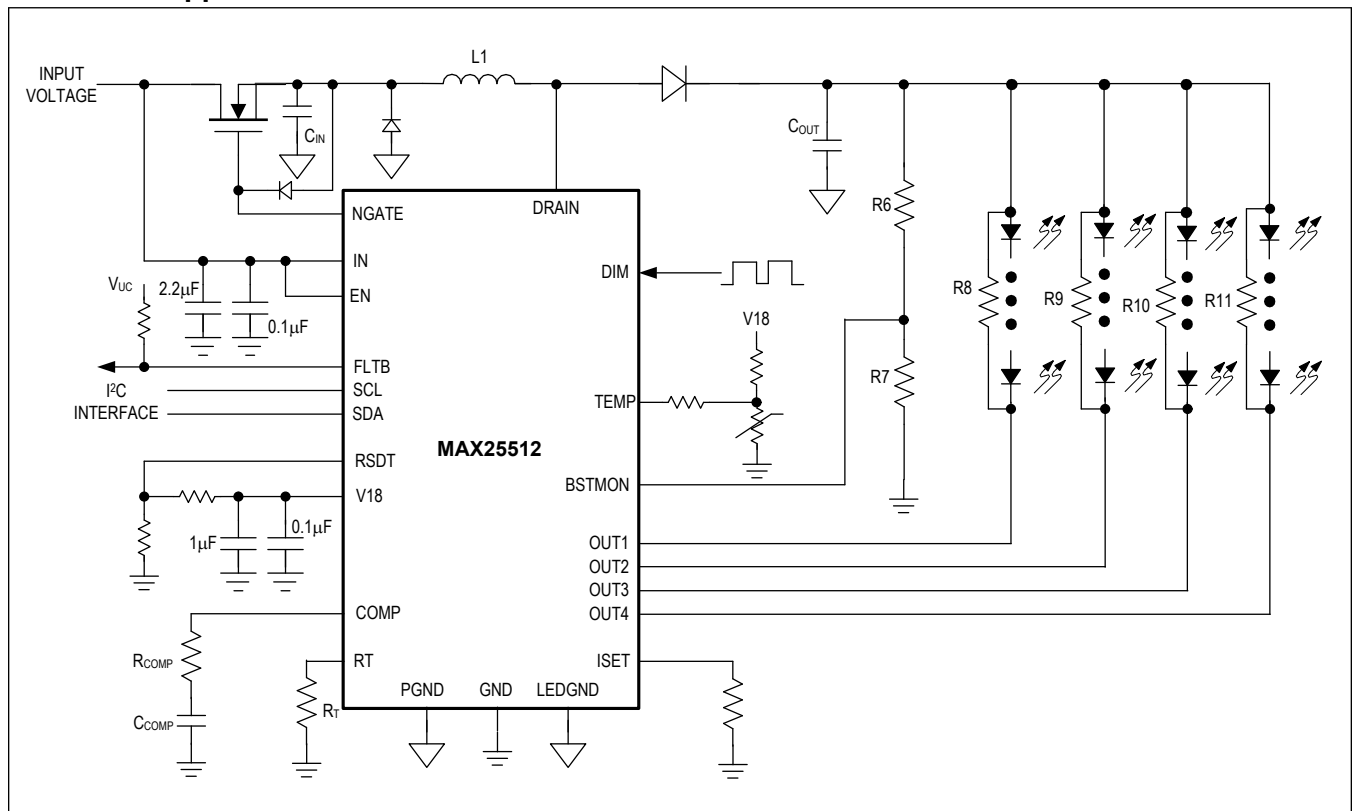


- decreases radiation during switching.
- Connect the power ground plane for the constant-current LED driver part of the circuit to the LEDGND pin. Also connect the LEDGND pin to the device's exposed pad.
- Add a small bypass capacitor (22pF to 47pF) to the BSTMON input. Place the capacitor as close as possible to the pin to suppress high-frequency noise.
- Boost output voltage for the LED strings must be taken directly from the output capacitors and not from the boost diode anode.
- Input and output capacitors need good grounding with wide traces and multiple vias to the ground plane.
- To enhance device power dissipation, add multiple vias under the device's exposed pad connected to an area of copper on the backside of the PCB. This is important for maintaining device efficiency and reducing junction temperature during operation.

Refer to the EV kit for a reference layout.

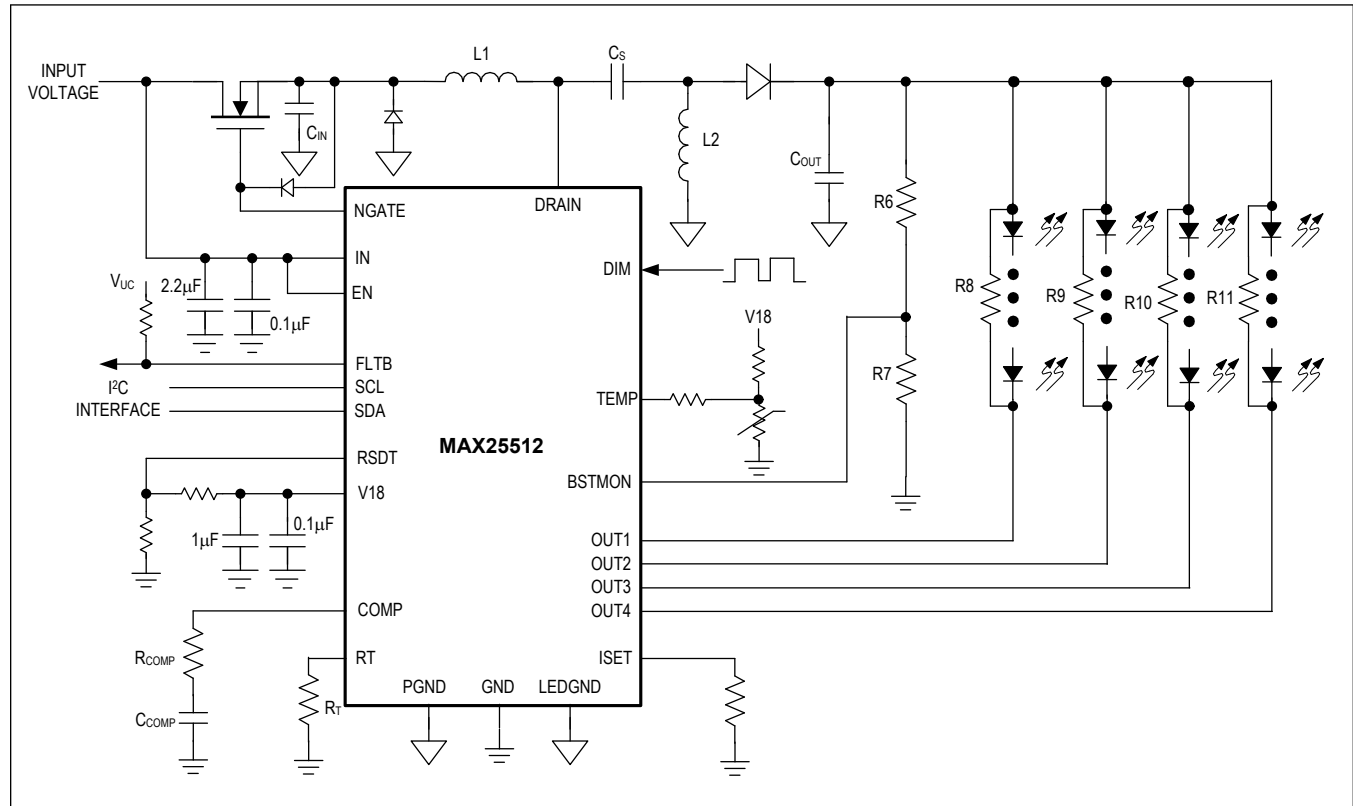
## Typical Application Circuits

### MAX25512 Application Circuit



I<sup>2</sup>C-Controlled 4-Channel Low-Voltage 120mA  
LED Backlight Driver with Integrated Boost  
Converter

## MAX25512 Application Circuit - SEPIC



PART NUMBER	TEMPERATURE RANGE	PIN-PACKAGE
MAX25512ATG/V+	-40°C to +125°C	24 TQFN-EP*

+ Denotes a lead(Pb)-free/RoHS-compliant package.

\*EP = Exposed pad.

*Y = Side-wettable (SW) package.*

MAX25512

# I<sup>2</sup>C-Controlled 4-Channel Low-Voltage 120mA LED Backlight Driver with Integrated Boost Converter

## Revision History

REVISION NUMBER	REVISION DATE	DESCRIPTION	PAGES CHANGED
0	8/21	Initial release	—
1	6/22	Corrected soft-start equations and TEMP resistor values in <i>Detailed Description</i> ; clarified power calculation in <i>Applications Information</i>	23, 26, 29

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