



AC/DC Converter
Non-Isolation Buck Converter
PWM method 12 W 15 V
BM2P151X Reference Board

<High Voltage Safety Precautions>

◇ Read all safety precautions before use

Please note that this document covers only the BM2P151X evaluation board (BM2P151X-EVK-001) and its functions. For additional information, please refer to the datasheet.

To ensure safe operation, please carefully read all precautions before handling the evaluation board



Depending on the configuration of the board and voltages used,

Potentially lethal voltages may be generated.

Therefore, please make sure to read and observe all safety precautions described in the red box below.

Before Use

- [1] Verify that the parts/components are not damaged or missing (i.e. due to the drops).
- [2] Check that there are no conductive foreign objects on the board.
- [3] Be careful when performing soldering on the module and/or evaluation board to ensure that solder splash does not occur.
- [4] Check that there is no condensation or water droplets on the circuit board.

During Use

- [5] Be careful to not allow conductive objects to come into contact with the board.
- [6] **Brief accidental contact or even bringing your hand close to the board may result in discharge and lead to severe injury or death.**

Therefore, DO NOT touch the board with your bare hands or bring them too close to the board.

In addition, as mentioned above please exercise extreme caution when using conductive tools such as tweezers and screwdrivers.

- [7] If used under conditions beyond its rated voltage, it may cause defects such as short-circuit or, depending on the circumstances, explosion or other permanent damages.
- [8] Be sure to wear insulated gloves when handling is required during operation.

After Use

- [9] The ROHM Evaluation Board contains the circuits which store the high voltage. Since it stores the charges even after the connected power circuits are cut, please discharge the electricity after using it, and please deal with it after confirming such electric discharge.
- [10] Protect against electric shocks by wearing insulated gloves when handling.

This evaluation board is intended for use only in research and development facilities and should be handled **only by qualified personnel familiar with all safety and operating procedures.**

We recommend carrying out operation in a safe environment that includes the use of high voltage signage at all entrances, safety interlocks, and protective glasses.

AC/DC Converter

Non-Isolation Buck Converter PWM method Output 12 W 15 V

BM2P151X Reference Board

BM2P151X-EVK-001

The BM2P151X-EVK-001 evaluation board outputs 15 V voltage from the input of 90 Vac to 264 Vac. The output current supplies up to 0.8 A. The BM2P151X which is PWM method DC/DC converter IC built-in 650 V MOSFET is used. The BM2P151X contributes to low power consumption by built-in a 650 V starting circuit. Built-in current detection resistor realizes compact power supply design. Current mode control imposes current limitation on every cycle, providing superior performance in bandwidth and transient response. The switching frequency is 65 kHz in fixed mode. At light load, frequency is reduced and high efficiency is realized. Built-in frequency hopping function contributes to low EMI. Low on-resistance 1.5 Ω 650 V MOSFET built-in contributes to low power consumption and easy design.



Figure.1 BM2P151X-EVK-001

Electronics Characteristics

Not guarantee the characteristics, is representative value.

Unless otherwise noted : $V_{IN} = 230 \text{ Vac}$, $I_{OUT} = 0.5 \text{ A}$, $T_a: 25 \text{ }^{\circ}\text{C}$

Parameter	Min	Typ	Max	Units	Conditions
Input Voltage Range	90	230	264	Vac	
Input Frequency	47	50/60	63	Hz	
Output Voltage	13.5	15.0	16.5	V	
Maximum Output Power	-	-	12.0	W	$I_{OUT} = 0.8 \text{ A}$
Output Current Range ^(NOTE1)	0.0	0.5	0.8	A	
Stand-by Power	-	150	-	mW	$I_{OUT} = 0 \text{ A}$
Efficiency	-	83.7	-	%	
Output Ripple Voltage ^(NOTE2)	-	70	-	mVpp	
Operating Temperature Range	-10	+25	+65	$^{\circ}\text{C}$	

(NOTE1) Please adjust operating time, within any parts surface temperature under 105 $^{\circ}\text{C}$

(NOTE2) Not include spike noise

Operation Procedure

1. Operation Equipment

- (1) AC Power supply 90 Vac~264 Vac, over 20W
- (2) Electronic Load capacity 0.8 A
- (3) Multi meter

2. Connect method

- (1) AC power supply presetting range 90~264 Vac, Output switch is off.
- (2) Load setting under 0.8 A. Load switch is off.
- (3) AC power supply N terminal connect to the board AC (N) of CN1, and L terminal connect to AC(L).
- (4) Load + terminal connect to VOUT, GND terminal connect to GND terminal
- (5) AC power meter connect between AC power supply and board.
- (6) Output test equipment connects to output terminal
- (7) AC power supply switch ON.
- (8) Check that output voltage is 15 V.
- (9) Electronic load switch ON
- (10) Check output voltage drop by load connect wire resistance



CN1 : from the top ①:AC (L), ②:AC (N)

Figure 2. Connection Circuit

Deleting

Maximum Output Power P_o of this reference board is 12.0 W. The derating curve is shown on the right. If ambient temperature is over 40°C, Please adjust load continuous time by over 105 °C of any parts surface temperature.

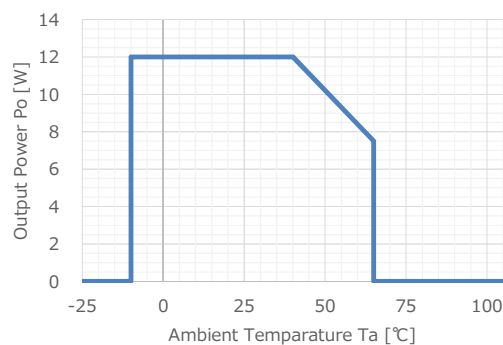


Figure 3. Temperature Deleting curve

Application Circuit

$V_{IN} = 90 \sim 264 \text{ Vac}$, $V_{OUT} = 15 \text{ V}$

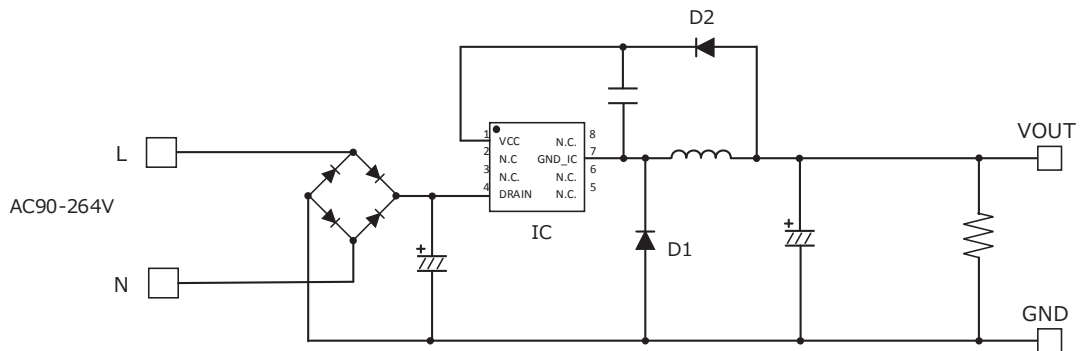


Figure 4. BM2P151X-EVK-001 Application Circuit

The BM2P151X is non-insulation method without opto-coupler and feeds back the VCC voltage to 15.0 V typ. This VCC voltage is the voltage between the VCC pin and the GND_IC pin.

The output voltage VOUT is defined by the following equation.

$$V_{OUT} = V_{CNT} + V_{FD2} - V_{FD1}$$

V_{CNT} : VCC Control Voltage

V_{FD1} : Forward Voltage of diode D1

V_{FD2} : Forward Voltage of diode D2

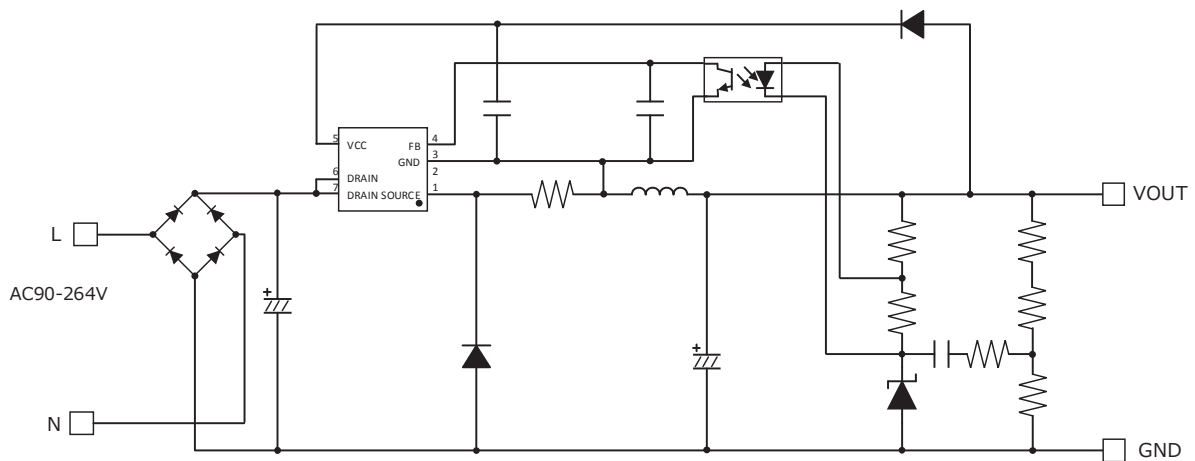


Figure 5. General Buck converter application circuit

Compared to the general Buck converter as shown above, the number of parts is reduced because the feedback circuit is not required. However, the output voltage may rise at light load because the VCC voltage and the output voltage that are fed back are different. In that case, please put a resistance on the output terminal and lower the output voltage.

BM2P151X Overview

Feature

- PWM Frequency=65 kHz
- PWM current mode control
- Switching frequency jitter
- Burst function around light load
- 650 V Starter
- 650 V Super-Junction Power MOSFET
- VCC Under voltage detection
- VCC Over voltage detection
- Cycle by cycle current limiter
- Soft Start function

Key specifications

- Operation Voltage Range: VCC: 12.0 V ~ 16.97 V
DRAI 650 V(Max)
- Circuit Current(ON): 0.85 mA(Typ)
- Circuit Current (Burst mode): 0.45 mA(Typ)
- Switching Frequency: 65 kHz(Typ)
- Operating Temperature: -40 °C ~ +105 °C
- MOSFET R-ON: 1.5 Ω(Typ)

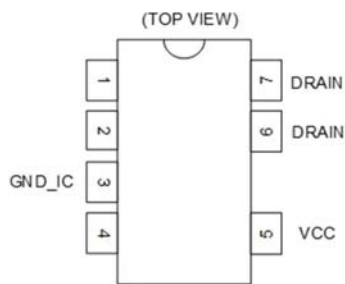


Figure 6. Block Diagram

Dimension

DIP7K

W(Typ) x D(Typ) x H(Max)

9.20 mm x 6.35 mm x 4.30 mm

Pitch 2.54 mm



Figure 7. DIP7K Package

Table 1. BM2P151X PIN description

No.	Name	I/O	Function	ESD Diode	
				VCC	GND
1	-	-	-	-	-
2	-	-	-	-	-
3	GND_IC	I/O	GND	✓	-
4	-	-	-	-	-
5	VCC	I	Vcc	-	✓
6	DRAIN	I/O	MOSEFET DRAIN	-	✓
7	DRAIN	I/O	MOSEFET DRAIN	-	✓

Design Overview

1 Important parameter

- V_{IN} : Input Voltage Range AC 90 V ~ 264 Vac (DC 100 V ~ 380 V)
- V_{OUT} : Output Voltage DC 15 V
- $I_{OUT(Typ)}$: Constant Output Current 0.5 A
- $I_{OUT(Max)}$: Maximum Output Current 0.8 A
- f_{SW} : Switching Frequency Min:60 kHz, Typ:65 kHz, Max:70 kHz
- $I_{peak(Min)}$: Over Current Detection Current Min:1.8 A, Typ:2.0 A, Max:2.2A

2 Coil Selection

2.1 Determining Coil Inductance

The switching operation mode determines the L value so that it becomes as discontinuous mode (DCM) as possible. In the continuous mode (CCM), reverse current in trr of the diode flows, which leads to an increase in power loss of diode. Furthermore, this reverse current becomes the peak current when the MOSFET is ON, and the power loss of the MOSFET also increases. The constant load current I_{OUT} (Typ): 0.5 A, the peak current I_L flowing through the inductor is:

$$I_L = I_{OUT(Typ)} \times 2 = 1.0 \quad [A]$$

It tends to be in continuous mode (CCM) when the input voltage drops.

Calculate with input voltage minimum voltage 100 Vdc with 20% margin and $V_{IN}(\text{Min}) = 80$ Vdc.

From the output voltage V_{OUT} : 15 V and the diode V_F : 1 V, Calculate the maximum value of Duty: Duty (Max).

$$\text{Duty(max)} = \frac{V_{OUT} + V_F}{V_{IN}(\text{Min})} = 0.2$$

From the minimum switching frequency $f_{SW}(\text{Min}) = 60$ kHz, Calculate on time $t_{on}(\text{Max})$

$$t_{on}(\text{Max}) = \frac{\text{Duty(Max)}}{f_{SW}(\text{Min})} = 3.33 \quad [\mu\text{sec}]$$

Calculate L value to operate in discontinuous mode.

$$L < t_{on}(\text{Max}) \times \frac{V_{IN}(\text{Min}) - V_o}{I_L} = 216.5 \quad [\mu\text{H}]$$

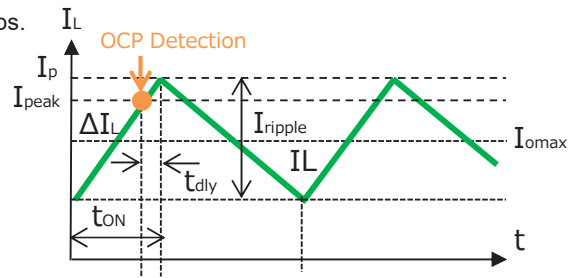


Figure 8. Coil current waveform at OCP detection

2.1 Determining Coil Inductance – Continued

Also, calculate L value so that the overcurrent detection becomes maximum load current I_{OUT} : 800 mA or more. Overcurrent detection is calculated by the current flowing through the MOSFET when operating in continuous mode at the minimum switching frequency f_{SW} (Min) = 60 kHz. When the current flowing through the MOSFET ($\neq$ the coil current at switching ON) exceeds the minimum value I_{peak} (Min): 1.8 A of the overcurrent detection current, the MOSFET is turned OFF. Since a delay of approximately $tdly = 0.1 \mu\text{sec}$ occurs, in reality, the peak current exceeds the I_{peak} value and the peak current becomes I_p . The peak current I_p is obtained by setting the current slope at switching ON to ΔI_L ,

$$I_p = I_{peak} + \Delta I_L \times tdly$$

$$I_p = I_{peak} + \frac{V_{IN} - V_O}{L} \times tdly$$

Calculate the output current I_O (LIM) at overcurrent detection by securing a margin of 10% from the maximum load current of 800 mA, and setting it as 880 mA.

$$I_{OUT}(LIM) = I_p - \frac{I_{ripple}}{2} > I_{OUT}(Max)$$

Calculate the minimum value of the L value of the coil. From the above formula,

$$L > \frac{\{2 \times tdly \times f_{SW}(Min) - (V_{OUT} + V_F)\} \times (V_{IN}(Min) - V_{OUT})}{2 \times f_{SW}(Min) \times (I_{OUT}(Max) - I_{peak}(Min)) \times V_{IN}(Min)} = 123.1 \quad [\mu\text{H}]$$

Therefore, the inductance value of the coil is discontinuous mode when the rated current I_O (Typ) is 0.5 A, and in order to detect the overcurrent of the maximum load current I_O (Max): 0.8 A or more, the condition of 123.1 μH to 216.5 μH , A coil of 150 μH is selected.

2.2 Inductor Current Calculation

Calculate the maximum peak current of the inductor. The condition where the peak current is maximized is when the input voltage is the maximum voltage V_{IN} (Max): 380 V, the maximum load current I_O (Max): 0.8 A, and the switching frequency is 60 kHz at the minimum. The ripple current I_{ripple} of the coil is given by the following formula.

$$I_{ripple} = \frac{di}{dt} \times t_{ON} = \frac{\{V_{IN}(Max) - (V_{OUT} + V_F)\}}{L} \times \frac{(V_{OUT} + V_F)}{V_{IN}(Max) \times f_{SW}(Min)}$$

2.2 Inductor Current Calculation -Continued

When it is applied to the formula of the peak current,

$$I_p = I_{OUT}(Max) + \frac{I_{ripple}}{2} = I_O + \frac{\{V_{IN}(Max) - (V_{OUT} + V_F)\}(V_{OUT} + V_F)}{2 \times L \times V_{IN}(Max) \times f_{SW}(Min)} = 1.65 \quad [A]$$

Select a coil with an allowable current of 1.65 A or more.

In this EVK, we use inductance value: 150 µH, rated: 1.9 A product.

Radial inductor (closed magnetic circuit type) Core size DR09 x 11 series

Product: XF1501Y-151

Manufacturer: ALPHA TRANS CO., LTD

〒541-0059 Senbanishi KID Bldg 7F, 4-4-11, Bakurou-machi, Chuo-ku, Osaka

<http://www.alphatrans.jp/>

3 Diode Selection

3.1 Flywheel Diode : D1

Flywheel diode uses fast diode (fast recovery diode). The reverse voltage of the diode is V_{IN} (Max): 380 V when the output voltage at startup is 0 V. Consider the derating and select 600 V diode. The condition where the effective current of the diode is maximized is when the input voltage is the maximum voltage V_{IN} (Max): 380 V, the maximum load current I_O (Max): 0.8 A, and the switching frequency is 60 kHz at the minimum.

$$Duty = \frac{V_{OUT} + V_F}{V_{IN}(Max)} = 4.21 \quad [\%]$$

The average current I_D of the diode is calculated from the peak current I_p : 1.65 A by the following formula

$$I_D(rms) = I_p \times \sqrt{\frac{1-Duty}{3}} = 0.93 \quad [A]$$

Select the rated current of 0.93 A or more.

In fact, we used RFN5BM6S of 5 A / 600 V product as a result of mounting the board and considering the parts temperature.

3.2 VCC Rectifier Diode : D1

Rectifier diodes are used for diodes to supply VCC. The reverse voltage applied to the diode is V_{IN} (Max): 380 V. Consider the derating and select 600 V diode. Since the current flowing to the IC is small enough, we use the 0.2 A / 600 V RRE02VSM6S.

Design Overview – Continued

4 Capacitor Selection

4.1 Input Capacitor : C4

The input capacitor is determined by input voltage V_I and output power P_{OUT} . As a guide, for an input voltage of 90 to 264 Vac, $2 \times P_{OUT}$ [W] μ F. For 176 to 264 Vac, set $1 \times P_{OUT}$ [W] μ F. Since the output power $P_{OUT} = 12$ W, 33 μ F / 450 V is selected at 24 μ F or more.

4.2 VCC Capacitor : C6

The VCC capacitor C6 is required for stable operation of the device and stable feedback of the output voltage. A withstand voltage of 25 V or more is required, and 1.0 μ F to 4.7 μ F is recommended. 2.2 μ F / 50 V is selected.

4.3 Output Capacitor : C7, C8

For the output capacitor, select output voltage V_O of 25 V or more in consideration of derating. For C7 electrolytic capacitors, capacitance, impedance and rated ripple current must be taken into consideration.

The output ripple voltage is a composite waveform generated by electrostatic capacity: C_{out} , impedance: ESR when the ripple component of inductor current: ΔI_L flows into the output capacitor and is expressed by the following formula.

$$\Delta V_{ripple} = \Delta I_L \times \left(\frac{1}{8 \times C_{out} \times f_{sw}} \right) + ESR$$

The inductor ripple current,

$$\Delta I_L = 2 \times \{I_p - I_{OUT(max)}\} = 2 \times (1.65 - 0.8) = 1.70 \quad [A]$$

For this EVK, we use electrostatic capacity: 680 μ F, ESR: 0.049 Ω , and the design value of output ripple voltage is less than 100 mV.

$$\Delta V_{ripple} = \Delta I_L \times \left\{ \left(\frac{1}{8 \times C_{out} \times f_{sw}} \right) + ESR \right\} = 1.70 \times \left\{ \left(\frac{1}{8 \times 680 \mu \times 65k} \right) + 0.049 \right\} = 88.1 \quad [mV]$$

Next, check whether the ripple current of the capacitor satisfies the rated ripple current.

Inductor ripple current RMS conversion,

$$I_L[rms] = \Delta I_L \times \sqrt{\frac{1}{3}} = 0.98 \quad [A]$$

The ripple current of the capacitor,

$$I_C[rms] = \sqrt{I_L^2 - I_{OUT}^2} = \sqrt{0.98^2 - 0.8^2} = 0.57 \quad [A]$$

4.3 Output Capacitor C7, C8 – Continued

Select a rated current of 0.57 A or more.

The output capacitor C7 used a rated ripple current of 1.24 A at 680 μ F / 25 V.

C8 has added a 0.1 μ F ceramic capacitor to reduce switching noise.

5 Resistor Selection

5.1 Discharge Resistor : R1,R2,R3

The resistor is for discharging X - Capacitor (C1). Considering withstand voltage, 3 pcs of chip resistance of ROHM product MCR18 (200 V withstand voltage) are connected in series. 220 k Ω is used in 3 pcs in series so that it becomes 45 V or less after 1 second after turning off the power supply.

5.2 Bleeder Resistor : R4

Because it is indirectly fed back to the output voltage, the output voltage increases at light load. This board uses bleeder resistance for its improvement. Reducing the resistance value improves the rise in the output voltage of the light load, but increases the power loss. 10 k Ω / 0.25 W is used.

6 EMI Filter Selection

As a measure against "Conducted Emission", Input filter is composed of X-Capacitor: C1 and common mode filter LF1.

X-Capacitor uses 0.22 μ F / X 2. The common mode filter uses 13 mH (Min) / 1 A.

As a measure against "Radiated Emission", Input filter is composed of Y-Capacitor: C2, C3 and a common mode filter LF2.

Y - Capacitor uses 2200 pF / Y1 and connects the midpoint to the output capacitor so that high frequency noise is not propagated from the input. Moreover, the common mode filter uses 60 μ H (Min) / 1 A with good characteristics of the 100 MHz band. If "Radiated Emission" does not have a problem in the state that it is loaded in the set, C2, C3, LF2 are unnecessary.

Performance Data

Constant Load Regulation

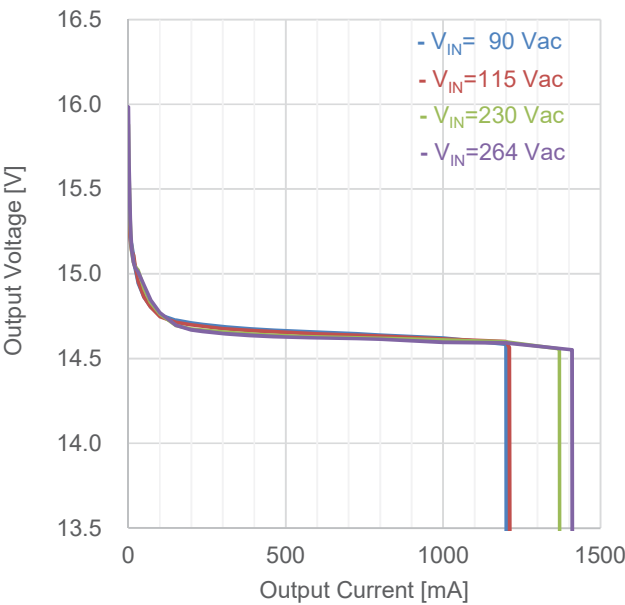


Figure 8. Load Regulation (I_{OUT} vs. V_{OUT})

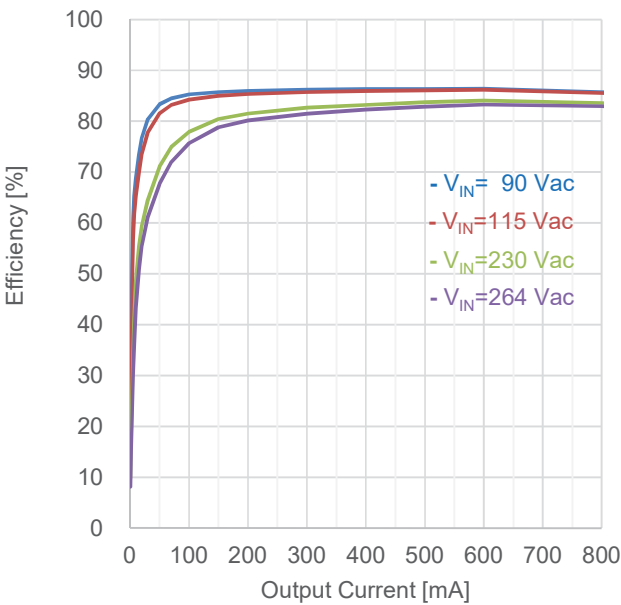


Figure 9. Load Regulation (I_{OUT} vs. Efficiency)

Table 2. Load Regulation ($V_{IN}=115$ Vac)

I_{OUT}	V_{OUT}	Efficiency
200 mA	14.699 V	85.34 %
400 mA	14.663 V	85.92 %
600 mA	14.646 V	86.19 %
800 mA	14.632 V	85.55 %

Table 3. Load Regulation ($V_{IN}=230$ Vac)

I_{OUT}	V_{OUT}	Efficiency
200 mA	14.674 V	81.48 %
400 mA	14.644 V	83.20 %
600 mA	14.628 V	84.07 %
800 mA	14.619 V	83.54 %

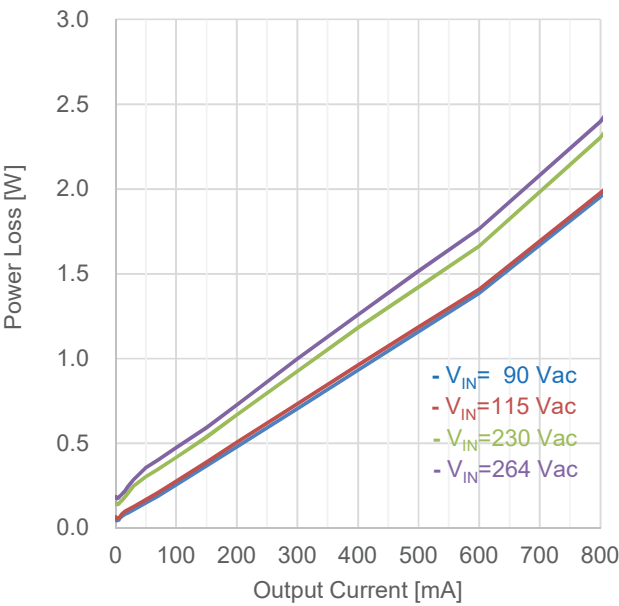


Figure 10. Load Regulation (I_{OUT} vs. P_{LOSS})

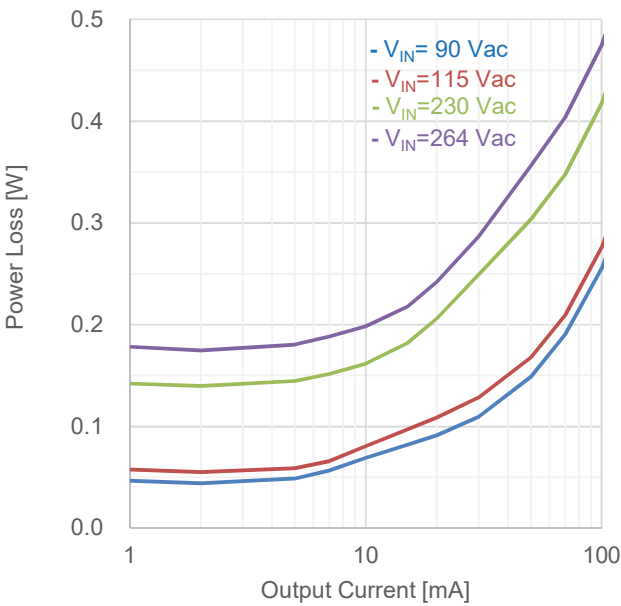


Figure 11. Load Regulation (I_{OUT} vs. P_{LOSS})

Performance Data -Continued

Table 4. Load Regulation : $V_{IN}=90$ Vac

V_{IN} [Vac]	P_{IN} [W]	V_{OUT} [V]	I_{OUT} [mA]	P_{OUT} [W]	P_{LOSS} [W]	Efficiency [%]
90	0.06	15.509	0	0.000	0.055	0.00
90	0.06	15.435	1	0.015	0.047	24.90
90	0.08	15.351	2	0.031	0.044	40.94
90	0.13	15.219	5	0.076	0.049	60.88
90	0.16	15.190	7	0.106	0.057	65.23
90	0.22	15.161	10	0.152	0.069	68.60
90	0.31	15.115	15	0.227	0.082	73.37
90	0.39	15.036	20	0.301	0.091	76.71
90	0.56	14.948	30	0.448	0.110	80.37
90	0.89	14.861	50	0.743	0.149	83.30
90	1.23	14.808	70	1.037	0.190	84.48
90	1.73	14.757	100	1.476	0.255	85.25
90	2.58	14.727	150	2.209	0.368	85.72
90	3.42	14.709	200	2.942	0.480	85.97
90	5.11	14.688	300	4.406	0.705	86.21
90	6.80	14.673	400	5.869	0.932	86.30
90	8.49	14.663	500	7.332	1.160	86.34
90	10.18	14.654	600	8.792	1.387	86.38
90	13.67	14.638	800	11.710	1.955	85.70
90	17.20	14.622	1000	14.622	2.576	85.02
90	20.77	14.585	1200	17.502	3.266	84.27
90	0.07	0.000	1210	0.000	0.070	0.00

Table 5. Load Regulation: $V_{IN}=100$ Vac

V_{IN} [Vac]	P_{IN} [W]	V_{OUT} [V]	I_{OUT} [mA]	P_{OUT} [W]	P_{LOSS} [W]	Efficiency [%]
100	0.06	15.528	0	0.000	0.060	0.00
100	0.07	15.446	1	0.015	0.051	23.40
100	0.08	15.356	2	0.031	0.048	38.88
100	0.13	15.208	5	0.076	0.053	58.95
100	0.17	15.170	7	0.106	0.060	63.97
100	0.23	15.141	10	0.151	0.074	67.29
100	0.32	15.116	15	0.227	0.089	71.75
100	0.40	15.040	20	0.301	0.098	75.39
100	0.57	14.946	30	0.448	0.118	79.22
100	0.90	14.856	50	0.743	0.157	82.53
100	1.24	14.802	70	1.036	0.199	83.90
100	1.74	14.749	100	1.475	0.264	84.81
100	2.59	14.718	150	2.208	0.377	85.40
100	3.43	14.701	200	2.940	0.492	85.67
100	5.12	14.685	300	4.406	0.718	85.99
100	6.81	14.669	400	5.868	0.946	86.11
100	8.50	14.659	500	7.330	1.172	86.22
100	10.19	14.651	600	8.791	1.395	86.30
100	13.67	14.638	800	11.710	1.958	85.68
100	17.20	14.623	1000	14.623	2.581	85.00
100	20.81	14.603	1200	17.524	3.281	84.23
100	20.86	14.579	1210	17.641	3.220	84.56
100	0.08	0.000	1220	0.000	0.083	0.00

Table 6. Load Regulation: $V_{IN}=115$ Vac

V_{IN} [Vac]	P_{IN} [W]	V_{OUT} [V]	I_{OUT} [mA]	P_{OUT} [W]	P_{LOSS} [W]	Efficiency [%]
176	0.11	15.750	0	0.000	0.105	0.00
176	0.11	15.626	1	0.016	0.095	14.08
176	0.12	15.486	2	0.031	0.093	24.98
176	0.17	15.252	5	0.076	0.098	43.83
176	0.21	15.181	7	0.106	0.104	50.60
176	0.27	15.129	10	0.151	0.115	56.88
176	0.36	15.092	15	0.226	0.138	62.19
176	0.46	15.075	20	0.302	0.159	65.54
176	0.64	15.013	30	0.450	0.189	70.48
176	0.98	14.883	50	0.744	0.231	76.32
176	1.31	14.819	70	1.037	0.274	79.13
176	1.82	14.756	100	1.476	0.340	81.26
176	2.67	14.704	150	2.206	0.459	82.76
176	3.52	14.688	200	2.938	0.583	83.43
176	5.23	14.666	300	4.400	0.825	84.21
176	6.93	14.654	400	5.862	1.064	84.63
176	8.62	14.645	500	7.323	1.296	84.97
176	10.31	14.638	600	8.783	1.522	85.23
176	13.86	14.631	800	11.705	2.154	84.46
176	17.51	14.618	1000	14.618	2.890	83.49
176	21.19	14.605	1200	17.526	3.665	82.70
176	22.87	14.582	1290	18.811	4.056	82.26
176	0.17	0.000	1300	0.000	0.173	0.00

Table 7. Load Regulation: $V_{IN}=176$ Vac

V_{IN} [Vac]	P_{IN} [W]	V_{OUT} [V]	I_{OUT} [mA]	P_{OUT} [W]	P_{LOSS} [W]	Efficiency [%]
176	0.11	15.750	0	0.000	0.105	0.00
176	0.11	15.626	1	0.016	0.095	14.08
176	0.12	15.486	2	0.031	0.093	24.98
176	0.17	15.252	5	0.076	0.098	43.83
176	0.21	15.181	7	0.106	0.104	50.60
176	0.27	15.129	10	0.151	0.115	56.88
176	0.36	15.092	15	0.226	0.138	62.19
176	0.46	15.075	20	0.302	0.159	65.54
176	0.64	15.013	30	0.450	0.189	70.48
176	0.98	14.883	50	0.744	0.231	76.32
176	1.31	14.819	70	1.037	0.274	79.13
176	1.82	14.756	100	1.476	0.340	81.26
176	2.67	14.704	150	2.206	0.459	82.76
176	3.52	14.688	200	2.938	0.583	83.43
176	5.23	14.666	300	4.400	0.825	84.21
176	6.93	14.654	400	5.862	1.064	84.63
176	8.62	14.645	500	7.323	1.296	84.97
176	10.31	14.638	600	8.783	1.522	85.23
176	13.86	14.631	800	11.705	2.154	84.46
176	17.51	14.618	1000	14.618	2.890	83.49
176	21.19	14.605	1200	17.526	3.665	82.70
176	22.87	14.582	1290	18.811	4.056	82.26
176	0.17	0.000	1300	0.000	0.173	0.00

Performance Data -Continued

Table 8. Load Regulation : $V_{IN}=230$ Vac

V_{IN} [Vac]	P_{IN} [W]	V_{OUT} [V]	I_{OUT} [mA]	P_{OUT} [W]	P_{LOSS} [W]	Efficiency [%]
230	0.15	15.878	0	0.000	0.151	0.00
230	0.16	15.744	1	0.016	0.142	9.96
230	0.17	15.578	2	0.031	0.140	18.22
230	0.22	15.290	5	0.076	0.145	34.59
230	0.26	15.201	7	0.106	0.152	41.24
230	0.31	15.126	10	0.151	0.162	48.33
230	0.41	15.071	15	0.226	0.182	55.41
230	0.51	15.045	20	0.301	0.206	59.35
230	0.70	15.023	30	0.451	0.249	64.38
230	1.05	14.911	50	0.746	0.303	71.07
230	1.39	14.831	70	1.038	0.348	74.90
230	1.89	14.763	100	1.476	0.418	77.95
230	2.74	14.695	150	2.204	0.537	80.42
230	3.60	14.674	200	2.935	0.667	81.48
230	5.32	14.656	300	4.397	0.925	82.62
230	7.04	14.644	400	5.858	1.182	83.20
230	8.74	14.635	500	7.318	1.423	83.72
230	10.44	14.628	600	8.777	1.663	84.07
230	14.00	14.619	800	11.695	2.305	83.54
230	17.80	14.610	1000	14.610	3.190	82.08
230	21.58	14.597	1200	17.516	4.064	81.17
230	24.98	14.557	1370	19.943	5.037	79.84
230	0.25	0.000	1380	0.000	0.250	0.00

Table 9. Load Regulation: $V_{IN}=264$ Vac

V_{IN} [Vac]	P_{IN} [W]	V_{OUT} [V]	I_{OUT} [mA]	P_{OUT} [W]	P_{LOSS} [W]	Efficiency [%]
264	0.19	15.983	0	0.000	0.187	0.00
264	0.19	15.830	1	0.016	0.178	8.16
264	0.21	15.644	2	0.031	0.175	15.19
264	0.26	15.320	5	0.077	0.180	29.81
264	0.30	15.220	7	0.107	0.188	36.12
264	0.35	15.137	10	0.151	0.199	43.25
264	0.44	15.071	15	0.226	0.218	50.92
264	0.54	15.038	20	0.301	0.242	55.39
264	0.74	15.012	30	0.450	0.287	61.11
264	1.10	14.931	50	0.747	0.356	67.68
264	1.44	14.845	70	1.039	0.404	72.01
264	1.95	14.771	100	1.477	0.475	75.67
264	2.80	14.697	150	2.205	0.594	78.76
264	3.66	14.669	200	2.934	0.727	80.14
264	5.39	14.648	300	4.394	0.998	81.50
264	7.11	14.636	400	5.854	1.259	82.31
264	8.83	14.627	500	7.314	1.517	82.83
264	10.54	14.622	600	8.773	1.767	83.24
264	14.09	14.614	800	11.691	2.399	82.98
264	17.93	14.595	1000	14.595	3.335	81.40
264	21.85	14.593	1200	17.512	4.338	80.14
264	26.07	14.551	1410	20.517	5.553	78.70
264	0.31	0.000	1420	0.000	0.311	0.00

Performance Data -Continued

Line Regulation

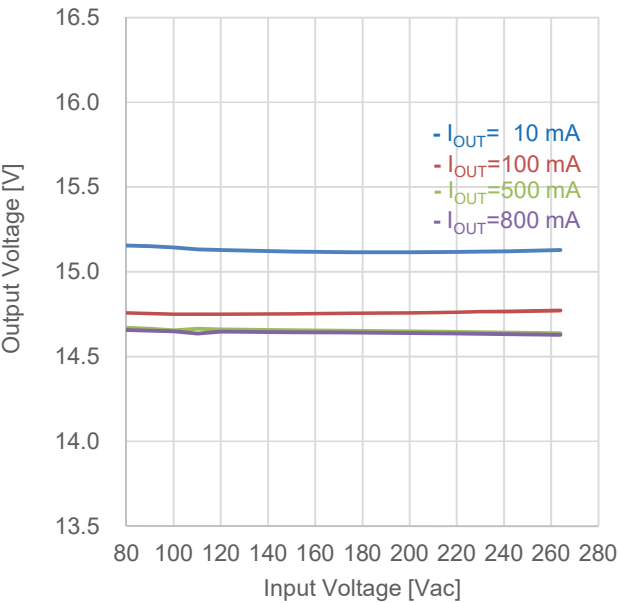


Figure 12. Line Regulation (I_{IN} vs. V_{OUT})

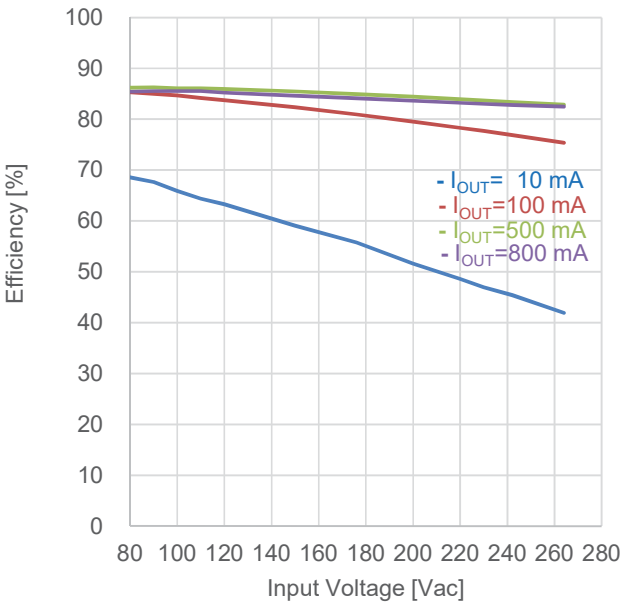


Figure 13. Line Regulation (I_{IN} vs. Efficiency)

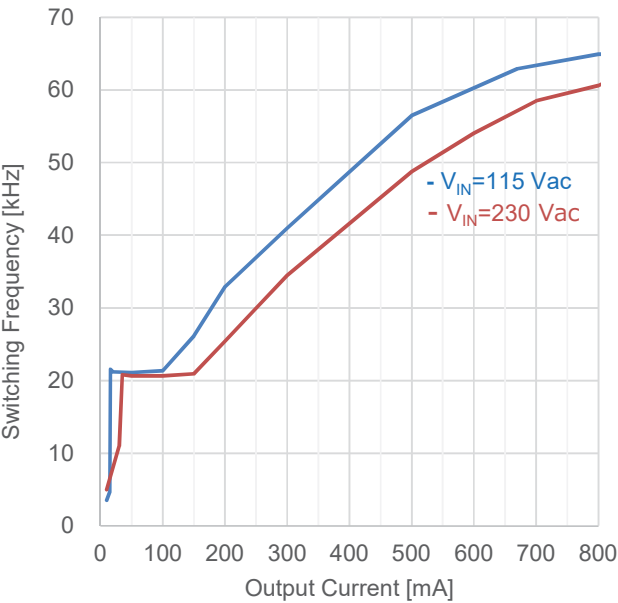


Figure 14. Switching Frequency (I_{OUT} vs. F_{SW})

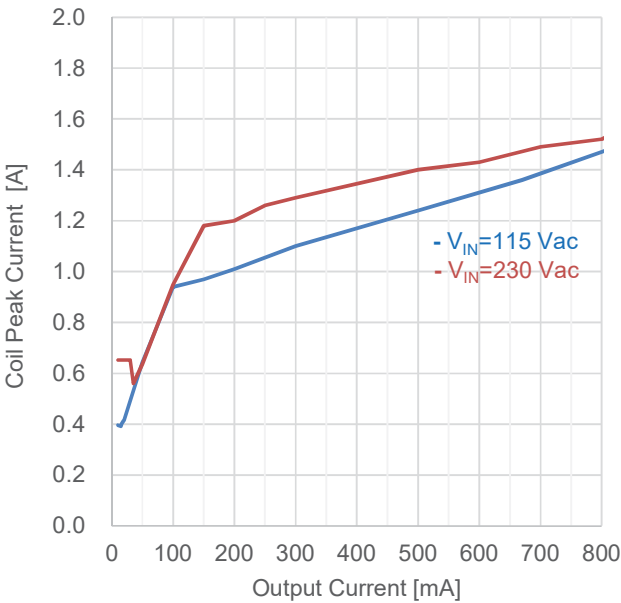


Figure 15. Coil Peak Current (I_{OUT} vs. I_{peak})

Performance Data -Continued

Operation Waveform

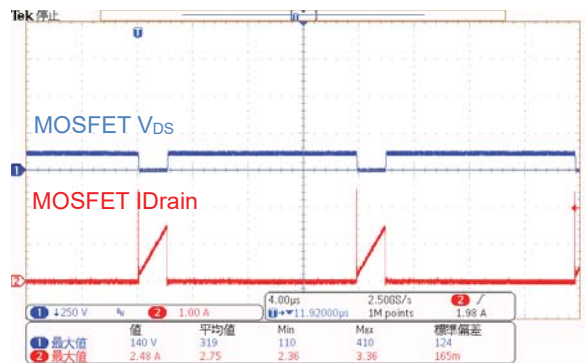


Figure 16. MOSFET $V_{IN} = 90 \text{ Vac}$, $I_{OUT} = 0.8 \text{ A}$

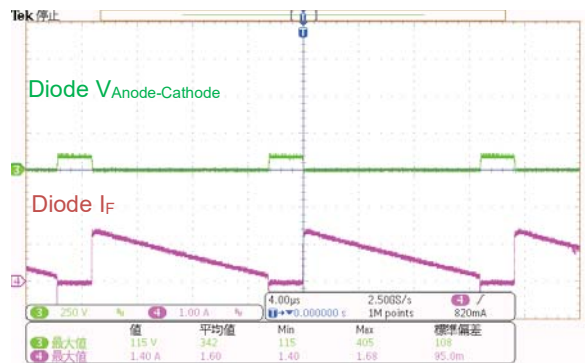


Figure 17. Diode $V_{IN} = 90 \text{ Vac}$, $I_{OUT} = 0.8 \text{ A}$

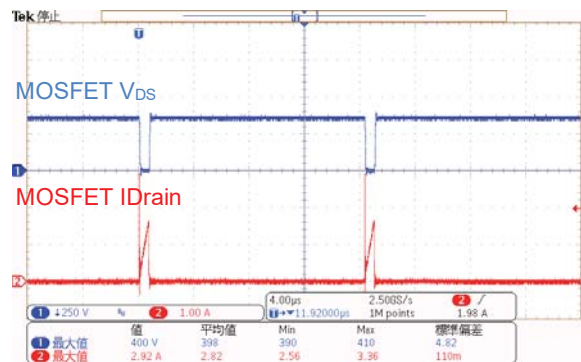


Figure 18. MOSFET $V_{IN} = 264 \text{ Vac}$, $I_{OUT} = 0.8 \text{ A}$

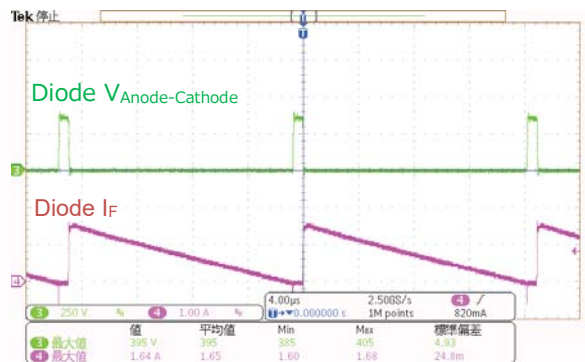


Figure 19. Diode $V_{IN} = 264 \text{ Vac}$, $I_{OUT} = 0.8 \text{ A}$

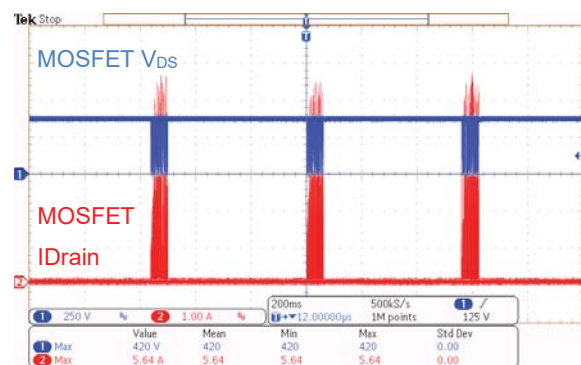


Figure 20. MOSFET $V_{IN} = 264 \text{ Vac}$, Output Short

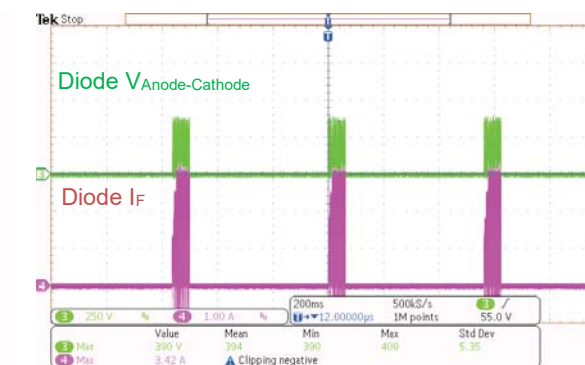


Figure 21. Diode $V_{IN} = 264 \text{ Vac}$, Output Short

Performance Data -Continued

Power ON

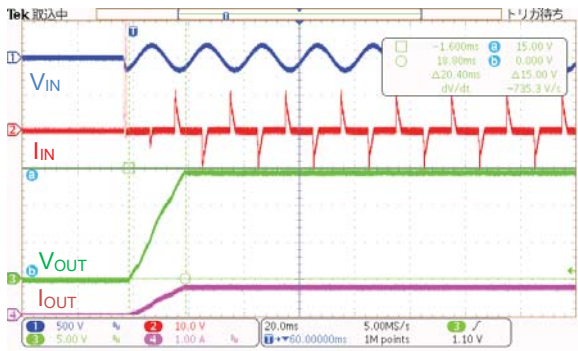


Figure 22. $V_{IN} = 115 \text{ Vac}$, $I_{OUT} = 0.8 \text{ A}$

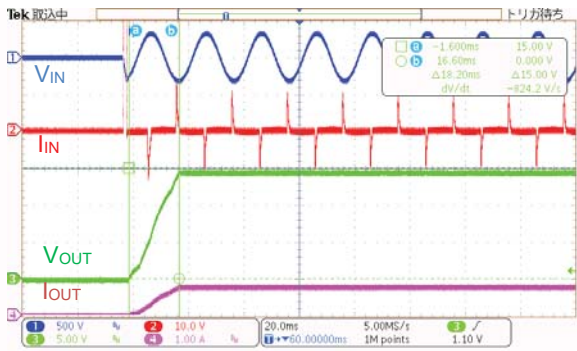


Figure 23. $V_{IN} = 230 \text{ Vac}$, $I_{OUT} = 0.8 \text{ A}$

Dynamic Response

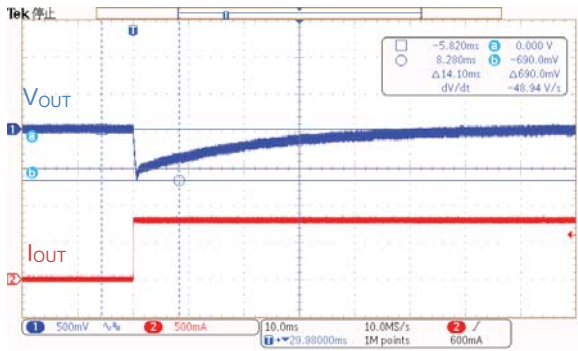


Figure 24. $V_{IN} = 115 \text{ Vac}$, $I_{OUT} = 10 \text{ mA} \rightarrow 0.8 \text{ A}$

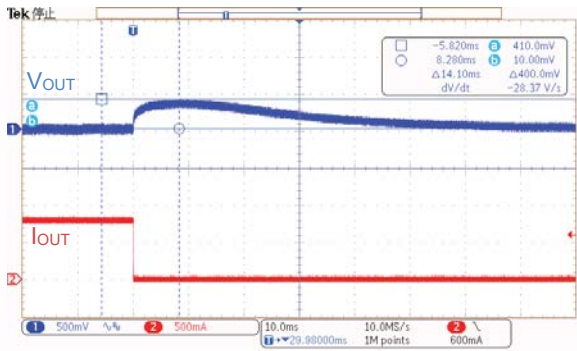


Figure 25. $V_{IN} = 115 \text{ Vac}$, $I_{OUT} = 0.8 \text{ A} \rightarrow 10 \text{ mA}$

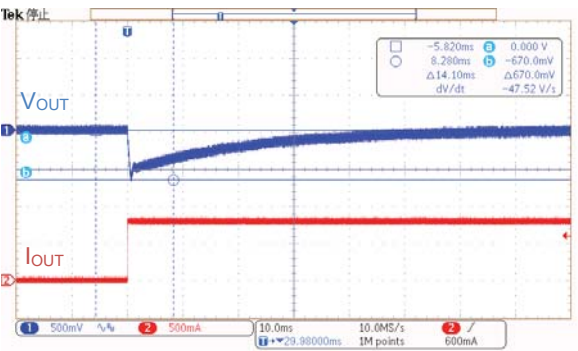


Figure 26. $V_{IN} = 230 \text{ Vac}$, $I_{OUT} = 10 \text{ mA} \rightarrow 0.8 \text{ A}$

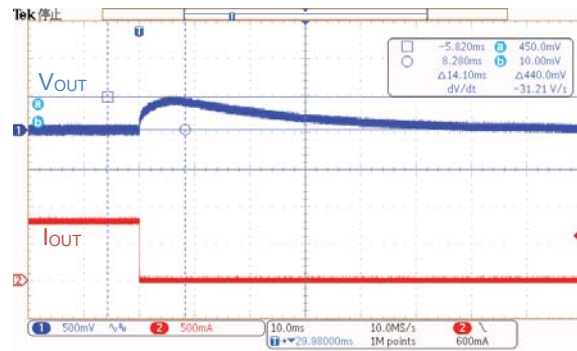
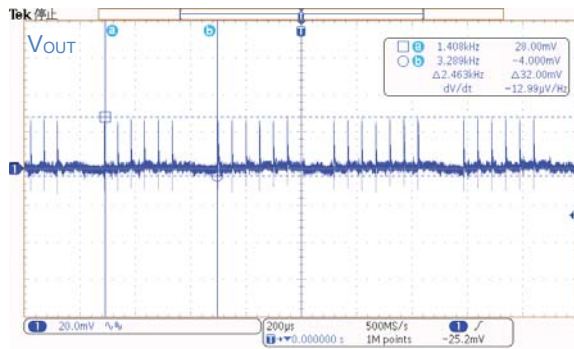
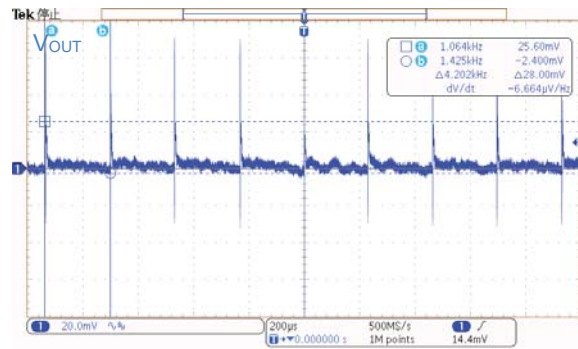
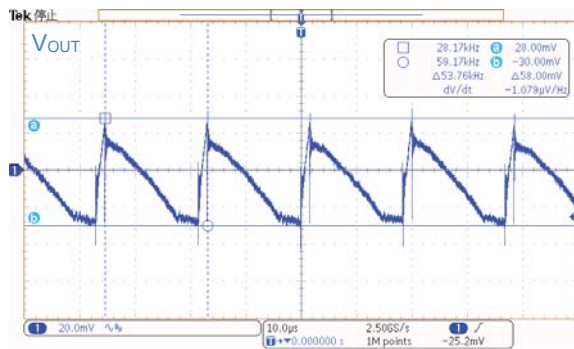
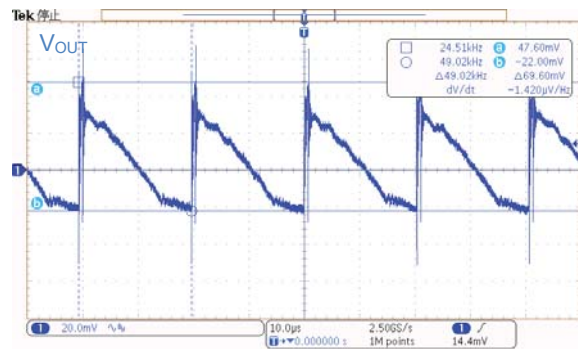
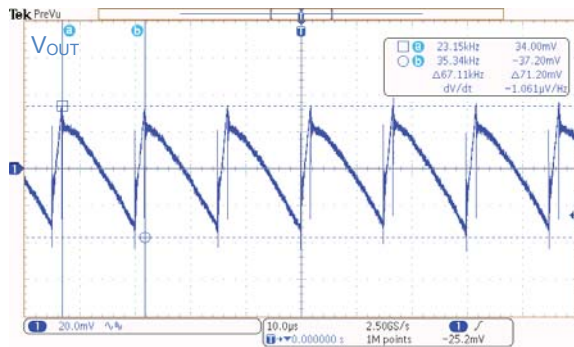
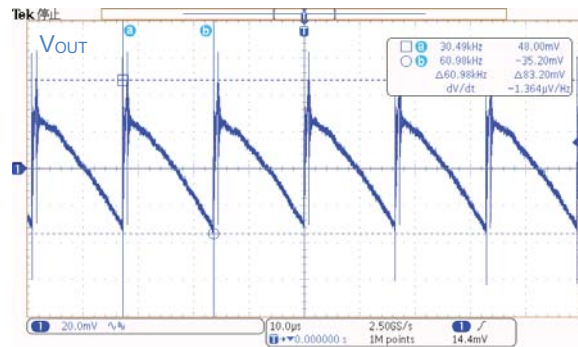


Figure 27. $V_{IN} = 230 \text{ Vac}$, $I_{OUT} = 0.8 \text{ A} \rightarrow 10 \text{ mA}$

Performance Data -Continued

Output Ripple Voltage

Figure 28. $V_{IN} = 115 \text{ Vac}$, $I_{OUT} = 10 \text{ mA}$ Figure 29. $V_{IN} = 230 \text{ Vac}$, $I_{OUT} = 10 \text{ mA}$ Figure 30. $V_{IN} = 115 \text{ Vac}$, $I_{OUT} = 0.5 \text{ A}$ Figure 31. $V_{IN} = 230 \text{ Vac}$, $I_{OUT} = 0.5 \text{ A}$ Figure 32. $V_{IN} = 115 \text{ Vac}$, $I_{OUT} = 0.8 \text{ A}$ Figure 33. $V_{IN} = 230 \text{ Vac}$, $I_{OUT} = 0.8 \text{ A}$

Performance Data -Continued

Parts surface temperature

Table 10. Parts surface temperature

Ta = 25 °C, measured 30 minutes after startup

Part	Condition			
	V _{IN} = 90 Vac, I _{OUT} = 0.50 A	V _{IN} = 90 Vac, I _{OUT} = 0.8 A	V _{IN} = 264 Vac, I _{OUT} = 0.50 A	V _{IN} = 264 Vac, I _{OUT} = 0.8 A
IC1	54.4 °C	76.5 °C	61.5 °C	88.7 °C
D1	60.3 °C	78.6 °C	64.3 °C	85.8 °C
DB1	47.4 °C	56.7 °C	42.2 °C	48.5 °C
L1	57.3 °C	60.7 °C	62.3 °C	77.3 °C

EMI

• Conducted Emission: CISPR22 Pub 22 Class B

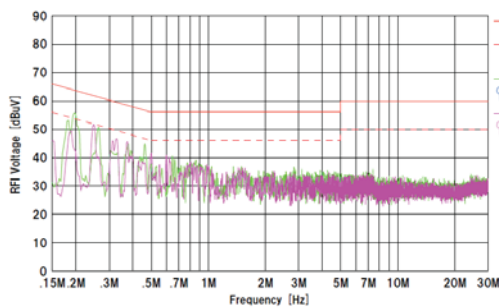


Figure 34. V_{IN} = 110 Vac / 60 Hz, I_{OUT} = 0.8 A
QP margin = 14.0 dB, AV margin = 17.1 dB

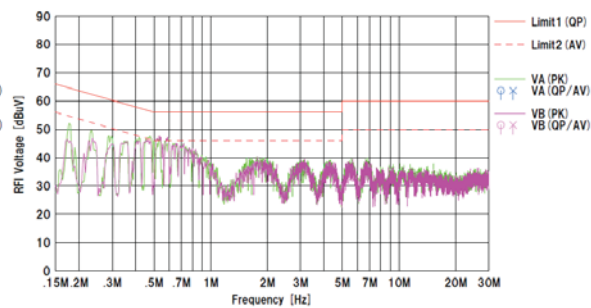


Figure 35. V_{IN} = 230 Vac / 50 Hz, I_{OUT} = 0.8 A
QP margin = 10.4 dB, AV margin = 7.9 dB

• Radiated Emission: CISPR22 Pub 22 Class B

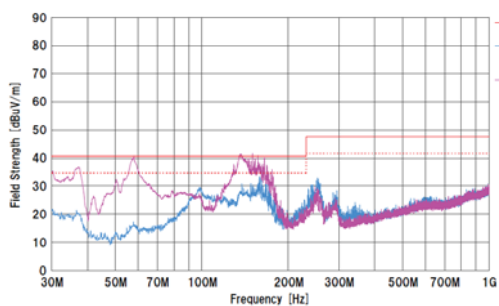


Figure 36. V_{IN} = 110 Vac / 60 Hz, I_{OUT} = 0.8 A
QP margin = 7.3 dB

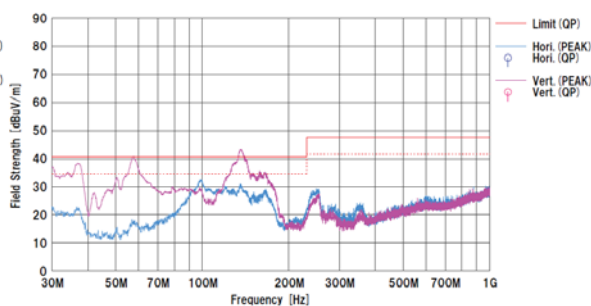


Figure 37. V_{IN} = 230 Vac / 50 Hz, I_{OUT} = 0.8 A
QP margin = 6.2 dB

Schematics

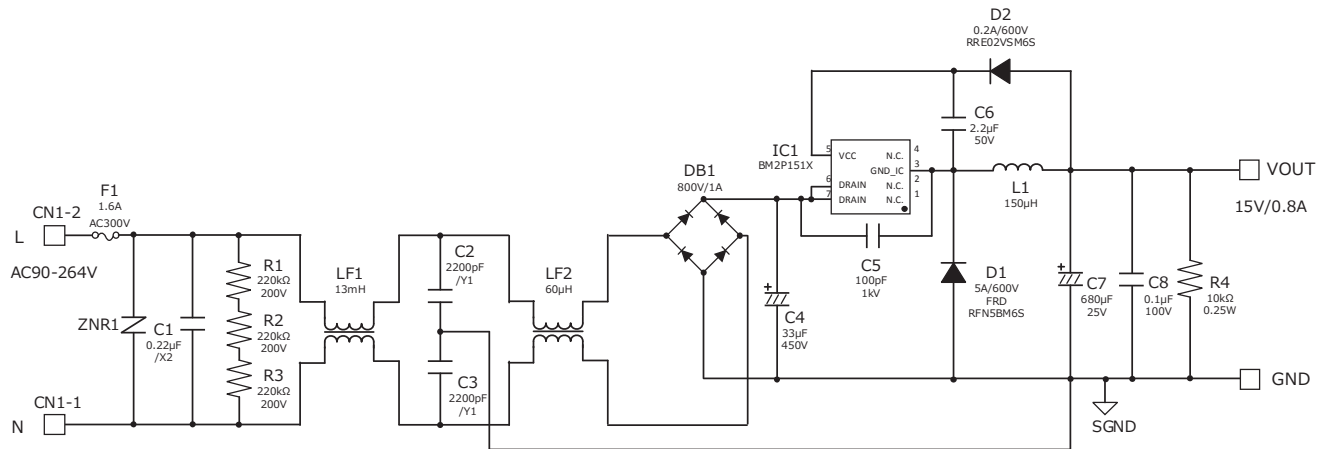
 $V_{IN} = 90 \sim 264 \text{ Vac}$, $V_{OUT} = 15 \text{ V}$


Figure 38. BM2P151X-EVK-001 Schematics

Bill of Materials

Table 11. BoM of BM2P151X-EVK-001

Part Reference	Qty.	Type	Value	Description	Part Number	Manufacture	Configuration mm (inch)
C1	1	X2 Capacitor	0.22μF	275Vac, ±20%	890324023028CS	Wurth	-
C2,C3	2	Y1 Capacitor	2200pF	Y1 capacitor	DE1E3KX222MB4BP01F	Murata	-
C4	1	Electrolytic	33μF	450V, ±20%	450BXW33MEFR12.5X20	Rubycon	12.5mmΦX20mm
C5	1	Ceramic	100pF	1kV, C0G, ±10%	GRM31A5C3A101J	Murata	3216 (1206)
C6	1	Ceramic	2.2μF	50V, X7R, ±10%	UMK316B7225KL-T	Taiyo Yuden	3216 (1206)
C7	1	Electrolytic	680uF	25V, ±20%	UPA1E681MPD	Nichicon	10mmΦX16mm
C8	1	Ceramic	0.1μF	100V, X7R, ±10%	HMK107B7104MA-T	Taiyo Yuden	1608 (0603)
CN1	1	Connector	2pin	5mm pitch	B2P-NV	JST	-
D1	1	FRD	5A	600V	RFN5BM6S	ROHM	TO-252
D2	1	REC Di	0.2A	600V	RRE02VSM6S	ROHM	TUMD2SM
DB1	1	Bridge	1A	800V	D1UBA80	Shindengen	SOP-4
F1	1	Fuse	1.6A	1.6A 300V	36911600000	Littelfuse	-
IC1	1	AC/DC Converter	-	650V	BM2P151X-Z	ROHM	DIP7
JP1	1	Jumper	-	Jumper Wire	-	-	Φ0.5mm
L1	1	Coil	150μH	1.9A	XF1501Y-151	Alpha Trans	-
LF1	1	Line Filter	13mH	1A	XF1482Y	Alpha Trans	-
LF2	1	Line Filter	60μH	1A	LF1246Y	Alpha Trans	-
PCB	1	FR4	-	-	-	-	-
R1,R2,R3	3	Resistor	220kΩ	0.25W, ±5%	MCR18EZPJ224	ROHM	3216 (1206)
R4	1	Resistor	10kΩ	0.25W, ±5%	MCR18EZPJ103	ROHM	3216 (1206)
ZNR1	1	Varistor	-	300Vac, 423Vmin, 400A	V470ZA05P	Littelfuse	5mmΦ Disc

PCB

Size : 91 mm x 30 mm

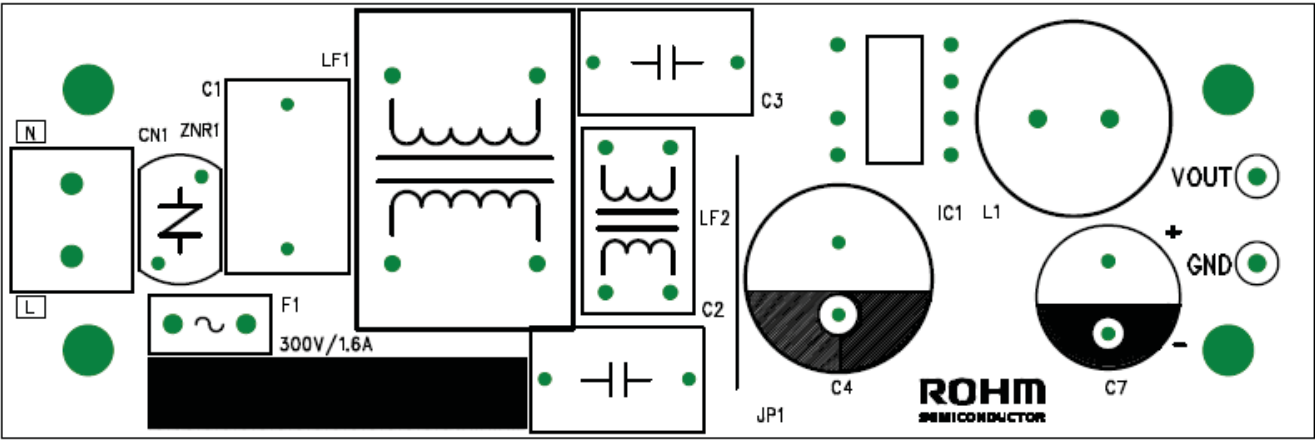


Figure 39. Top Silkscreen (Top view)

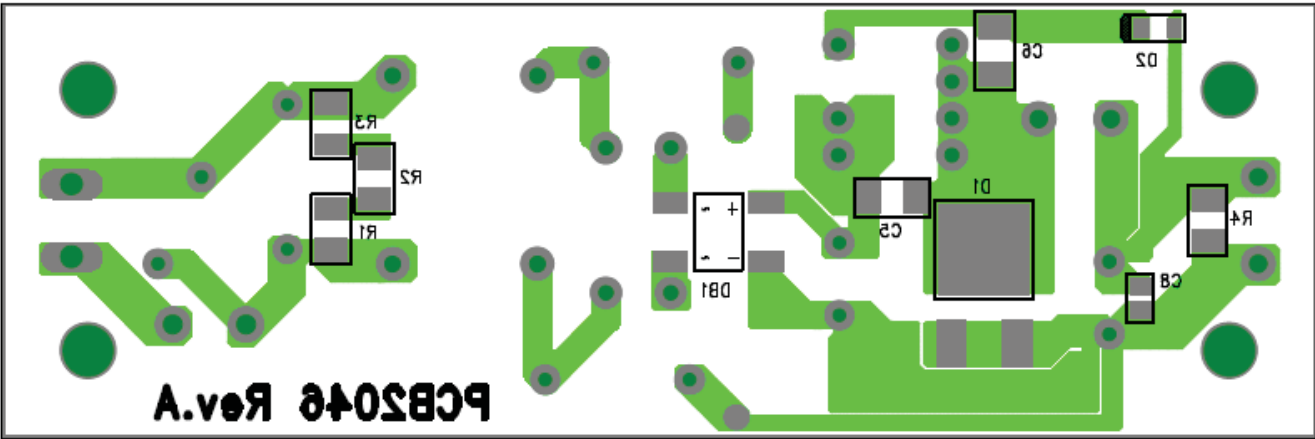


Figure 40. Bottom Layout (Top view)

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