## 28V Internal Switch, Step-Up DC-DC Converter

#### **General Description**

The MAX618 CMOS, PWM, step-up DC-DC converter generates output voltages up to 28V and accepts inputs from +3V to +28V. An internal 2A,  $0.3\Omega$  switch eliminates the need for external power MOSFETs while supplying output currents up to 500mA or more. A PWM control scheme combined with Idle Mode<sup>TM</sup> operation at light loads minimizes noise and ripple while maximizing efficiency over a wide load range. No-load operating current is 500µA, which allows efficiency up to 93%.

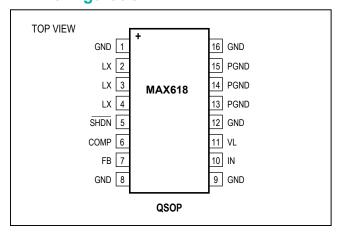
A fast 250kHz switching frequency allows the use of small surface-mount inductors and capacitors. A shutdown mode extends battery life when the device is not in use. Adaptive slope compensation allows the MAX618 to accommodate a wide range of input and output voltages with a simple, single compensation capacitor.

The MAX618 is available in a thermally enhanced 16-pin QSOP package that is the same size as an industry-standard 8-pin SO but dissipates up to 1W. An evaluation kit (MAX618EVKIT) is available to help speed designs.

## **Applications**

- Industrial +24V and +28V Systems
- LCD Displays
- Palmtop Computers

## **Pin Configuration**



Idle Mode is a trademark of Maxim Integrated Products, Inc.

#### **Features**

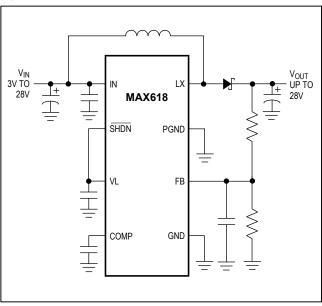
- Adjustable Output Voltage Up to +28V
- Up to 93% Efficiency
- Wide Input Voltage Range (+3V to +28V)
- Up to 500mA Output Current at +12V
- 500µA Quiescent Supply Current
- 3µA Shutdown Current
- 250kHz Switching Frequency
- Small 1W, 16-Pin QSOP Package

## **Ordering Information**

PART	TEMP. RANGE	PIN-PACKAGE
MAX618EEE+	-40°C to +85°C	16 QSOP

<sup>+</sup>Denotes a lead(Pb)-free/RoHS-compliant package.

## **Typical Application Circuit**





## **Absolute Maximum Ratings**

IN to GND	0.3V to +30V
LX to GND	0.3V to +30V
VL to GND	0.3V to +6V
SHDN, COMP, FB to GND	0.3V to (VL + 0.3V)
PGND to GND	±0.3V

) (Note 1)
70°C)1W
40°C to +85°C
+150°C
65°C to +150°C
+260°C

Note 1: With part mounted on 0.9 in.<sup>2</sup> of copper.

Stresses beyond those listed under "Absolute Maximum Ratings" may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated in the operational sections of the specifications is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

#### **Electrical Characteristics**

 $(V_{IN}$  = +6V, PGND = GND,  $C_{VL}$  = 4.7 $\mu$ F,  $T_A$  = 0°C to +85°C, unless otherwise noted. Typical values are at  $T_A$  = +25°C.)

PARAMETER	SYMBOL	CONDITIONS	MIN	TYP	MAX	UNITS
Input Voltage	V <sub>IN</sub>		3		28	V
Supply Current, No Load	I <sub>IN</sub>	V <sub>IN</sub> = 3V to 28V, V <sub>FB</sub> = 1.6V, <del>SHDN</del> = VL		500	700	μA
Supply Current, Full Load, VL Connected to IN	I <sub>IN</sub>	$V_{IN}$ = 3V to 5.5V, $V_{FB}$ = 1.4V, SHDN = VL = IN		5	6.5	mA
Supply Current, Full Load	I <sub>IN</sub>	$V_{IN} = 3.4V \text{ to } 28V, V_{FB} = 1.4V, \\ \overline{\text{SHDN}} = VL, V_{VL} < V_{IN}$		2.5	3.5	mA
Shutdown Supply Current	I <sub>IN</sub>	V <sub>IN</sub> = 28V, V <sub>FB</sub> = 1.6V, <del>SHDN</del> = GND		3	8	μA
VL Output Voltage	$V_{VL}$	V <sub>IN</sub> = 3.5V or 28V, no load	2.9	3.05	3.2	V
VL Load Regulation	$\Delta V_{VL}$	I <sub>LOAD</sub> = 0 to 2mA, V <sub>FB</sub> = 1.6V		25	40	mV
VL Undervoltage Lockout		Rising edge, 1% hysteresis	2.58	2.7	2.8	V
FB Set Voltage	$V_{FB}$		1.47	1.5	1.53	V
FB Input Bias Current	I <sub>FB</sub>	V <sub>FB</sub> = 1.6V		1	50	nA
Line Regulation	$\Delta V_{OUT}$	V <sub>IN</sub> = 3V to 6V,V <sub>OUT</sub> = 12V		0.01	0.08	%/V
Load Regulation	$\Delta V_{OUT}$	V <sub>OUT</sub> = 12V, I <sub>LOAD</sub> = 10mA to 500mA		0.2		%
LX Voltage	$V_{LX}$				28	V
LX Switch Current Limit	I <sub>LXON</sub>	PWM mode	1.7	2.2	2.7	Α
Idle Mode Current Limit Threshold			0.25	0.35	0.45	А
LX On-Resistance	R <sub>LXON</sub>			0.3	0.6	Ω
LX Leakage Current	I <sub>LXOFF</sub>	V <sub>LX</sub> = 28V		0.02	10	μA
COMP Maximum Output Current	I <sub>COMP</sub>	FB = GND	100	200		μA
COMP Voltage to Switch Current Transconductance		ΔFB = 0.1V	0.8	1		mmho
SHDN Input Logic Low	V <sub>IL</sub>				0.8	V
SHDN Input Logic High	V <sub>IH</sub>		2.0			V
Shutdown Input Current		SHDN = GND or VL			1	μA
Switching Frequency	f		200	250	300	kHz
Maximum Duty Cycle	DC		90	95		%

#### **Electrical Characteristics (continued)**

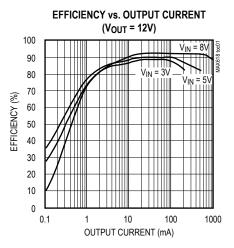
 $(V_{IN}$  = +6V, PGND = GND,  $C_{VL}$  = 4.7 $\mu$ F,  $T_A$  = 0°C to +85°C, unless otherwise noted. Typical values are at  $T_A$  = +25°C.)

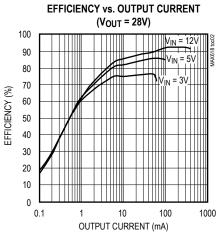
PARAMETER	SYMBOL	CONDITIONS	MIN	TYP	MAX	UNITS
Input Voltage	V <sub>IN</sub>		3		28	V
Supply Current, No Load	I <sub>IN</sub>	$V_{IN}$ = 3V to 28V, $V_{FB}$ = 1.6V, $\overline{SHDN}$ = VL			800	μA
Supply Current, Full Load, VL Connected to IN	I <sub>IN</sub>	$V_{IN} = 3V \text{ to } 5.5, V_{FB} = 1.4V,$ $\overline{SHDN} = VL = IN$			7.5	mA
Supply Current, Full Load	I <sub>IN</sub>	$V_{IN} = 3.4V \text{ to } 28V, V_{FB} = 1.4V, \\ \overline{\text{SHDN}} = VL, V_{VL} < V_{IN}$			4	mA
Supply Current Shutdown	I <sub>IN</sub>	V <sub>IN</sub> = 28V, V <sub>FB</sub> = 1.6V, <del>SHDN</del> = GND			10	μA
VL Output Voltage	$V_{VL}$	V <sub>IN</sub> = 3.5V or 28V, no load	2.85		3.3	V
VL Undervoltage Lockout	$V_{VL}$	Rising edge, 1% hysteresis	2.55		2.85	V
FB Set Voltage	V <sub>FB</sub>		1.455		1.545	V
LX Voltage Range	V <sub>LXON</sub>				28	V
LX Switch Current Limit	I <sub>LXON</sub>	PWM mode	1.4		3	Α
LX On-Resistance	R <sub>LXON</sub>				0.6	Ω
Switching Frequency	f		188		312	kHz

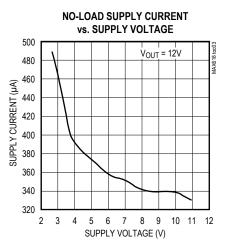
Note 2: Specifications to -40°C are guaranteed by design, not production tested.

## **Typical Operating Characteristics**

(Circuit of Figure 1,  $T_A = +25$ °C.)

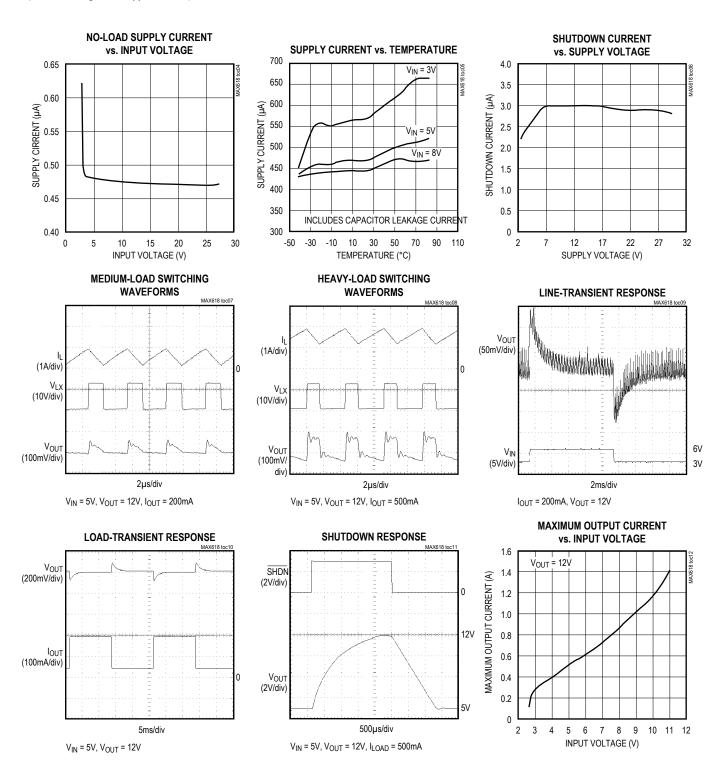






## **Typical Operating Characteristics (continued)**

(Circuit of Figure 1,  $T_A = +25$ °C.)



## **Pin Description**

PIN	NAME	FUNCTION
1, 8, 9, 12, 16	GND	Ground
2, 3, 4	LX	Drain of Internal n-channel Switch. Connect the inductor between IN and LX.
5	SHDN	Shutdown Input. A logic low puts the MAX618 in shutdown mode and reduces supply current to 3µA.  SHDN must not exceed VL. In shutdown, the output falls to V <sub>IN</sub> less one diode drop.
6	COMP	Compensation Input. Bypass to GND with the value of capacitance shown in Table 2.
7	FB	Feedback Input. Connect a resistor-divider network to set V <sub>OUT</sub> . FB threshold is 1.5V.
10	IN	LDO Regulator Supply Input. IN accepts inputs up to +28V. Bypass to GND with a $1\mu F$ ceramic capacitor as close to pins 10 and 12 as possible.
11	VL	Internal 3.1V LDO Regulator Output. Bypass to GND with a 4.7µF capacitor.
13, 14, 15	PGND	Power Ground. Source of internal N-channel switch.

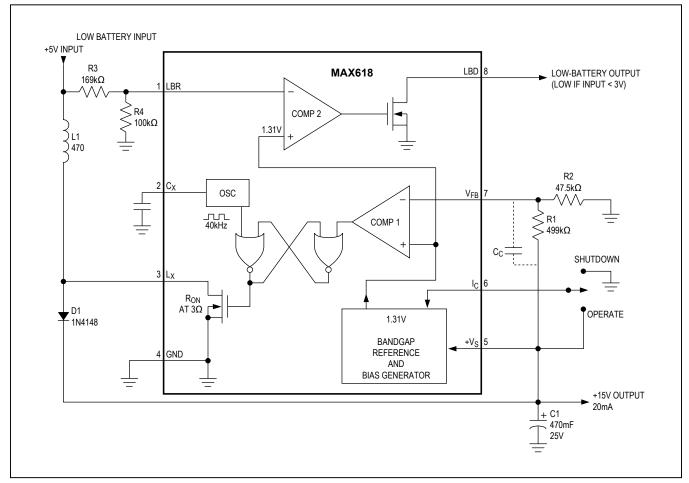


Figure 1. Single-Supply Operation

### **Detailed Description**

The MAX618 pulse-width modulation (PWM) DC-DC converter with an internal 28V switch operates in a wide range of DC-DC conversion applications including boost, SEPIC, and flyback configurations. The MAX618 uses fixed-frequency PWM operation and Maxim's proprietary Idle Mode control to optimize efficiency over a wide range of loads. It also features a shutdown mode to minimize quiescent current when not in operation.

# PWM Control Scheme and Idle Mode Operation

The MAX618 combines continuous-conduction PWM operation at medium to high loads and Idle Mode operation at light loads to provide high efficiency over a wide

range of load conditions. The MAX618 control scheme actively monitors the output current and automatically switches between PWM and Idle Mode to optimize efficiency and load regulation. Figure 2 shows a functional diagram of the MAX618's control scheme.

The MAX618 normally operates in low-noise, continuous-conduction PWM mode, switching at 250kHz. In PWM mode, the internal MOSFET switch turns on with each clock pulse. It remains on until either the error comparator trips or the inductor current reaches the 2A switch-current limit. The error comparator compares the feedback-error signal, current-sense signal, and slope-compensation signal in one circuit block. When the switch turns off, energy transfers from the inductor to the output capacitor. Output current is limited by the 2A MOSFET current limit

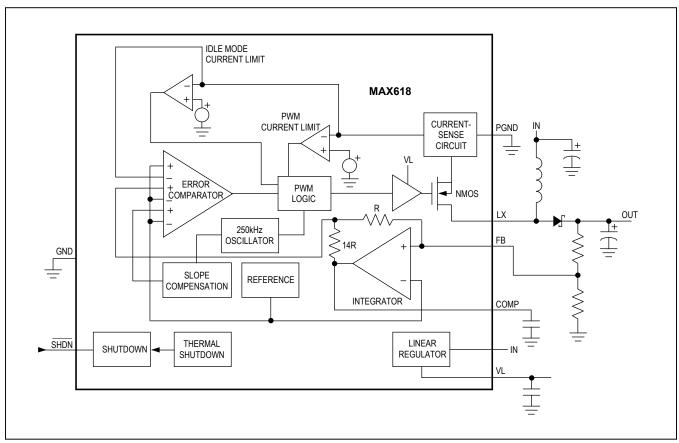


Figure 2. Functional Diagram

and the MAX618's package power-dissipation limit. See the *Maximum Output Current* section for details.

In Idle Mode, the MAX618 improves light-load efficiency by reducing inductor current and skipping cycles to reduce the losses in the internal switch, diode, and inductor. In this mode, a switching cycle initiates only when the error comparator senses that the output voltage is about to drop out of regulation. When this occurs, the NMOS switch turns on and remains on until the inductor current exceeds the nominal 350mA Idle Mode current limit.

Refer to Table 1 for an estimate of load currents at which the MAX618 transitions between PWM and Idle Mode.

#### **Compensation Scheme**

Although the higher loop gain of voltage-controlled architectures tends to provide tighter load regulation, current-controlled architectures are generally easier to compensate over wide input and output voltage ranges. The MAX618 uses both control schemes in parallel: the dominant, low-frequency components of the error signal are tightly regulated with a voltage-control loop, while a current-control loop improves stability at higher

frequencies. Compensation is achieved through the selection of the output capacitor ( $C_{OUT}$ ), the integrator capacitor ( $C_{COMP}$ ), and the pole capacitor ( $C_P$ ) from FB to GND.  $C_P$  cancels the zero formed by  $C_{OUT}$  and its ESR. Refer to the *Capacitor Selection* section for guidance on selecting these capacitors.

#### **VL Low-Dropout Regulator**

The MAX618 contains a 3.1V low-dropout linear regulator to power internal circuitry. The regulator's input is IN and its output is VL. The IN to VL dropout voltage is 100mV, so that when IN is less than 3.2V, VL is typically 100mV below IN. The MAX618 still operates when the LDO is in dropout, as long as VL remains above the 2.7V undervoltage lockout. Bypass VL with a 4.7 $\mu$ F ceramic capacitor placed as close to the VL and GND pins as possible.

VL can be overdriven by an external supply between 2.7V and 5.5V. In systems with +3.3V or +5V logic power supplies available, improve efficiency by powering VL and  $V_{IN}$  directly from the logic supply as shown in Figure 3.

Table 1. PWM/Idle-Mode Transition Load Current (IOUT in Amps) vs. Input and Output Voltage

;												>	Vout											
Z >	4	2	9	7	8	9	10	11	12	13	14	15	16	17 1	18 1	19 2	20 21	1 22		23 24	4 25	56	27	28
က	0.20	0.20	0.18	0.15	0.12	0.10	60.0	0.08	0.07	90.0	0.05	0.04	0.04 0	0.04 0.0	0.03 0.	0.03 0.	0.03 0.03	0.03		0.02 0.0	0.02 0.02	2 0.02	0.02	0.02
4		0.18	0.21	0.20	0.17	0.15	0.13	0.12	0.10	0.09	0.08	0.07	0.07	0.06 0.0	0.05 0.	0.05 0.	0.04 0.04	0.04		0.03 0.0	0.03 0.03	3 0.03	0.03	0.03
5			0.16	0.20	0.21	0.19	0.17	0.16	0.14	0.13	0.11	0.10	0.09	0.09	0.08 0.	0.07 0.	0.07 0.06	90.0 90		0.05 0.0	0.05 0.04	4 0.04	0.04	0.04
9				0.15	0.20	0.21	0.20	0.19	0.18	0.16	0.15 (	0.13 C	0.12 0	0.11 0.	0.10 0.	0.10 0.	0.09 0.08	90.08	$\overline{}$	0.07 0.0	0.07 0.06	6 0.06	0.05	0.05
7					0.17	0.19	0.21	0.21	0.20	0.19	0.17	0.16	0.15 0	0.14 0.	0.13 0.	0.12 0.	0.11 0.10	0.10		0.09 0.0	0.08 0.08	8 0.07	0.07	0.07
80						0.19	0.18	0.20	0.21	0.20	0.20	0.19	0.17 0	0.16 0.	0.15 0.	0.14 0.	0.13 0.13	13 0.12		0.11 0.	0.10 0.10	0.09	0.09	0.08
6							0.20	0.17	0.20	0.21	0.21	0.20	0.19 0	0.18 0.	0.18 0.	0.17 0.	0.16 0.15	15 0.14		0.13 0.	0.12 0.12	2 0.11	0.10	0.10
10								0.21	0.16	0.19	0.20	0.21	0.21	0.20	0.19 0.	0.18 0.	0.17 0.17	17 0.16		0.15 0.	0.14 0.13	3 0.13	0.12	0.11
11									0.22	0.15	0.19	0.20	0.21	0.21 0.3	0.20	0.20 0.	0.19 0.18	18 0.17		0.17 0.	0.16 0.15	5 0.14	0.14	0.13
12										0.23	0.15 (	0.18	0.20	0.21 0.21		0.21 0.	0.20 0.20	20 0.19		0.18 0.	0.18 0.17	7 0.16	0.15	0.15
13											0.24 (	0.16 C	0.17 0	0.19 0.3	0.20 0.3	0.21 0.21	21 0.20	20 0.20		0.19 0.	0.19 0.18	8 0.17	0.17	0.16
14												0.25	0.17 0	0.17 0.	0.19 0.	0.20 0.21	21 0.21	21 0.21		0.20	0.20 0.19	9 0.19	0.18	0.17
15												0	0.25 0	0.18 0.	0.16 0.	0.18 0.	0.20 0.20	20 0.21	21 0.21		0.21 0.2	0.20 0.20	0.19	0.19
16													0	0.26 0.	0.19 0.	0.16 0.	0.18 0.19	19 0.20	20 0.21	21 0.21	21 0.21	1 0.20	0.20	0.20
17														0.	0.26 0.	0.20 0.	0.15 0.17	17 0.19		0.20 0.3	0.20 0.21	1 0.21	0.21	0.20
18															0.	0.27 0.	0.20 0.15	15 0.17		0.19 0.2	0.20 0.20	0 0.21	0.21	0.21
19																0.	0.27 0.21	21 0.16		0.17 0.	0.18 0.19	9 0.20	0.21	0.21
20																	0.27	27 0.21	21 0.17		0.16 0.18	8 0.19	0.20	0.20
21																		0.28		0.22 0.	0.17 0.16	6 0.18	0.19	0.20
22																			0	0.28 0.2	0.22 0.18	8 0.15	0.17	0.19
23																				0.5	0.28 0.23	3 0.18	0.15	0.17
24																					0.28	8 0.23	0.19	0.15
25																						0.29	0.24	0.19
26																							0.29	0.24
27																								0.29

#### **Operating Configurations**

The MAX618 can be connected in one of three configurations described in Table 2 and shown in Figures 1, 3, and 4. The VL linear regulator allows operation from a single supply between +3V and +28V as shown in Figure 1.

The circuit in Figure 3 allows a logic supply to power the MAX618 while using a separate source for DC-DC conversion power (inductor voltage). The logic supply (between 2.7V and 5.5V) connects to VL and IN. VL = IN; voltages of 3.3V or more improve efficiency by providing greater gate drive for the internal MOSFET.

The circuit in Figure 4 allows separate supplies to power IN and the inductor voltage. It differs from the connection in Figure 3 in that the MAX618 chip supply is not limited to 5.5V.

**Table 2. Input Configurations** 

CIRCUIT	CONNECTION	V <sub>IN</sub> RANGE	INDUCTOR VOLTAGE	BENEFITS/COMMENTS
Figure 1	Input voltage connects to IN and inductor.	3V to V <sub>OUT</sub> (up to 28V)	V <sub>IN</sub>	Single supply operation.     SHDN must be connected to or pulled up to VL. On/off control requires an open-drain or open-collector connection to SHDN.
Figure 3	IN and VL connect together. Inductor voltage supplied by a separate source.	2.7V to 5.5V	0V to V <sub>OUT</sub> (up to 28V)	Increased efficiency.  This is a supply connected to IN and VL, or can be connected to or pulled up to VL.  Input power source (inductor voltage) is separate from the MAX618's bias (V <sub>IN</sub> = VL) and can be less than or greater than V <sub>IN</sub> .
Figure 4	IN and inductor voltage supplied by separate sources.	3V to 28V	0V to V <sub>OUT</sub> (up to 28V)	Input power source (inductor voltage) is separate from the MAX618's bias (V <sub>IN</sub> ) and can be less than or greater than V <sub>IN</sub> .     SHDN must be connected to or pulled up to VL. On/off control requires an open-drain or open-collector connection to SHDN.

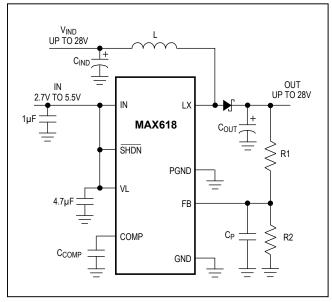


Figure 3. Dual-Supply Operation ( $V_{IN} = 2.7V$  to 5.5V)

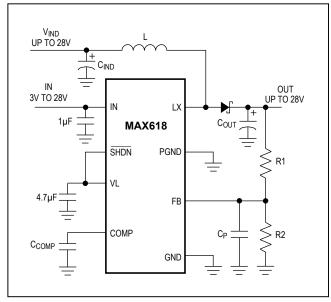


Figure 4. Dual-Supply Operation ( $V_{IN} = 3V$  to 28V)

#### **Shutdown Mode**

In shutdown mode ( $\overline{SHDN} = 0$ ), the MAX618's feedback and control circuit, reference, and internal biasing circuitry turn off and reduce the IN supply current to 3µA (10µA max). When in shutdown, a current path remains from the input to the output through the external inductor and diode. Consequently, the output falls to V<sub>IN</sub> less one diode drop in shutdown.

SHDN may not exceed VL. For always-on operation, connect SHDN to VL. To add on/off control to the circuit of Figure 1 or 4, pull  $\overline{SHDN}$  to VL with a resistor (10k $\Omega$ to  $100k\Omega$ ) and drive SHDN with an open-drain logic gate or switch as shown in Figure 5. Alternatively, the circuit of Figure 3 allows direct SHDN drive by any logic-level gate powered from the same supply that powers VL and IN, as shown in Figure 6.

#### **Design Procedure**

The MAX618 operates in a number of DC-DC converter configurations including step-up, SEPIC, and flyback. The following design discussion is limited to step-up converters.

#### **Setting the Output Voltage**

Two external resistors (R1 and R2) set the output voltage. First, select a value for R2 between  $10k\Omega$  and  $200k\Omega$ . Calculate R1 with:

$$R_1 = R_2 \left( \frac{V_{OUT}}{V_{FB}} - 1 \right)$$

where  $V_{FB}$  is 1.5V.

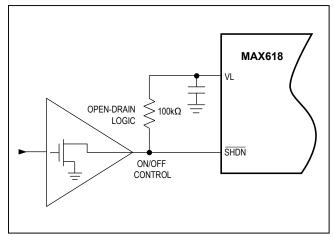


Figure 5. Adding On/Off Control to Circuit of Figure 1 or 4

#### **Determining the Inductor Value**

The MAX618's high switching frequency allows the use of a small value inductor. The recommended inductor value is proportional to the output voltage and is given by the following:

$$L = \frac{V_{OUT}}{7 \times 10^5}$$

After solving for the above equation, round down as necessary to select a standard inductor value.

When selecting an inductor, choose one rated to 250kHz, with a saturation current exceeding the peak inductor current, and with a DC resistance under  $200m\Omega$ . Ferrite core or equivalent inductors are generally appropriate (see MAX618 EV kit data sheet). Calculate the peak inductor current with the following equation:

$$I_{LX(PEAK)} = I_{OUT} \ \frac{V_{OUT}}{V_{IN}} + 2\mu s \left(\frac{V_{IN}}{L}\right) \left(\frac{\left(V_{OUT} - V_{IN}\right)}{V_{OUT}}\right)$$

Note that the peak inductor current is internally limited to 2A.

#### **Diode Selection**

The MAX618's high switching frequency demands a highspeed rectifier. Schottky diodes are preferred for most applications because of their fast recovery time and low forward voltage. Make sure that the diode's peak current rating exceeds the 2A peak switch current, and that its breakdown voltage exceeds the output voltage.

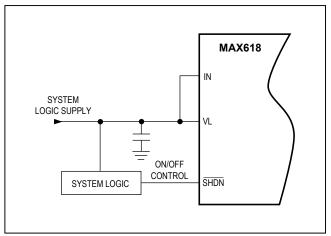


Figure 6. Adding On/Off Control to Circuit of Figure 3

#### **Maximum Output Current**

The MAX618's 2.2A LX current limit determines the output power that can be supplied for most applications. In some cases, particularly when the input voltage is low, output power is sometimes restricted by package dissipation limits. The MAX618 is protected by a thermal shutdown circuit that turns off the switch when the die temperature exceeds +150°C. When the device cools by 10°C, the switch is enabled again. Table 3 details output current with a variety of input and output voltages. Each listing in Table 3 is either the limit set by an LX current limit or by package dissipation at +85°C ambient, whichever is lower. The values in Table 3 assume a  $40m\Omega$  inductor resistance.

#### **Capacitor Selection**

#### **Input Capacitors**

The input bypass capacitor ( $C_{IND}$ ) reduces the input ripple created by the boost configuration. High-impedance sources require high  $C_{IND}$  values. However,  $68\mu F$  is generally adequate for input currents up to 2A. Low-ESR capacitors are recommended because they will decrease the ripple created on the input and improve efficiency. Capacitors with ESR below  $0.3\Omega$  are generally appropriate.

In addition to the input bypass capacitor, bypass IN with a  $1\mu F$  ceramic capacitor placed as close to the IN and GND pins as possible. Bypass VL with a  $4.7\mu F$  ceramic capacitor placed as close to the VL and GND pins as possible.

#### **Output Capacitor**

Use Table 4 to find the minimum output capacitance necessary to ensure stable operation. In addition, choose an output capacitor with low ESR to reduce the output ripple. The dominant component of output ripple is the product of the peak-to-peak inductor ripple current and the ESR of the output capacitor. ESR below  $50 m\Omega$  generates acceptable levels of output ripple for most applications.

#### **Integrator Capacitor**

The compensation capacitor ( $C_{COMP}$ ) sets the dominant pole in the MAX618's transfer function. The proper compensation capacitance depends upon output capacitance. Table 5 shows the capacitance value needed for the output capacitances specified in Table 4. However, if a

different output capacitor is used (e.g., a standard value), then recalculate the value of capacitance needed for the integrator capacitor with the following formula:

$$C_{COMP} = \frac{C_{COMP}(Table 5) \times C_{OUT}}{C_{OUT}(Table 4)}$$

Pole Compensation Capacitor

The pole capacitor ( $C_P$ ) cancels the unwanted zero introduced by  $C_{OUT}$ 's ESR, and thereby ensures stability in PWM operation. The exact value of the pole capacitor is not critical, but it should be near the value calculated by the following equation:

$$C_{P} = \frac{R_{ESR} \times C_{OUT}(R_1 + R_2)}{R_1 \times R_2}$$

where RESR is COUT'S ESR.

#### **Layout Considerations**

Proper PC board layout is essential due to high current levels and fast switching waveforms that radiate noise. Use the MAX618 evaluation kit or equivalent PC layout to perform initial prototyping. Breadboards, wire-wrap, and proto-boards are not recommended when prototyping switching regulators.

It is important to connect the GND pin, the input bypass capacitor ground lead, and the output filter capacitor ground lead to a single point to minimize ground noise and improve regulation. Also, minimize lead lengths to reduce stray capacitance, trace resistance, and radiated noise, with preference given to the feedback circuit, the ground circuit, and LX. Place the feedback resistors as close to the FB pin as possible. Place a  $1\mu F$  input bypass capacitor as close as possible to IN and GND.

Refer to the MAX618 evaluation kit for an example of proper board layout.

### **Chip Information**

PROCESS: BiCMOS

## **Package Information**

For the latest package outline information and land patterns (footprints), go to <a href="www.maximintegrated.com/packages">www.maximintegrated.com/packages</a>. Note that a "+", "#", or "-" in the package code indicates RoHS status only. Package drawings may show a different suffix character, but the drawing pertains to the package regardless of RoHS status.

PACKAGE TYPE	PACKAGE CODE	DOCUMENT NO.
16 QSOP	EF16+8F	<u>21-0055</u>

Table 3. Typical Output Current vs. Input and Output Voltages

	78	0.07	0.12	0.18	0.23	0.29	0.35	0.41	0.47	0.54	09.0	0.65	0.71	92.0	0.82	0.88	0.94	1.00	1.07	1.14	1.22	1.29	1.38	1.46	1.56	1.66
	27 2	0.08 0.	0.13 0.	0.18 0.	0.24 0.	0.30 0.	0.36 0.	0.43 0.	0.50 0.	0.56 0.	0.62 0.	0.67 0.		0.79 0.	0.85 0.	0.91 0.	0.98 0.	1.05 1.	12 1.	1.20 1.	1.28 1.	1.36 1.	1.45 1.	1.55 1.	1.65 1.	<u>–</u>
	26 2	0.08 0.	0.14 0.	0.19 0.	0.25 0.	0.31 0.	0.38 0.	0.45 0.	0.52 0.	58 0.	0.64 0.	0.70 0.	0.83 0.79 0.76 0.73	0.82 0.	0.89 0.	95 0.	1.02 0.	1.10 1.	1.31 1.24 1.18 1.12	1.26 1.	1.35 1.		1.54 1.	1.64 1.	<del>-</del>	
	25 2	0 80	0.14 0.	0.20	0.26 0.3	0.33 0.	0.40 0.3	0.47 0.	55 0.	31 0.	0.67 0.	73 0.	79 0.	0.86	93 0.	000	1.07	1.15 1.	24 1.	1.33 1.	1.42	1.53 1.44	1.64 1.3	1		
		80.0   60.0   60.0		21 0.2	28 0.2	35 0.3	12 0.4	50 0.4	0.57 0.55	0.63 0.61 0.58	0.0	0.76 0.73	33 0.7	30 0.8	0.97 0.93	1.11 1.05 1.00 0.95			31 1.2		-		1.6			
	24	9 0.0	6 0.15	2 0.21	9 0.28	6 0.35	4 0.42	3 0.50		6 0.6	3 0.70	0 0.7	7 0.8	4 0.90	2 0.6	1.0	0 1.13	9 1.22		0 1.41	2 1.51	1.63				
	23		3 0.16	3 0.22	1 0.29	3 0.36	7 0.44	5 0.53	2 0.59	99.0	3 0.73	3 0.80	1 0.87	9 0.94	3 1.02	1.1	7 1.20	1.29	9 1.39	1.50	1.62					
	22	0.10	0.16	0.23	0.31	0.38	0.47	0.55	0.62	69.0	92.0	0.83	0.91	0.99	1.08	1.17	1.27	1.37	1.49	1.61						
	2	0.10	0.17	0.25	0.32	0.41	0.50	0.58	0.65	0.72	0.80	0.88	96.0	1.05	1.14	1.25	1.36	1.47	1.60							
	20	0.12 0.12 0.11 0.10 0.10	0.18	0.26	0.37 0.34	0.46 0.43	0.56 0.53	0.64 0.61	0.72 0.68	0.85 0.80 0.76	0.84	1.05 0.99 0.93	1.02	1.12	1.22	1.44 1.33 1.25	1.46	1.59								
	19	0.12	0.19	0.28	0.37	0.46	0.56	0.64	0.72	0.80	0.89	0.99	1.09	1.19	1.31	1.44	1.58									
	18	0.12	0.21	0.30	0.39	0.50	0.59	0.67	0.76	0.85	0.95	1.05	1.16	1.29	1.42	1.57										
	17	0.13	0.22	0.32	0.42	0.53	0.62	0.71	0.81	0.91	1.02	1.13	1.26	1.40	1.55											
Vout	16	0.17 0.15 0.14 0.13	0.24	0.34	0.46		99.0	92.0	0.93 0.86 0.81	0.97	1.10	1.23	1.37   1.26   1.16   1.09   1.02	1.53												
	15	0.15	0.26 0.24	0.37	0.50 0.46	0.60 0.57	0.71 0.66	0.81	0.93	1.05 0.97	1.19	1.34	1.52													
	4	1.17	0.28	0.41	0.54	0.65	0.76	0.88	1.01	1.15	1.31	1.49														
	13	0.18	0.31	0.45	0.58	0.70	0.82	0.96	1.11	1.28	1.47	`														
	12	0.20	0.34	0.50	0.63	0.76	0.90	1.06	1.24	1.44																
	7	0.22	0.38	0.54	0.68	0.83	1.00	1.19	1.41	_																
	9		0.43 0	0.60		0.93 0	1.13 1	1.37	1																	
	ر و	0.29 0.25	0.49 0	0.67 0	0.85 0.76	1.07 0	1.32	1																		
	ω	0.34 0.	0.56 0.	0.76 0.	0.99 0.	1.26 1.	1																			
	2	0.41 0.	0.64 0.	0.89 0.	1.18 0.	1.																				
					1.																					
	9	9 0.49	92.0 9	1.09																						
	2	69'0 2	96.0																							
	4	0.77																								
7	2	3	4	2	9	7	8	6	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27

Table 4. Minimum Cout for Stability (µF)

	28	10	13	15	17	19	20	21	23	24	22	25	56	27	27	28	28	53	53	30	31	31	32	32	33	33
	27	1	14	16	18	20	21	23	24	25	26	27	27	28	29	29	30	30	31	32	32	33	33	34	34	
	26	12	15	17	19	21	22	24	25	26	27	28	29	29	30	31	31	32	33	33	34	34	35	35		
	25	12	15	18	20	22	24	25	27	28	29	29	30	31	32	32	33	34	34	35	36	36	37			
	24	13	16	19	21	23	25	27	28	29	30	31	32	33	33	8	35	36	36	37	38	38				
	23	14	17	20	23	25	27	29	30	31	32	33	34	35	35	36	37	38	38	39	40					
	22	15	18	21	24	26	29	30	32	33	34	35	36	37	37	38	39	40	41	42						
	21	15	20	23	26	28	31	32	34	35	36	37	38	39	40	41	42	43	43							
	20	17	21	25	28	30	33	34	36	37	38	39	40	42	43	4	45	46								
	19	18	23	26	30	33	35	37	38	40	4	42	43	4	46	47	48									
	18	19	24	58	32	35	38	39	41	43	44	45	47	48	49	20										
	17	21	27	31	35	39	41	42	44	46	47	49	20	52	53											
Vout	16	23	29	34	38	42	44	46	48	20	51	53	22	26												
	15	25	32	37	42	45	48	20	52	54	26	28	09													
	14	28	35	41	46	20	52	22	22	69	62	64														
	13	31	39	46	51	22	28	61	63	99	89															
	12	35	45	52	22	61	64	29	70	73																
	11	40	51	29	64	89	72	92	79																	
	10	46	29	29	72	77	82	98																		
	6	54	89	22	83	89	94																			
	8	65	80	06	97	104																				
	7	80	96	107	117																					
	9	100	118	132																						
	2	128	151																							
	4	173																								
, i	Z	ဇ	4	2	9	7	∞	6	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27

Table 5. Minimum CCOMP for Stability (nF)

	78	391	287	220	176	146	124	109	26	88	62	72	99	62	28	22	53	21	49	48	48	48	48	48	49	21
	27	370 3	272 2	209 2	167 1	139 1	119 1	104	93	84	. 22	. 69	64	29	26	53	51	20	49	48	48	48	48	49	51 ,	
	56	349	257 2	197 2	159 1	132 1	113 1	99	68	80	. 22	99	61	22	42	25	20	49	48	48	48	48	49	51		
	52	329 3	242 2	187 1	150   1	125 1	108	95	82	92	69	63	29	22	53	51	49	48	48	47	48	49	51			
	24	309	228 2	176 1	142 1	119 1	103 1	91	81	72	99	61	22	53	51	49	48	48	47	48	49	20				
	23	290	214 2	166 1	134 1	113 1	98	98	22	69	63	28	22	52	20	48	48	47	48	49	20					
	22	271	201	156	127	107	93	82	72	65	09	26	53	20	49	48	47	47	48	20						
	21	253	188	147	119	101	88	22	69	62	22	54	51	49	48	47	47	48	20							
	20	236	176	137	112	95	83	73	65	29	22	25	49	48	47	47	48	20								
	19	219	164	128	105	06	78	89	61	26	52	20	48	47	47	48	20									
	18	203	152	120	66	85	73	64	28	54	20	48	47	47	48	49										
	17	187	141	111	92	62	89	61	22	51	49	47	47	47	49											
Vout	16	172	130	103	98	74	64	22	25	49	47	47	47	49												
>	15	157	119	96	80	89	09	54	20	48	47	47	49													
	41	143	109	88	74	63	26	51	48	46	47	48														
	13	130	100	81	89	28	52	48	46	46	48															
	12	118	91	75	62	54	49	47	46	47																
	7	105	82	29	22	20	47	46	47																	
	10	94	74	09	52	47	45	46																		
	6	83	99	54	48	45	46																			
	80	73	28	49	45	45																				
	7	64	51	45	4																					
	9	42	45	43																						
	2	46	42																							
	4	40																								
>	Z >	က	4	2	9	7	80	6	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	56	27

## 28V Internal Switch, Step-Up DC-DC Converter

## **Revision History**

REVISION NUMBER	REVISION DATE	DESCRIPTION	PAGES CHANGED
0	6/09	Initial release	_
1	12/09	Updated part to lead-free, added soldering temperatures (reflow), and corrected error in equation	1, 2, 10
2	4/15	No /V ordering information; removed Automotive reference from <i>Applications</i> section	1

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