Quick start guide KIT_DRIVER_2EDN7524R

August 2018



KIT_DRIVER_2EDN7524R





Included in this kit

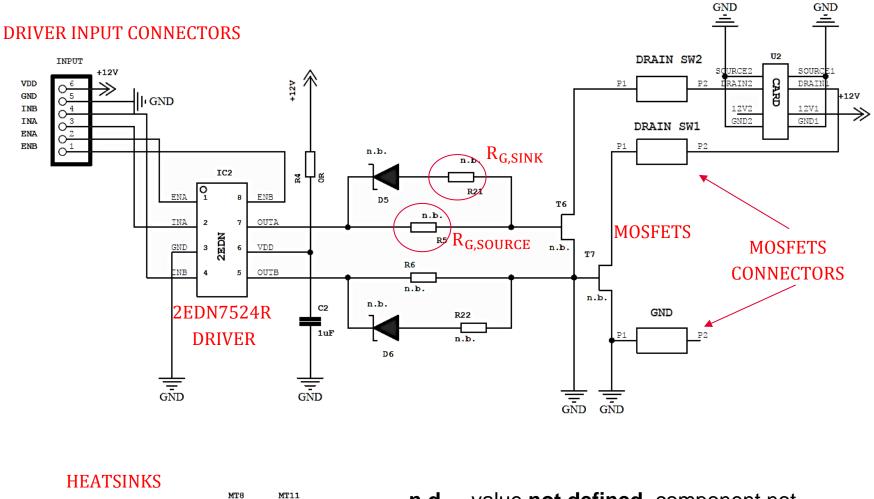




Heatsinks for TO-220 MOSFETs



Board schematic



HS8 TO-220 20

HS7 TO-220 20



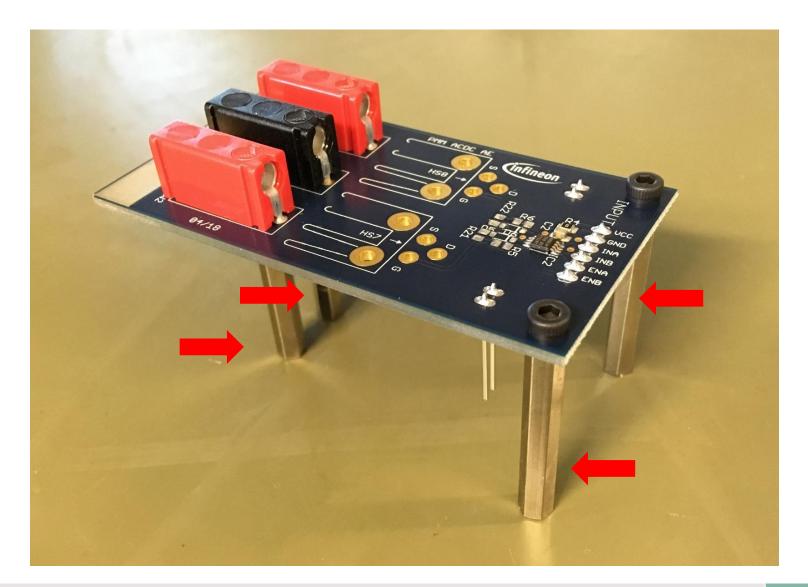
Components to add – BOM suggestion

Distance bolts	Screws for distance bolts	Screws and washers for MOSFET mounting to heatsink	TO-220 sockets		
		0	170		
TO-220 MOSFETs	Source resistors (R5, R6)	Sink resistors (R21, R22)	Sink diodes		
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Component	Quantity	Designator	Comment	Voltage	Footprint	Туре	Part number/ supplies
Sink diode	2	D5,D6	Schottky diode	30 V	SOD-123	PMEG3020 Schottky diode	816-6858 RS-Components
Resistors	4	R5,R6,R21,R22			RES805R	SMD ceramic resistor	
TO-220 sockets	2	Т6,Т7	TO-220 socket		TO-220	Receptacle Connector 0.034" ~ 0.041" (0.86 mm ~ 1.04 mm)	5050865-5 Digi-key



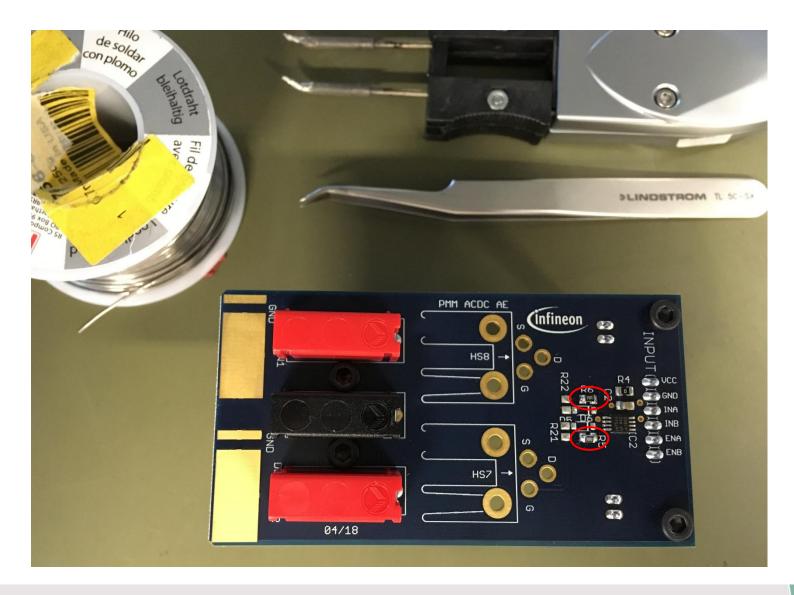
Step 1: Distance bolts mounting



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Step 2: Source resistors soldering



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Step 3: Sink resistors and sink diodes soldering

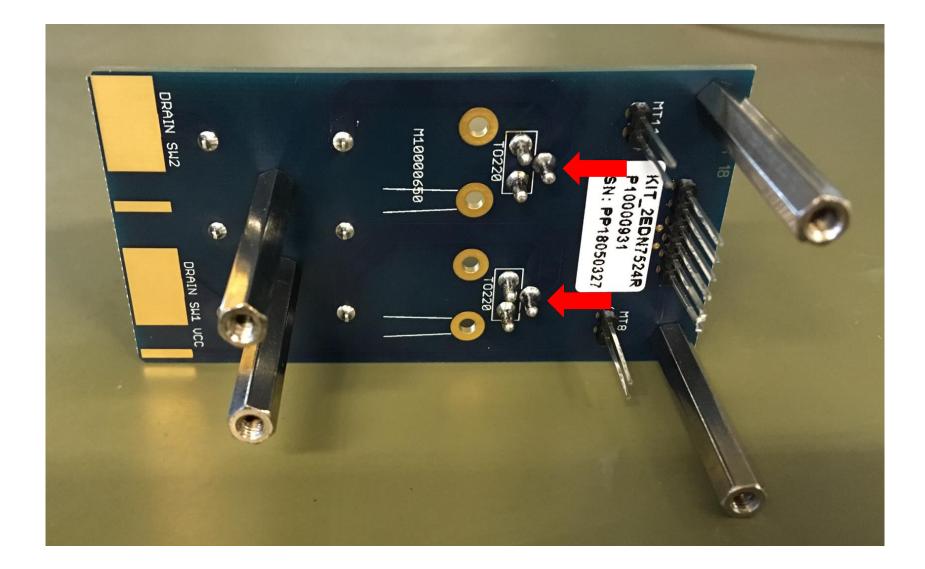


 Add the sink resistors and the sink diodes only if a differentiation between the turn-on and the turn-off behavior is required



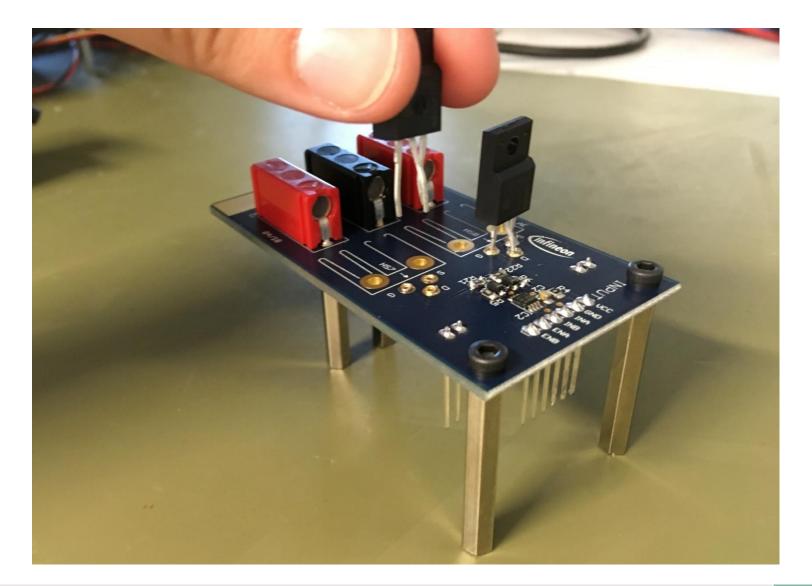
Step 4: TO-220 sockets soldering







Step 5: MOSFETs placement into the sockets

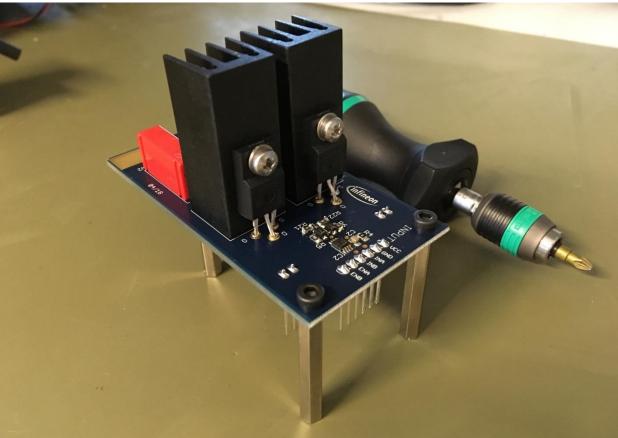


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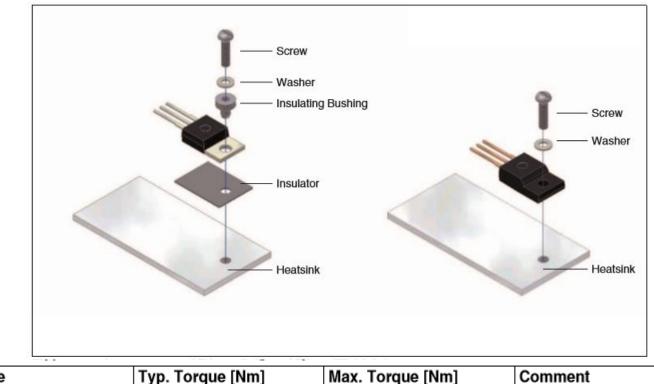
Step 6: Heatsink mounting (optional)

- > Solder the heatsink if the board is used in high voltage scenarios
- > In basic measurements it is not necessary
- See next slide for further information on how to properly mount the MOSFETs to the heatsink





TO-220 MOSFET mounting to the heatsink

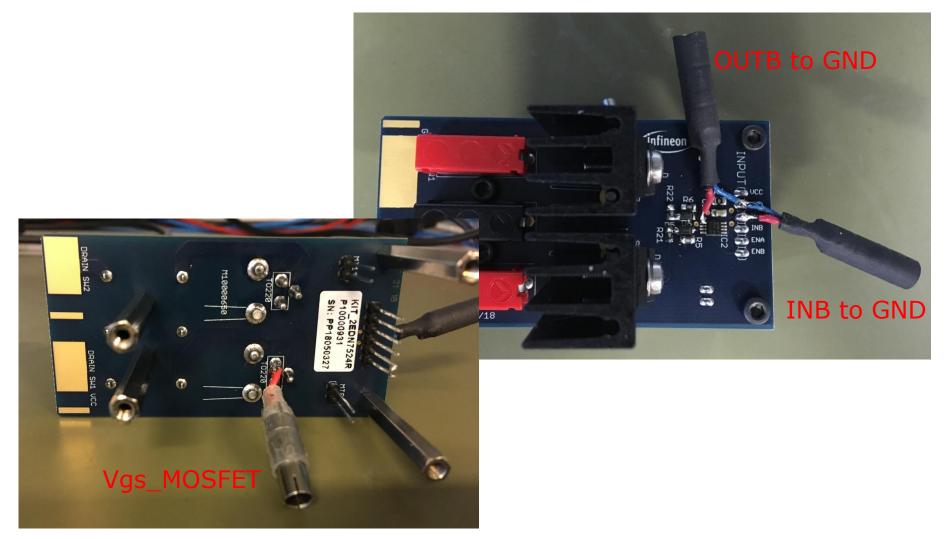


Package	Typ. Torque [Nm]	Max. Torque [Nm]	Comment
PG-TO220	0.6	0.7	Screw M3
PG-TO220 FullPAK	0.5	0.7	Screw M2.5

Recommendations for assembly of Infineon TO packages: <u>https://www.infineon.com/dgdl/Infineon-</u> <u>Package recommendations for assembly of Infineon TO packages-AN-v01 00-</u> <u>EN.pdf?fileId=db3a30431936bc4b011938532f885a38</u>



Step 7: BNC connectors soldering



> N.B. Please note that the silkscreen labels for INA and INB are merged



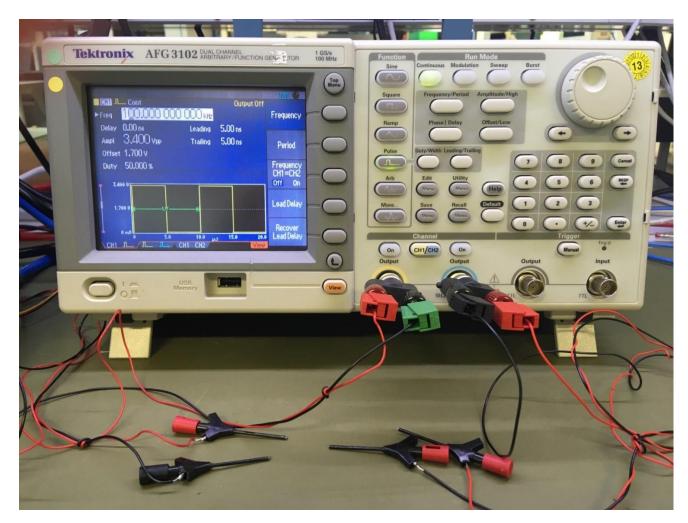
Instrumentation for driver supply generation



- V_{cc}=12 V for CoolMOS[™] and 8 V for OptiMOS[™]
- > Set the current limit below 1 A (0.8 A e.g.)



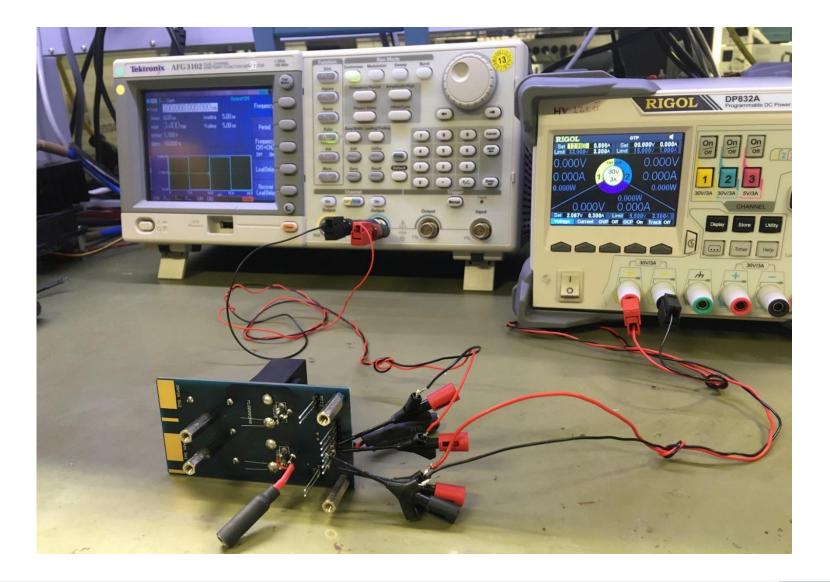
Instrumentation for PWM signals generation



> Use a function generator or a microcontroller

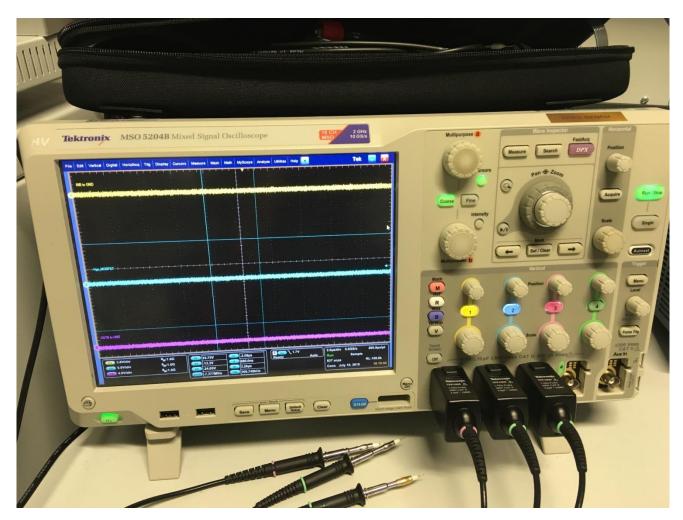


Connections





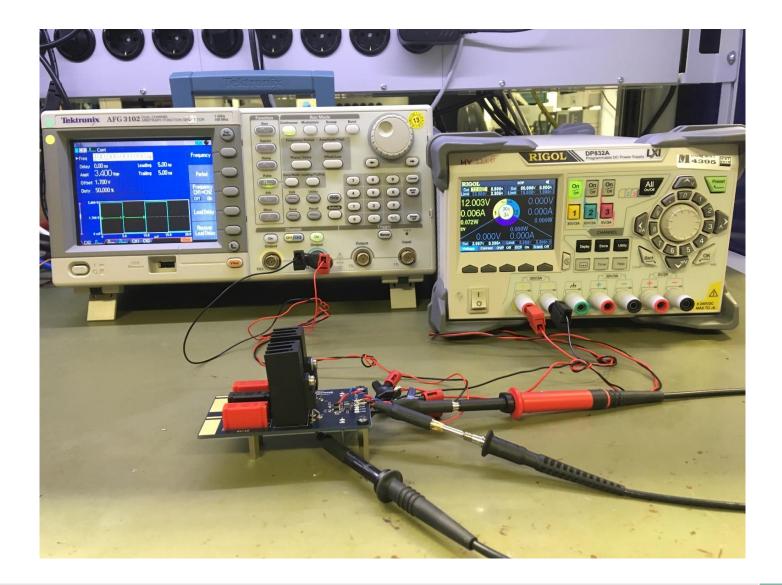
Instrumentation for signals evaluation



> Voltage probes used: Tetronix TPP1000 1 GHz, 3.9 pF

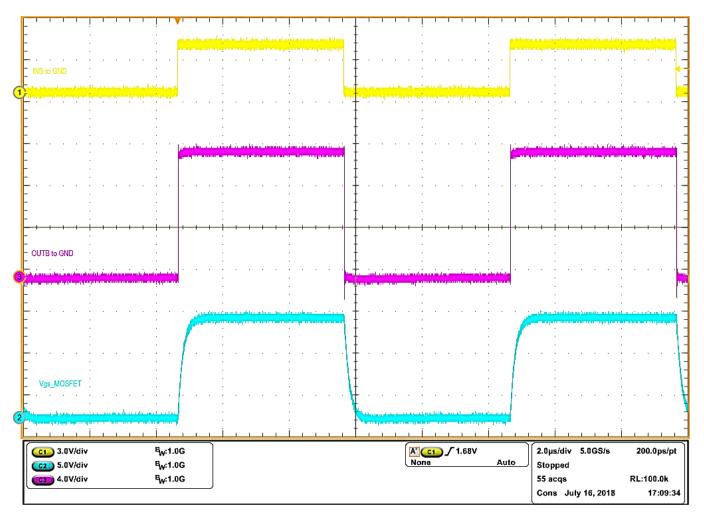


Complete measurement setup





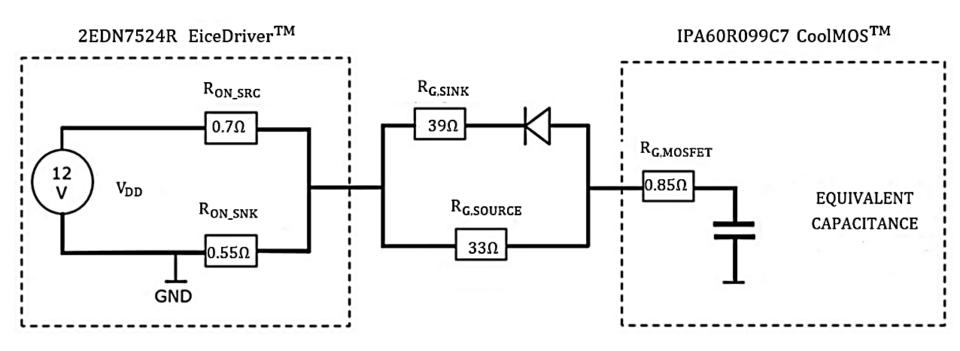
Oscilloscope waveforms



> Measurements done on a single MOSFET with $V_{DS} = 0 V$ (drain and source shorted)

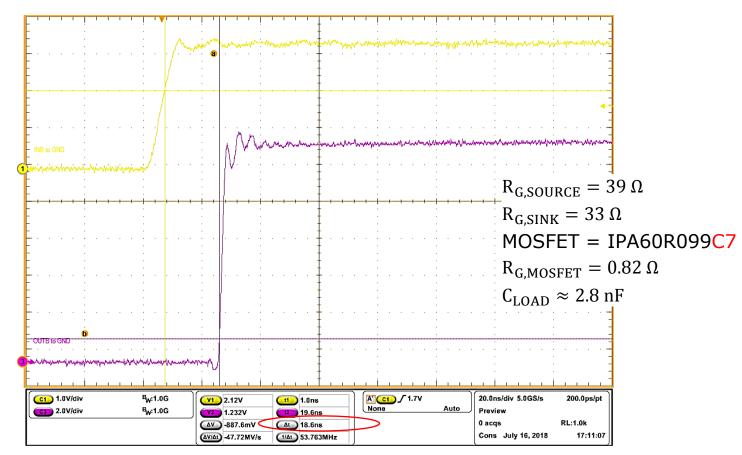


Equivalent model of the driving circuit





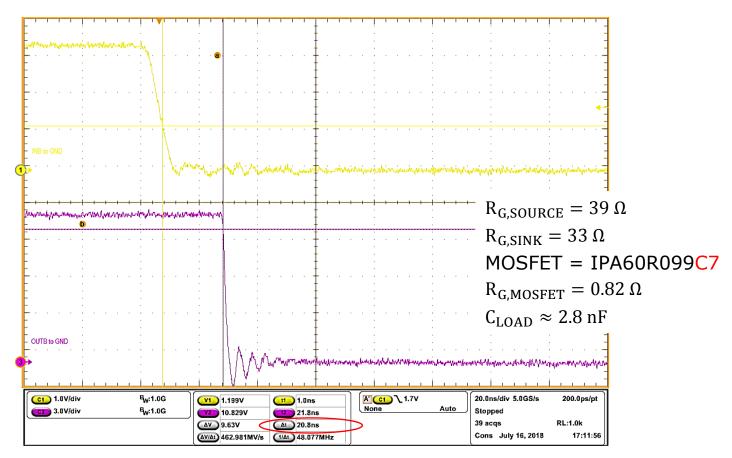
Low-high propagation delay



- > t_{PDlh} defined in the datasheed as time interval t(OUTB = 10% VDD) t(INB = V_{INH} = 2.1 V) for a pure capacitive load $C_{LOAD} = 1.8 \text{ nF}$ with $R_{G,SOURCE} = 0 \Omega$
- > N.B. In the considered measurements the load is the transistor with $R_{G,MOSFET} = 0.82 \Omega$, $R_{G,SOURCE} = 39 \Omega$, $C_{LOAD} \approx 2.8 \text{ nF}$ (see slide 23 for C_{LOAD} calculation)



High-Low propagation delay

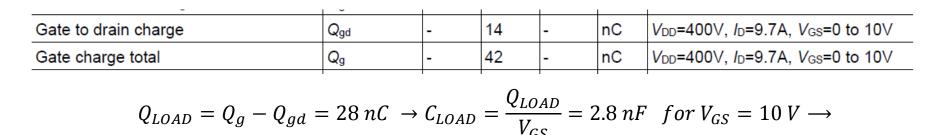


- > t_{PDhl} defined in the datasheed as time interval t(OUTB = 90% VDD) t(INB = V_{INL} = 1.02 V) for a pure capacitive load $C_{LOAD} = 1.8 \text{ nF}$ with $R_{G,SINK} = 0 \Omega$
- > N.B. In the considered measurements the load is the transistor with $R_{G,MOSFET} = 0.82 \Omega$, $R_{G,SINK} = 33 \Omega$, $C_{LOAD} \approx 2.8 nF$

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C_{LOAD} calculation for IPA60R099C7

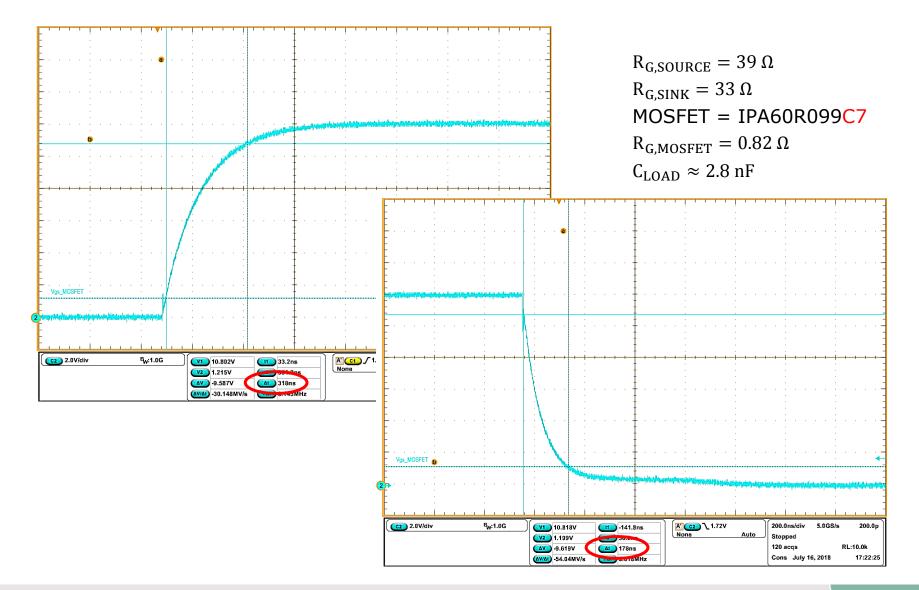




 $C_{LOAD} \approx 2.8 \, nF \, for \, V_{GS} = 12 \, V$

Rise/fall times





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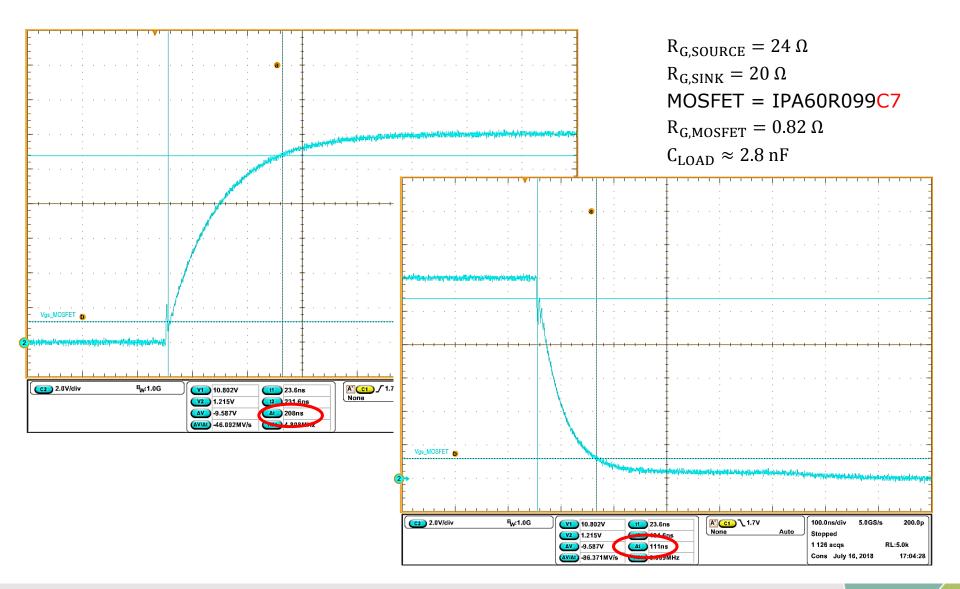


$R_{G,SOURCE} = 39 \Omega \rightarrow 24 \Omega$ $R_{G,SINK} = 33 \Omega \rightarrow 20 \Omega$

MOSFET = IPA60R099C7



Rise/fall times: New set of gate resistances



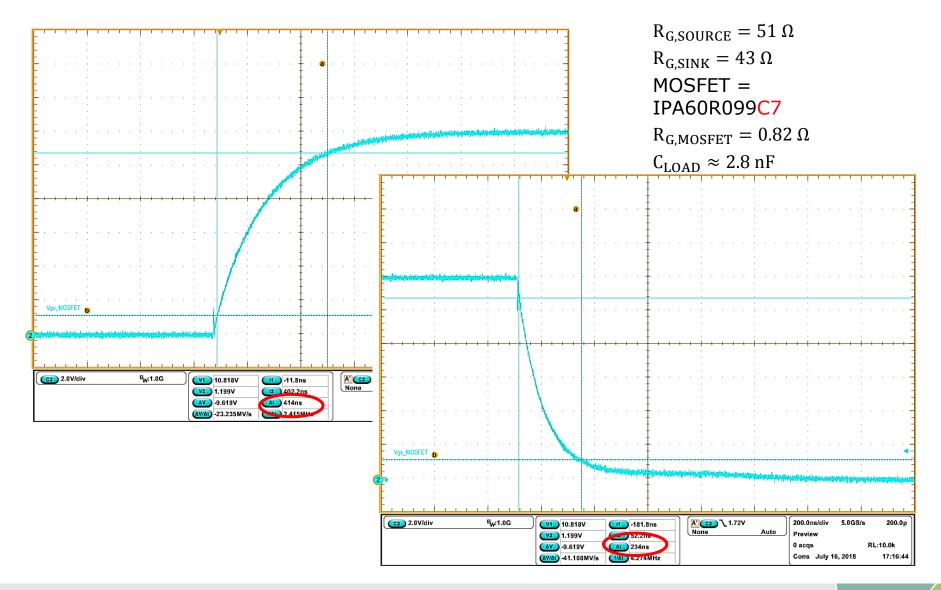


$R_{G,SOURCE} = 24 \Omega \rightarrow 51 \Omega$ $R_{G,SINK} = 20 \Omega \rightarrow 43 \Omega$

MOSFET = IPA60R099C7



Rise/fall times: New set of gate resistances





MOSFET Replacement

$IPA60R099C7 \rightarrow IPA60R280CFD7$

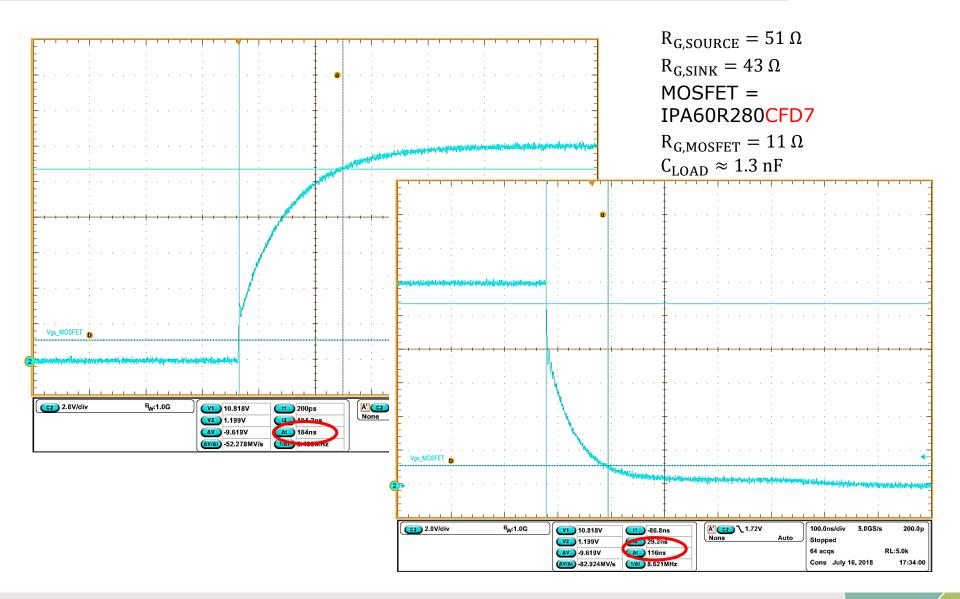


Gate to drain charge	Q _{gd}	-	5	-	nC	V_{DD} =400V, I_{D} =5.0A, V_{GS} =0 to 10V
Gate charge total	Qg	-	18	-	nC	V_{DD} =400V, I_{D} =5.0A, V_{GS} =0 to 10V

$$C_{LOAD} \approx \frac{13 \ nC}{10 \ V} = 1.3 \ nF \ for \ V_{GS} = 12 \ V$$



Rise/fall times: New MOSFET





MOSFET replacement

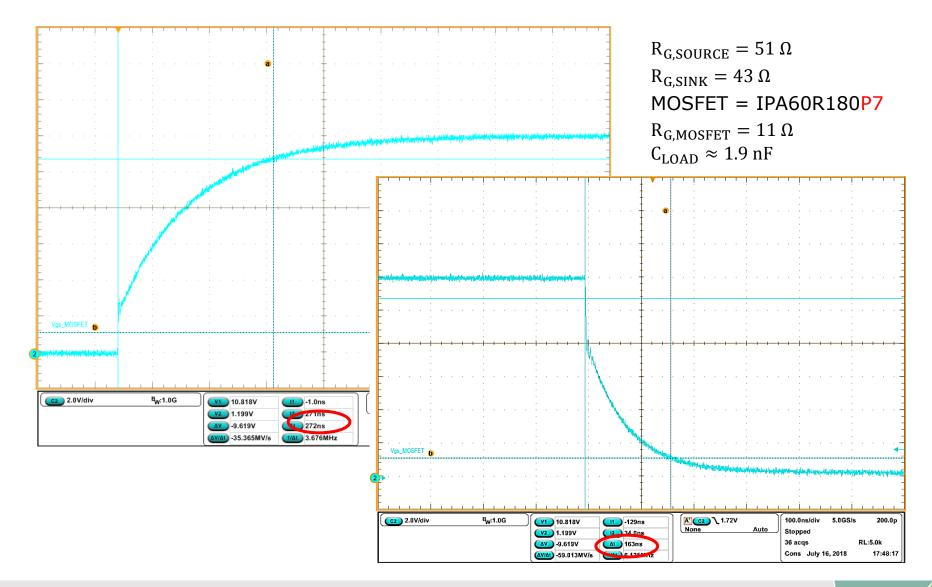
$IPA60R280CFD7 \rightarrow IPA60R180P7$

Gate to drain charge	Q _{gd}	-	8	-	nC	V _{DD} =400V, <i>I</i> _D =5.6A, <i>V</i> _{GS} =0 to 10V
Gate charge total	Qg	-	25	-	nC	V _{DD} =400V, <i>I</i> _D =5.6A, <i>V</i> _{GS} =0 to 10V

$$C_{LOAD} \approx \frac{19 \ nC}{10 \ V} = 1.9 \ nF \ for \ V_{GS} = 12 \ V$$



Rise/fall times: New MOSFET





Additional notes

- Note that the MOSFET is not turned-on or -off, you are only charging/discharging the gate-to-source capacitance
- Changing the gate resistors and the MOSFETs, you are changing the load for the driver
- If you want to turn-on or turn-off the MOSFET, you must integrate the board in a proper circuit
- You can not apply directly the voltage (e.g 400 V) across the MOSFET through the banana connectors on the board
- You must limit the input current from the DC source generator → add an inductance
- You must create a freewheeling path for the current when MOSFET is off

Example: boost converter, simple MOSFET in clamped inductive mode



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