FAN501
Offline DCM / CCM Flyback PWM Controller for Charger Applications

Features
- WSaver® Technology Provides Ultra-Low Standby Power Consumption for Energy Star’s 5-Star Level (<30 mW)
- Constant-Current (CC) Control without Secondary-Side Feedback Circuitry for Discontinuous Conduction Mode (DCM) and Continuous Conduction Mode (CCM)
- Dual-Frequency Function Changes Switching Frequency (140 kHz / 85 kHz) According to Input Voltage to Maximize Transformer Utilization and Improve Efficiency
- High Power Density and High Conversion Efficiency with CCM Operation in Typical 10 W to 15 W Compact Charger Applications
- Frequency Hopping to Reduce EMI Noise
- High-Voltage Startup
- Precise Maximum Output Power Limit by CC Regulation through External Resistor Adjustment
- Peak-Current-Mode Control with Slope Compensation to Avoid Sub-Harmonic Oscillation
- Programmable Over-Temperature Protection with Latch Mode through External NTC Resistor
- V_{OVP} Over-Voltage Protection with Latch Mode
- V_{UV} Under-Voltage Protection with Auto-Restart
- V_{DD} Over-Voltage-Protection with Auto-Restart
- Available in MLP 4x3 Package

Applications
- Battery Chargers for Smart Phones, Feature Phones, and Tablet PCs
- AC-DC Adapters for Portable Devices or Battery Chargers that Require CV / CC Control

Description
The advanced PWM controller, FAN501, simplifies isolated power supply design that requires CC regulation of the output. The output current is precisely estimated with only the information in the primary side of the transformer and controlled with an internal compensation circuit, removing the output current-sensing loss and eliminating external CC control circuitry. With an extremely low operating current (250 µA), Burst Mode maximizes light-load efficiency, allowing conformance to worldwide Standby Mode efficiency guidelines.

Compared with a conventional approach using external control circuit in the secondary side for CC regulation, the FAN501 can reduce total cost, component count, size, and weight; while increasing efficiency, productivity, and system reliability.

Figure 1. Typical Output V-I Characteristic

Ordering Information

<table>
<thead>
<tr>
<th>Part Number</th>
<th>Operating Temperature Range</th>
<th>Package</th>
<th>Packing Method</th>
</tr>
</thead>
<tbody>
<tr>
<td>FAN501MPX</td>
<td>-40°C to +125°C</td>
<td>10-Lead, MLP, QUAD, JEDEC MO-220 4 mm x 3 mm, 0.8 mm Pitch, Single DAP</td>
<td>Tape &amp; Reel</td>
</tr>
</tbody>
</table>
Application Diagram

Figure 2. Typical Application

Internal Block Diagram

Figure 3. Function Block Diagram
Marking Information

FAN501

F- Fairchild Logo
Z: Assembly Plant Code
X: Year Code
Y: Week Code
TT: Die Run Code
T: Package Type (MP=MLP)
M: Manufacture Flow Code

Figure 4. Top Mark

Pin Configuration

HV

SD

FB

CS

FAN501

5

SGND

4

COMP

3

2

1

PGND

10

9

8

7

6

Pin Definitions

<table>
<thead>
<tr>
<th>Pin #</th>
<th>Name</th>
<th>Description</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>GATE</td>
<td>PWM Signal Output. This pin has an internal totem-pole output driver to drive the power MOSFET. The gate driving voltage is internally clamped at 7.5 V.</td>
</tr>
<tr>
<td>2</td>
<td>VDD</td>
<td>Power Supply. IC operating current and MOSFET driving current are supplied through this pin. This pin is typically connected to an external capacitor.</td>
</tr>
<tr>
<td>3</td>
<td>VS</td>
<td>Voltage Sense. This pin detects the output voltage information and diode current discharge time based on the voltage of the auxiliary winding. It also senses sink current through the auxiliary winding to detect input voltage information.</td>
</tr>
<tr>
<td>4</td>
<td>COMP</td>
<td>CC Control Correction. This pin connects to external resistor to program the CC control correction weighting.</td>
</tr>
<tr>
<td>5</td>
<td>SGND</td>
<td>Signal Ground</td>
</tr>
<tr>
<td>6</td>
<td>FB</td>
<td>Feedback. An opto-coupler is typically connected to this pin to provide feedback information to the internal PWM comparator. This feedback is used to control the duty cycle in Constant-Voltage (CV) regulation.</td>
</tr>
<tr>
<td>7</td>
<td>SD</td>
<td>Shut Down. This pin is implemented for external over-temperature protection by connecting to an NTC thermistor.</td>
</tr>
<tr>
<td>8</td>
<td>HV</td>
<td>High Voltage. This pin connects to a DC bus for high-voltage startup.</td>
</tr>
<tr>
<td>9</td>
<td>CS</td>
<td>Current Sense. This pin connects to a current-sense resistor to detect the MOSFET current for Peak-Current-Mode control for output regulation. The current-sense information is also used to estimate the output current for CC regulation.</td>
</tr>
<tr>
<td>10</td>
<td>PGND</td>
<td>Power Ground</td>
</tr>
</tbody>
</table>
Absolute Maximum Ratings

Stresses exceeding the absolute maximum ratings may damage the device. The device may not function or be operable above the recommended operating conditions and stressing the parts to these levels is not recommended. In addition, extended exposure to stresses above the recommended operating conditions may affect device reliability. The absolute maximum ratings are stress ratings only.

<table>
<thead>
<tr>
<th>Symbol</th>
<th>Parameter</th>
<th>Min.</th>
<th>Max.</th>
<th>Unit</th>
</tr>
</thead>
<tbody>
<tr>
<td>$V_{HV}$</td>
<td>HV Pin Input Voltage</td>
<td></td>
<td>500</td>
<td>V</td>
</tr>
<tr>
<td>$V_{VDD}$</td>
<td>DC Supply Voltage</td>
<td></td>
<td>30</td>
<td>V</td>
</tr>
<tr>
<td>$V_{VS}$</td>
<td>VS Pin Input Voltage</td>
<td>-0.3</td>
<td>6.0</td>
<td>V</td>
</tr>
<tr>
<td>$V_{CS}$</td>
<td>CS Pin Input Voltage</td>
<td>-0.3</td>
<td>6.0</td>
<td>V</td>
</tr>
<tr>
<td>$V_{FB}$</td>
<td>FB Pin Input Voltage</td>
<td>-0.3</td>
<td>6.0</td>
<td>V</td>
</tr>
<tr>
<td>$V_{COMP}$</td>
<td>COMP Pin Input Voltage</td>
<td>-0.3</td>
<td>6.0</td>
<td>V</td>
</tr>
<tr>
<td>$V_{SD}$</td>
<td>SD Pin Input Voltage</td>
<td>-0.3</td>
<td>6.0</td>
<td>V</td>
</tr>
<tr>
<td>$P_D$</td>
<td>Power Dissipation ($T_A=25^\circ C$)</td>
<td></td>
<td>850</td>
<td>mW</td>
</tr>
<tr>
<td>$\theta_{JA}$</td>
<td>Thermal Resistance (Junction-to-Air)</td>
<td></td>
<td>150</td>
<td>°C/W</td>
</tr>
<tr>
<td>$\theta_{JC}$</td>
<td>Thermal Resistance (Junction-to-Case)</td>
<td></td>
<td>10</td>
<td>°C/W</td>
</tr>
<tr>
<td>$T_J$</td>
<td>Operating Junction Temperature</td>
<td>-40</td>
<td>+150</td>
<td>°C</td>
</tr>
<tr>
<td>$T_{STG}$</td>
<td>Storage Temperature Range</td>
<td>-40</td>
<td>+150</td>
<td>°C</td>
</tr>
<tr>
<td>$T_L$</td>
<td>Lead Temperature (Wave soldering or IR, 10 Seconds)</td>
<td></td>
<td>+260</td>
<td>°C</td>
</tr>
<tr>
<td>ESD</td>
<td>Electrostatic Discharge Capability(a)</td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td></td>
<td>Human Body Model, ANSI/ESDA/JEDEC JS-001-2012 (Except HV Pin)</td>
<td>5.0</td>
<td></td>
<td>kV</td>
</tr>
<tr>
<td></td>
<td>Charged Device Model, JEDEC:JESD22_C101 (Except HV Pin)</td>
<td>2.0</td>
<td></td>
<td></td>
</tr>
</tbody>
</table>

Notes:
1. All voltage values, except differential voltages, are given with respect to the GND pin.
2. Stresses beyond those listed under Absolute Maximum Ratings may cause permanent damage to the device.
3. ESD ratings including HV pin: HBM=3.0 kV, CDM=750 V.
## Electrical Characteristics

\( V_{DD} = 15 \text{ V} \) and \( T_{J} = 40 \sim 125 \degree \text{C} \) unless noted.

<table>
<thead>
<tr>
<th>Symbol</th>
<th>Parameter</th>
<th>Conditions</th>
<th>Min.</th>
<th>Typ.</th>
<th>Max.</th>
<th>Unit</th>
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</thead>
<tbody>
<tr>
<td>( V_{HV-MIN} )</td>
<td>Minimum Startup Voltage on HV Pin</td>
<td>( V_{HV}=120 \text{ V}, V_{DD}=0 \text{ V} )</td>
<td>30</td>
<td></td>
<td></td>
<td>V</td>
</tr>
<tr>
<td>( I_{HV} )</td>
<td>Supply Current Drawn from HV Pin</td>
<td>( V_{HV}=500 \text{ V}, V_{DD}=V_{DD-OFF}+1 \text{ V} )</td>
<td>1.2</td>
<td>2.0</td>
<td>5.0</td>
<td>mA</td>
</tr>
<tr>
<td>( I_{HV-LC} )</td>
<td>Leakage Current Drawn from HV Pin</td>
<td></td>
<td>0.8</td>
<td>10.0</td>
<td></td>
<td>( \mu \text{A} )</td>
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<table>
<thead>
<tr>
<th>( V_{DD} ) Section</th>
<th></th>
<th></th>
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<tbody>
<tr>
<td>( V_{DD-ON} )</td>
<td>Turn-On Threshold Voltage(^4)</td>
<td>( V_{DD} ) Rising</td>
<td>16.5</td>
<td>17.5</td>
</tr>
<tr>
<td>( V_{DD-OFF} )</td>
<td>Turn-Off Threshold Voltage</td>
<td>( V_{DD} ) Falling</td>
<td>5.3</td>
<td>5.8</td>
</tr>
<tr>
<td>( V_{DD-DLH} )</td>
<td>Threshold Voltage for Latch Release(^5)</td>
<td>( V_{DD}=V_{DD-ON}-0.16 \text{ V} )</td>
<td>2.50</td>
<td></td>
</tr>
<tr>
<td>( I_{DD-ST} )</td>
<td>Startup Current</td>
<td>( V_{DD}=V_{DD-ON}-0.16 \text{ V} )</td>
<td>150</td>
<td>250</td>
</tr>
<tr>
<td>( I_{DD-OP} )</td>
<td>Operating Supply Current</td>
<td>( \text{Typical} )</td>
<td>3.5</td>
<td>4.0</td>
</tr>
<tr>
<td>( I_{DD-Burst} )</td>
<td>Burst Mode Operating Supply Current</td>
<td>( \text{Typical} )</td>
<td>250</td>
<td>300</td>
</tr>
<tr>
<td>( V_{DD-OVP} )</td>
<td>( V_{DD} ) Over-Voltage Protection Level</td>
<td>( \text{Typical} )</td>
<td>26.5</td>
<td>28.0</td>
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</table>

<table>
<thead>
<tr>
<th>Oscillator Section</th>
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<tbody>
<tr>
<td>( f_{OSC-H} )</td>
<td>Operating Frequency, ( I_{VS} ) Below Threshold</td>
<td>( V_{CS}=5 \text{ V}, V_{S}=2.5 \text{ V}, V_{FB}=6 \text{ V} )</td>
<td>133</td>
<td>140</td>
</tr>
<tr>
<td>( f_{OSC-L} )</td>
<td>Operating Frequency, ( I_{VS} ) Over Threshold</td>
<td>( V_{CS}=5 \text{ V}, V_{S}=2.5 \text{ V}, V_{FB}=4 \text{ V} )</td>
<td>79</td>
<td>85</td>
</tr>
<tr>
<td>( \Delta f_{hopping-H} )</td>
<td>Frequency Hopping Range, High Line</td>
<td>( V_{CS}=0.5 \text{ V}, V_{S}=0.7 \text{ V}, V_{FB}=3 \text{ V} )</td>
<td>( \pm 5.5 )</td>
<td>( \pm 7.0 )</td>
</tr>
<tr>
<td>( \Delta f_{hopping-L} )</td>
<td>Frequency Hopping Range, Low Line</td>
<td>( V_{CS}=0.5 \text{ V}, V_{S}=0.0 \text{ V}, V_{FB}=3 \text{ V} )</td>
<td>( \pm 2.5 )</td>
<td>( \pm 4.0 )</td>
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<tr>
<td>( \Delta t_{hopping} )</td>
<td>Frequency Hopping Period</td>
<td>( \text{Typical} )</td>
<td>2.54</td>
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<table>
<thead>
<tr>
<th>Feedback Input Section</th>
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<tbody>
<tr>
<td>( Z_{FB} )</td>
<td>FB Pin Input Impedance(^4)</td>
<td>( \text{Typical} )</td>
<td>38</td>
</tr>
<tr>
<td>( A_{V} )</td>
<td>Internal Voltage Attenuator of FB Pin(^5)</td>
<td>( \text{Typical} )</td>
<td>1/2.5</td>
</tr>
<tr>
<td>( V_{FB-Open} )</td>
<td>FB Pin Pull-Up Voltage</td>
<td>( \text{FB Pin Open} )</td>
<td>5.00</td>
</tr>
<tr>
<td>( V_{FB'-Burst-H} )</td>
<td>FB Threshold to Enable Gate Drive in Burst Mode(^4)</td>
<td>( V_{FB} ) Rising with ( V_{CS}=0.3 \text{ V}, V_{S}=0 \text{ V} )</td>
<td>1.60</td>
</tr>
<tr>
<td>( V_{FB'-Burst-L} )</td>
<td>FB Threshold to Disable Gate Drive in Burst Mode(^4)</td>
<td>( V_{FB} ) Falling with ( V_{CS}=0.3 \text{ V}, V_{S}=0 \text{ V} )</td>
<td>1.55</td>
</tr>
</tbody>
</table>

<table>
<thead>
<tr>
<th>Over-Temperature Protection Section</th>
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</thead>
<tbody>
<tr>
<td>( T_{OTP} )</td>
<td>Threshold Temperature for Over-Temperature Protection</td>
<td>( \text{Typical} )</td>
</tr>
</tbody>
</table>

<table>
<thead>
<tr>
<th>Shutdown Function Section</th>
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<th></th>
</tr>
</thead>
<tbody>
<tr>
<td>( I_{SD} )</td>
<td>SD Pin Source Current</td>
<td>( V_{CS}=0.3 \text{ V} )</td>
</tr>
<tr>
<td>( V_{SD-TH} )</td>
<td>Threshold Voltage for Shutdown Function Enable</td>
<td>( V_{CS}=0.3 \text{ V} )</td>
</tr>
</tbody>
</table>

Continued on the following page...
## Electrical Characteristics

$V_{DD}=15 \text{ V}$ and $T_J=\text{-}40\text{ to }125^\circ \text{C}$ unless noted.

### Symbol | Parameter | Conditions | Min. | Typ. | Max. | Unit
--- | --- | --- | --- | --- | --- | ---

#### Voltage-Sense Section

<table>
<thead>
<tr>
<th>Symbol</th>
<th>Parameter</th>
<th>Conditions</th>
<th>Min.</th>
<th>Typ.</th>
<th>Max.</th>
<th>Unit</th>
</tr>
</thead>
<tbody>
<tr>
<td>$I_{TC}$</td>
<td>Temperature-Independent Bias Current</td>
<td>$V_{CS}=5 \text{ V}, V_{FB}=3 \text{ V}$</td>
<td>8.75</td>
<td>10.00</td>
<td>11.25</td>
<td>$\mu\text{A}$</td>
</tr>
<tr>
<td>$I_{VS-H}$</td>
<td>$V_S$ Source Current Threshold to $f_{OSC-L}$ Operation$^4$</td>
<td>750</td>
<td>$\mu\text{A}$</td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>$I_{VS-L}$</td>
<td>$V_S$ Source Current Threshold to $f_{OSC-H}$ Operation$^5$</td>
<td>680</td>
<td>$\mu\text{A}$</td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>$I_{VS-Brownout}$</td>
<td>$V_S$ Source Current Threshold to Enable Brownout</td>
<td>160</td>
<td>$\mu\text{A}$</td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>$V_{VS-OVP}$</td>
<td>Output Over-Voltage Protection with $V_S$ Sampling Voltage$^4$</td>
<td>3.10</td>
<td>3.20</td>
<td>3.30</td>
<td>$V$</td>
<td></td>
</tr>
<tr>
<td>$N_{VS-OVP}$</td>
<td>Output Over-Voltage Protection Debounce Cycle Counts$^6$</td>
<td>8</td>
<td>Cycle</td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>$V_{VS-UVLP}$</td>
<td>Output Under-Voltage Protection</td>
<td>1.45</td>
<td>1.55</td>
<td>1.65</td>
<td>$V$</td>
<td></td>
</tr>
<tr>
<td>$t_{UVLP}$</td>
<td>Output Under-Voltage Protection Blanking Time at Startup$^5$</td>
<td>30</td>
<td>45</td>
<td>60</td>
<td>$\text{ms}$</td>
<td></td>
</tr>
<tr>
<td>$N_{UVLP}$</td>
<td>Output Under-Voltage Protection Debounce Cycle Counts$^5$</td>
<td>8</td>
<td>Cycle</td>
<td></td>
<td></td>
<td></td>
</tr>
</tbody>
</table>

#### Current-Sense Section

<table>
<thead>
<tr>
<th>Symbol</th>
<th>Parameter</th>
<th>Conditions</th>
<th>Min.</th>
<th>Typ.</th>
<th>Max.</th>
<th>Unit</th>
</tr>
</thead>
<tbody>
<tr>
<td>$V_{VR}$</td>
<td>Internal Reference Voltage for CC Regulation</td>
<td>2.460</td>
<td>2.500</td>
<td>2.540</td>
<td>$V$</td>
<td></td>
</tr>
<tr>
<td>$V_{CCR}$</td>
<td>Variation Test Voltage on CS Pin for CC Regulation (Non-Inverting Input of Error Amplifier for CC Regulation, EAI)</td>
<td>$V_{CS}=0.375 \text{ V}, V_{COMP}=1.59 \text{ V}, V_S=6 \text{ V}$</td>
<td>2.405</td>
<td>2.430</td>
<td>2.455</td>
<td>$V$</td>
</tr>
<tr>
<td>$K_{CCM}$</td>
<td>Design Parameter in CC Regulation$^4$</td>
<td>12.0</td>
<td>V/V</td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>$V_{CS-LIM}$</td>
<td>Current Limit Threshold Voltage</td>
<td>0.80</td>
<td>0.85</td>
<td>0.90</td>
<td>$V$</td>
<td></td>
</tr>
<tr>
<td>$t_{PD}$</td>
<td>GATE Output Turn-Off Delay</td>
<td>100</td>
<td>200</td>
<td>$\text{ns}$</td>
<td></td>
<td></td>
</tr>
<tr>
<td>$t_{LEB}$</td>
<td>Leading-Edge Blanking Time$^4$</td>
<td>150</td>
<td>200</td>
<td>$\text{ns}$</td>
<td></td>
<td></td>
</tr>
<tr>
<td>$V_{Slope}$</td>
<td>Slope Compensation$^4$</td>
<td>Maximum Duty Cycle</td>
<td>66.6</td>
<td>mV/$\mu$s</td>
<td></td>
<td></td>
</tr>
</tbody>
</table>

#### Constant Current Correction

<table>
<thead>
<tr>
<th>Symbol</th>
<th>Parameter</th>
<th>Conditions</th>
<th>Min.</th>
<th>Typ.</th>
<th>Max.</th>
<th>Unit</th>
</tr>
</thead>
<tbody>
<tr>
<td>$I_{COMP}$</td>
<td>COMP Pin Source Current as $V_S=0.3 \text{ V}$</td>
<td>$V_{CS}=0.3 \text{ V}, V_{FB}=2.5 \text{ V}, V_S=0 \text{ V}$</td>
<td>42</td>
<td>50</td>
<td>58</td>
<td>$\mu\text{A}$</td>
</tr>
</tbody>
</table>

#### GATE Section

<table>
<thead>
<tr>
<th>Symbol</th>
<th>Parameter</th>
<th>Conditions</th>
<th>Min.</th>
<th>Typ.</th>
<th>Max.</th>
<th>Unit</th>
</tr>
</thead>
<tbody>
<tr>
<td>$t_{ON-MIN}$</td>
<td>Minimum On Time</td>
<td>$V_{CS}=0.6 \text{ V}, V_S=0.3 \text{ V}, V_{FB}=1.7 \text{ V}$</td>
<td>450</td>
<td>550</td>
<td>650</td>
<td>$\text{ns}$</td>
</tr>
<tr>
<td>$t_{ON-MIN-LIM}$</td>
<td>Limited Minimum On Time</td>
<td>$V_{CS}=0.6 \text{ V}, V_S=0.5 \text{ V}, V_{FB}=1.7 \text{ V}$</td>
<td>0.95</td>
<td>1.20</td>
<td>1.45</td>
<td>$\mu\text{s}$</td>
</tr>
<tr>
<td>$D_{CYMax}$</td>
<td>Maximum Duty Cycle</td>
<td>$V_{CS}=0.6 \text{ V}, V_S=0 \text{ V}, V_{FB}=4 \text{ V}$</td>
<td>60.0</td>
<td>68.5</td>
<td>77.0</td>
<td>$%$</td>
</tr>
<tr>
<td>$V_{GATE-L}$</td>
<td>Gate Output Voltage Low</td>
<td>0</td>
<td>1.5</td>
<td>$V$</td>
<td></td>
<td></td>
</tr>
<tr>
<td>$V_{DD-PMOS-ON}$</td>
<td>Internal Gate PMOS Driver ON</td>
<td>7.0</td>
<td>7.5</td>
<td>8.0</td>
<td>$V$</td>
<td></td>
</tr>
<tr>
<td>$V_{DD-PMOS-OFF}$</td>
<td>Internal Gate PMOS Driver OFF</td>
<td>9.0</td>
<td>9.5</td>
<td>10.0</td>
<td>$V$</td>
<td></td>
</tr>
<tr>
<td>$t_r$</td>
<td>Rising Time</td>
<td>$V_{CS}=0 \text{ V}, V_S=0 \text{ V}, C_{GATE}=1 \text{ nF}$</td>
<td>100</td>
<td>140</td>
<td>180</td>
<td>$\text{ns}$</td>
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<tr>
<td>$t_f$</td>
<td>Falling Time</td>
<td>$V_{CS}=0 \text{ V}, V_S=0 \text{ V}, C_{GATE}=1 \text{ nF}$</td>
<td>30</td>
<td>50</td>
<td>70</td>
<td>$\text{ns}$</td>
</tr>
<tr>
<td>$V_{GATE-CLAMP}$</td>
<td>Gate Output Clamping Voltage</td>
<td>$V_{DD}=25 \text{ V}$</td>
<td>7.0</td>
<td>7.5</td>
<td>8.0</td>
<td>$V$</td>
</tr>
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### Notes:

4. $T_J$ guaranteed range at 25°C.
5. Design guaranteed.
Typical Performance Characteristics

Figure 6. $V_{DD}$ Turn-On Threshold Voltage ($V_{DD-ON}$) vs. Temperature

Figure 7. $V_{DD}$ Turn-Off Threshold Voltage ($V_{DD-OFF}$) vs. Temperature

Figure 8. Operating Supply Current ($I_{DD-OP}$) vs. Temperature

Figure 9. Burst Mode Operating Supply Current ($I_{DD-Burst}$) vs. Temperature

Figure 10. Operating Frequency, $I_{VS} < I_{VS-L}$ Threshold ($f_{OSC-H}$) vs. Temperature

Figure 11. Operating Frequency while $I_{VS} < I_{VS-H}$ Threshold ($f_{OSC-L}$) vs. Temperature
Typical Performance Characteristics (Continued)

**Figure 12.** Output OVP with $V_s$ Sampling Voltage ($V_{VS-OVP}$) vs. Temperature

**Figure 13.** Output UVP with $V_s$ Sampling Voltage ($V_{VS-UVP}$) vs. Temperature

**Figure 14.** Internal Reference Voltage for CC Regulation ($V_{VR}$) vs. Temperature

**Figure 15.** Variation Test Voltage on CS Pin for CC Regulation ($V_{CCR}$) vs. Temperature

**Figure 16.** Temperature-Independent Bias Current ($I_{TC}$) vs. Temperature

**Figure 17.** Current Limit Threshold Voltage ($V_{CS-LIM}$) vs. Temperature
Typical Performance Characteristics (Continued)

Figure 18. Maximum Duty Cycle ($DCY_{\text{MAX}}$) vs. Temperature

Figure 19. Gate Output Clamping Voltage ($V_{\text{GATE-Clamp}}$) vs. Temperature
**Functional Description**

FAN501 is an offline flyback converter controller that offers constant output voltage (CV) regulation through opto-coupler feedback circuitry and constant output current (CC) regulation with primary-side control. Advanced output current estimation technology allows stable CC regulation regardless of the power stage operation mode: Continuous Conduction Mode (CCM) or Discontinuous Conduction Mode (DCM).

Dual-switching-frequency operation adaptively selects the operational frequency between 85 kHz and 140 kHz according to the line voltage. As a result, the transformer can be fully utilized and high efficiency is maintained over entire line range. A frequency-hopping function is incorporated to reduce EMI noise.

Line voltage information through transformer auxiliary winding is used for dual-switching frequency selection and CC control correction.

mWSaver® technology, including high-voltage startup and ultra-low operating current in Burst Mode, enables system compliance with Energy Star’s 5-star requirement of <30 mW standby power consumption.

Protections such as $V_{DD}$ Over-Voltage Protection ($V_{OVP}$), $V_s$ Over-Voltage Protection ($V_{OVP}$), $V_s$ Under-Voltage Protection ($V_{UVP}$), internal Over-Temperature Protection (OTP), Brownout protection and externally triggered shut-down function improve reliability.

All these innovative technologies allow the FAN501 to offer low total cost, reduced component counts, small size / weight, high conversion efficiency, and high power density for compact charger / adapter applications requiring CV / CC control.

**CV / CC PWM Operation Principle**

Figure 20 shows a simplified CV / CC PWM control circuit of the FAN501. The Constant Voltage (CV) regulation is implemented in the same manner as the conventional isolated power supply, where the output voltage is sensed using a voltage divider and compared with the internal reference of the shunt regulator to generate a compensation signal. The compensation signal is transferred to the primary side through an opto-coupler and scaled down by attenuator AV to generate a COMV signal. This COMV signal is applied to the PWM comparator to determine the duty cycle.

The Constant Current (CC) regulation is implemented internally with primary-side control. The output current estimator calculates the output current using the transformer primary-side current and diode current discharge time. By comparing the estimated output current with internal reference signal, a COMI signal is generated to determine the duty cycle.

These two control signals, COMV and COMI, are compared with an internal sawtooth waveform ($V_{SAW}$) by two PWM comparators to determine the duty cycle. Figure 21 illustrates the outputs of two comparators, combined with an OR gate, to determine the MOSFET turn-off instant. Of COMV and COMI, the lower signal determines the duty cycle. As shown in Figure 21, during CV regulation, COMV determines the duty cycle while COMI is saturated to HIGH level. During CC regulation, COMI determines the duty cycle while COMV is saturated to HIGH level.

**Primary-Side Constant Current Operation**

Figure 22 and Figure 23 show the key waveforms of a flyback converter operating in DCM and CCM, respectively. The output current of each mode is estimated by calculating the average of output diode current over one switching cycle:

$$I_D = \frac{1}{t_s} \int_{t_0}^{t_s} I_D(t) \, dt = \frac{[I_D]_{AREA}}{t_s} \tag{1}$$

The area of output diode current in both DCM and CCM operation can be expressed in a same form, as a product of diode current discharge time ($t_{DIS}$) and diode current at the middle of diode discharge ($I_{DMid}$), such as:

$$[I_D]_{AREA} = I_{DMid} \cdot t_{DIS} \tag{2}$$

In steady state, $I_{DMid}$ can be expressed as:

$$I_{DMid} = \frac{N_p}{N_s} \cdot I_{DSMid} \tag{3}$$

where $I_{DSMid}$ is primary-side current at the middle of MOSFET conduction time and $N_p/N_s$ is primary-to-secondary turn ratio.
The unified output current equation both for DCM and CCM operation is obtained as:

\[ I_D = \frac{N_P}{N_S} \frac{t_{DIS}}{t_S} = N_P \frac{V_{CS,Mid}}{R_{CS}} \]  

(4)

\( V_{CS,Mid} \) is obtained by sampling the current-sense voltage at the middle of the MOSFET conduction time. The diode current discharge time is obtained by detecting the diode current zero-crossing instant. Since the diode current cannot be sensed directly in the primary side, Zero-Crossing Detection (ZCD) is accomplished indirectly by monitoring the auxiliary winding voltage in the primary side. When the diode current reaches zero, the transformer winding voltage begins to drop sharply. To detect the corner voltage, the \( V_S \) is sampled, called \( V_{SH} \), at 85% of diode current discharge time (\( t_{DIS} \)) of the previous switching cycle and compared with the instantaneous \( V_S \) voltage. When instantaneous voltage of the \( V_S \) pin drops below \( V_{SH} \) by more than 200 mV, the ZCD of diode current is obtained, as shown in Figure 24.

The output current can be programmable by setting current sensing resistor as:

\[ R_{CS} = \frac{1}{N_P} \frac{V_{CCR}}{I_D} \frac{1}{N_S} K_{CC} \]  

(5)

where \( V_{CCR} \) is the internal voltage for CC control and \( K_{CC} \) is the IC design parameter, 12 for the FAN501.

The peak transformer current decreases as the switching frequency between 85 kHz and 140 kHz according to the line voltage. It is typical to design the flyback converter to operate in CCM for low line and DCM in high line. Therefore, the peak transformer current decreases as the operation mode changes from CCM to DCM, as shown in Figure 25(a), for single-frequency operation. The transformer is not fully utilized at high line when a single switching frequency is used. The peak transformer current can be maintained almost constant when the flyback converter operates at lower frequency at high line, as illustrated in Figure 25(b). This allows full transformer utilization and improves the efficiency by decreasing the switching losses at high line.

When \( I_{VS} \) is larger than \( I_{VS,H} \) (750 µA), the switching frequency is set at \( f_{OSC,L} \) (85 kHz) in CV Mode. When \( I_{VS} \) is less than \( I_{VS,L} \) (680 µA), the switching frequency is set at \( f_{OSC,H} \) (140 kHz) in CV Mode. For the universal line range, the frequency change should occur between 132 – 180 VAC to avoid the transition within the actual

Figure 24. Operation Waveform for ZCD Function

**Line Voltage Detection and Its Utilization**

The FAN501 indirectly senses line voltage using the current flowing out of the \( V_S \) pin while the MOSFET is turned on, as illustrated in Figure 26 and Figure 27. During the MOSFET turn-on period, auxiliary winding voltage, \( V_{Aux} \), reflects input bulk capacitor voltage, \( V_{BLK} \), by the transformer coupling between primary and auxiliary. During MOSFET conduction time, the line voltage detector clamps the \( V_S \) pin voltage ~0.5 V and the current, \( I_{VS} \), flowing from the \( V_S \) pin is expressed as:

\[ I_{VS} = \frac{N_A}{N_P} \frac{V_{BLK}}{R_{VS1}} + \frac{0.5}{R_{VS1}/R_{VS2}} \]  

(6)

Typically, the second term in Equation (6) can be ignored because it is much smaller than the first term. The current, \( I_{VS} \), is approximately proportional to the line voltage, calculated as:

\[ I_{VS} = \frac{N_A}{N_P} \frac{V_{BLK}}{R_{VS1}} \]  

(7)

The \( I_{VS} \) current, reflecting the line voltage information, is used for dual switching frequency operation, CC control correction weighting, and brownout protection; as illustrated in Figure 26.

**Dual Switching Frequency**

The FAN501 changes the switching frequency between 85 kHz and 140 kHz according to the line voltage. It is typical to design the flyback converter to operate in CCM for low line and DCM in high line. Therefore, the peak transformer current decreases as the operation mode changes from CCM to DCM, as shown in Figure 25(a), for single-frequency operation. The transformer is not fully utilized at high line when a single switching frequency is used. The peak transformer current can be maintained almost constant when the flyback converter operates at lower frequency at high line, as illustrated in Figure 25(b). This allows full transformer utilization and improves the efficiency by decreasing the switching losses at high line.
operation range. It is typical to design the voltage divider for the VS pin such that frequency change occurs at 170 V\textsubscript{AC} (V\textsubscript{DC} 170 V\textsubscript{AC} = 240 V); calculated as:

\[ R_{VS1} = \frac{N_s}{N_p} \cdot \frac{240}{I_{VS-H}} \]  
(8)

With the value of \( R_{VS1} \) determined from Equation (8), the switching frequency drops to 85 kHz as line voltage increases above 170 V\textsubscript{AC}, while switching frequency increases to 140 kHz, as line voltage drops <155 V\textsubscript{AC}.

(b) Dual frequency operation

Figure 25. Peak Switch Current, Single- and Dual-Frequency Operation

Brownout Protection
Line voltage information is also used for brownout protection. When the \( I_{VS} \) current out of the VS pin during the MOSFET conduction time is less than 160 \( \mu \text{A} \) for longer than 30 ms, the brownout protection is triggered. When setting \( R_{VS1} \) as calculated in Equation (8), the brownout level is set at 30 V\textsubscript{AC}.

Figure 26. Line Voltage Detection Circuit

Maximum Power Limit by Precision CC Control
Primary-side current-sensing voltage is used to estimate the output current for CC regulation. However, the actual output current regulation is also affected by the turn-off delay of the MOSFET, as illustrated in Figure 28. While FAN501 samples the CS pin voltage at the half on-time of gate drive signal, the actual turn-off is delayed by the MOSFET gate charge and driving current resulting in peak current detection error as:

\[ \Delta I_{DS}^{PK} = \frac{V_{CSF}}{L_m} t_{OFF-DLY} \]  
(9)

where \( L_m \) is the primary side magnetic inductance.

As can be seen, the error is proportional to the line voltage. FAN501 has an internal correction function to improve CC regulation, as shown in Figure 29. Line information is obtained through the line voltage detector as shown in Figure 26 and Figure 27 and this information is used for the CC control correction. The correction gain can be programmed using external resistor \( R_{COMP} \) on the COMP pin. This correction current, \( I_{LVF} \), flows through internal resistor, \( R_{LVF} \), and external resistor, \( R_{CSF} \), to introduce offset voltage on current sensing voltage. Thus, the primary current detection error affected by line voltage and turn-off delay is corrected for better CC regulation. The \( R_{COMP} \) resistor can be calculated as:

\[ R_{COMP} = \frac{N_p}{N_s} \cdot \frac{R_{CS}}{R_{LVF} + R_{CSF}} \cdot \frac{R_{VS1}}{R_{OFF-DLY} \cdot L_m} \cdot K_{COMP} \]  
(10)

where \( R_{LVF} \) is the internal resistor on the IC, which is 2.0 k\( \Omega \), and \( K_{COMP} \) is the design factor of the IC, which is 3.745 M\( \Omega \).
The turn-off delay should be obtained by measuring the time between the falling edge and actual turn-off instant of MOSFET, as illustrated in Figure 28.

Figure 28. CC Control Correction Concept

**Pulse-by-Pulse Current Limit**

Since the peak transformer current is controlled by a feedback loop, the peak transformer current is not properly controlled when the feedback loop is saturated to HIGH, which typically occurs under startup or overload conditions. To limit the current, a pulse-by-pulse current limit forces the gate drive signal to turn off when the CS pin voltage reaches the current-limit threshold (VCS-LIM) in normal operation.

**Burst Mode Operation**

The power supply enters Burst Mode at no-load or extremely light-load condition. As shown in Figure 30, when VFB drops below VFB-Burst-L, the PWM output shuts off and the output voltage drops at a rate dependent on load current. This causes the feedback voltage to rise. Once VFB exceeds VFB-Burst-H, the internal circuit starts to provide a switching pulse. The feedback voltage then falls and the process repeats. In this manner, Burst Mode alternately enables and disables switching of the MOSFET to reduce the switching losses in Standby Mode. In Burst Mode, the operating current is reduced from 3.5 mA to 250 µA to minimize power consumption.

**Frequency Hopping**

EMI reduction is accomplished by frequency hopping, which spreads the energy over a wider frequency range than the bandwidth of the EMI test equipment, allowing compliance with EMI limitations.

**Slope Compensation**

The sensed voltage across the current-sense resistor is used for current-mode control and pulse-by-pulse current limiting. A synchronized ramp signal with a positive slope is added to the current-sense information at each switching cycle, improving noise immunity during current mode control and avoiding sub-harmonic oscillation during CCM operation.

**Leading-Edge blanking (LEB)**

Each time the power MOSFET is switched on, a turn-on spike occurs at the sense resistor. To avoid premature termination of the switching pulse by the spike, a 150 ns leading-edge blanking time is incorporated. Conventional RC filtering can therefore be omitted. During this blanking period, the current-limit comparator is disabled and it cannot switch off the gate driver.

**Noise Immunity**

Noise from the current sense or the control signal can cause significant pulse-width jitter. Though slope compensation helps alleviate this problem, precautions should be taken to improve the noise immunity. Good placement and layout practices are important. Avoid long PCB traces and component leads and locate bypass capacitor as close to the PWM IC as possible.

**High Voltage (HV) Startup**

Figure 31 shows the high-voltage (HV) startup circuit for FAN501 applications. The JFET is used to internally implement the high-voltage current source (see Figure 32 for characteristics). Technically, the HV pin can be directly connected to voltage (VBLK) on an input bulk capacitor. To improve reliability and surge immunity, however, it is typical to use a ~100 kΩ resistor between the HV pin and bulk capacitor voltage. The actual HV current with a given bulk capacitor voltage and startup resistor is determined by the intersection of V-I characteristics line and load line, as shown in Figure 32.
During startup, the internal startup circuit is enabled and the bulk capacitor voltage supplies the current, \( i_{HV} \), to charge the hold-up capacitor, \( C_{VDD} \), through \( R_{HV} \). When \( V_{DD} \) reaches \( V_{DD-ON} \), the internal HV startup circuit is disabled and the IC starts PWM switching. Once the HV startup circuit is disabled, the energy stored in \( C_{VDD} \) should supply the IC operating current until the transformer auxiliary winding voltage reaches the nominal value. Therefore, \( C_{VDD} \) should be designed to prevent \( V_{DD} \) from dropping to \( V_{DD-OFF} \) before the auxiliary winding builds up enough voltage to supply \( V_{DD} \).

![HV Startup Circuit](image)

**Figure 31. HV Startup Circuit**

**Figure 32. V-I Characteristic of HV Pin**

**Protections**

The protection functions include \( V_{DD} \) Over-Voltage Protection (\( V_{DD-OVP} \)), brownout protection, \( V_{S} \) Over-voltage Protection (\( V_{S-OVP} \)), \( V_{S} \) Under-Voltage Protection (\( V_{S-UVP} \)), internal Over-Temperature Protection (OTP), and externally triggered shutdown (SD) protection. The \( V_{DD-OVP} \) and brownout protection are implemented as Auto-Restart Mode. \( V_{S-OVP} \), OTP, and SD protections are implemented as Latch Mode.

When an Auto-Restart Mode protection is triggered, switching is terminated and the MOSFET remains off, causing \( V_{DD} \) to drop. When \( V_{DD} \) drops to the \( V_{DD} \) turn-off voltage of 5.8 V, the internal startup circuit is enabled without resetting the protection and the supply current drawn from HV pin charges the hold-up capacitor. Since the protection is not reset, the IC does not resume PWM switching even when \( V_{DD} \) reaches the turn-on voltage of 17.5 V, disabling HV startup circuit. Then \( V_{DD} \) drops again down to 5.8 V. In this manner, Latch Mode protection alternately charges and discharges \( V_{DD} \) until there is no more energy in DC link capacitor. The protection is reset when \( V_{DD} \) drops to 2.5 V, which is allowed only after power supply is unplugged from the AC line, as shown in Figure 34.

![Auto-Restart Mode Operation](image)

**Figure 33. Auto-Restart Mode Operation**

![Latch Mode Operation](image)

**Figure 34. Latch Mode Operation**
**V_{DD} Over-Voltage-Protection**

V_{DD} over-voltage protection prevents damage from over-voltage exceeding the IC voltage rating. When V_{DD} exceeds 28 V due to an abnormal condition, protection is triggered. This protection is typically caused by an open circuit in the secondary-side feedback network.

**Brownout Protection**

Brownout protection is implemented through line voltage detection circuit using the auxiliary winding, as shown in Figure 26 and Figure 27. When the current flowing out of the VS pin during the MOSFET conduction time is smaller than 160 μA for longer than 30 ms, the brownout protection is triggered.

**Over-Temperature Protection (OTP)**

If the junction temperature exceeds 140°C (T_{OTP}), the internal temperature-sensing circuit shuts down PWM output and enters Latch Mode protection.

**V_{S} Under-Voltage Protection (V_{S} UVP)**

Generally, the fold-back point in CC regulation as output drops is determined by the V_{DD-OFF} level. Thus, the fold-back level mainly depends on the characteristics of the V_{DD} diode and transformer. V_{S} under-voltage protection provides accurate fold-back point control to minimize the effect from the external component tolerance. Figure 35 shows the internal circuit for V_{S} UVP. By sampling the auxiliary winding voltage on the VS pin around the end of diode conduction time, the output voltage is indirectly sensed. When V_{S} sampling voltage is less than V_{VS-UVP} (1.55 V) longer than debounce cycles N_{VS-UVP}, V_{S} UVP is triggered and the FAN501 enters Auto-Restart Mode.

To avoid V_{S} UVP triggering during the startup sequence, a startup blanking time, t_{VS-UVP-BLANK} (45 ms) in included for system power on. For VS pin voltage divider design, R_{VS1} is obtained from Equation (11) and R_{VS2} is determined by V_{S} UVP protection function as:

\[
R_{VS2} = R_{VS1} \cdot \left( V_{O-UVP} \cdot \frac{N_A}{N_S} - 1 \right)^{-1} \quad (11)
\]

where V_{O-UVP} is the output under-voltage protection level.

**V_{S} Over-Voltage-Protection (V_{S} OVP)**

V_{S} over-voltage protection prevents damage caused by output over-voltage condition. Figure 36 shows the internal circuit of V_{S} OVP. When abnormal system conditions occur that cause V_{S} sampling voltage to exceed V_{VS-OVP} (3.2 V) for more than debounce switching cycles (N_{VS-OVP}), PWM pulses are disabled and the FAN501 enters Latch Mode protection. V_{S} over-voltage conditions are usually caused by an open circuit in the secondary-side feedback network or a fault condition in the VS pin voltage divider resistors.

**Externally Triggered Shutdown**

By pulling the SD pin voltage below threshold voltage, V_{SD-TH} (1.0 V), shutdown can be externally triggered and the FAN501 enters Latch Mode protection. It can be also used for external OTP protection by connecting an NTC thermistor between the shutdown (SD) programming pin and ground. An internal constant current source, I_{SD} (100 μA), introduces voltage drop across the thermistor. Resistance of the NTC thermistor becomes smaller as the ambient temperature increases, which reduces the voltage drops across the thermistor. When the voltage of the SD pin is less than threshold voltage V_{SD-TH} (1.0 V), OTP protection is triggered.
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