The NB650/NB650H is fully-integrated, high-frequency, synchronous, rectified, step-down, switch-mode converters with dynamic-output-voltage control. It offers a very compact solution to achieve 6A of continuous output current over a wide input supply range, and has excellent load and line regulation. The NB650/NB650H operates at high efficiency over a wide output-current-load range.

Constant-On-Time control mode provides fast transient response and eases loop stabilization.

2-bit VID inputs support changing the output voltage on-the-fly.

Full protection features include short-circuit protection, over-current protection, over-voltage protection, under-voltage protection, and thermal shut down.

The NB650/NB650H requires a minimal number of readily-available standard external components, and is available in a space-saving 3mm×4mm QFN17 package.
ORDERING INFORMATION

<table>
<thead>
<tr>
<th>Part Number</th>
<th>Package</th>
<th>Top Marking</th>
</tr>
</thead>
<tbody>
<tr>
<td>NB650GL*</td>
<td>QFN17 (3 x 4mm)</td>
<td>NB650</td>
</tr>
<tr>
<td>NB650HGL**</td>
<td></td>
<td>NB650H</td>
</tr>
</tbody>
</table>

* For Tape & Reel, add suffix –Z (e.g. NB650GL–Z)
** For Tape & Reel, add suffix –Z (e.g. NB650HGL–Z)

ABSOLUTE MAXIMUM RATINGS (1)

Supply Voltage $V_{IN}$ ....................................... 28V
$V_{SW}$ ........................................ -0.3V to $V_{IN}$ + 0.3V
$V_{BST}$ ........................................... -3V to $V_{IN}$ + 3V for <30ns
All Other Pins ........................................... -0.3V to +6V

Continuous Power Dissipation  $(T_A = +25^\circ C)$ (2)
QFN17 ...................................................... 2.4W

Junction Temperature ......................... 150°C
Lead Temperature ................................. 260°C
Storage Temperature ......................... -65°C to +150°C

Recommended Operating Conditions (3)

Supply Voltage $V_{IN}$ ......................... 4.5V to 22.5V
Output Voltage $V_{OUT}$ ....................... 0.6V to 13V
Operating Junction Temp. $(T_J)$ ............ -40°C to +125°C

Thermal Resistance (4)  $\theta_{JA}$ $\theta_{JC}$
QFN17(3 x 4mm) ......................... 52 .... 11 .. °C/W

Notes:
1) Exceeding these ratings may damage the device.
2) The maximum allowable power dissipation is a function of the maximum junction temperature $T_J(MAX)$, the junction-to-ambient thermal resistance $\theta_{JA}$, and the ambient temperature $T_A$. The maximum allowable continuous power dissipation at any ambient temperature is calculated by $P_D(MAX) = (T_J(MAX)-T_A)/\theta_{JA}$. Exceeding the maximum allowable power dissipation will cause excessive die temperature, and the regulator will go into thermal shutdown. Internal thermal shutdown circuitry protects the device from permanent damage.
3) The device is not guaranteed to function outside of its operating conditions.
4) Measured on JESD51-7, 4-layer PCB.
## ELECTRICAL CHARACTERISTICS

\( V_{\text{IN}} = 12\text{V}, \ T_{J} = +25^\circ\text{C}, \) unless otherwise noted.

<table>
<thead>
<tr>
<th>Parameters</th>
<th>Symbol</th>
<th>Condition</th>
<th>Min</th>
<th>Typ</th>
<th>Max</th>
<th>Units</th>
</tr>
</thead>
<tbody>
<tr>
<td>Input Supply Current (Shutdown)</td>
<td>( I_{\text{IN}} )</td>
<td>( V_{\text{EN}} = 0\text{V} )</td>
<td>0</td>
<td></td>
<td></td>
<td>( \mu\text{A} )</td>
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<tr>
<td>Input Supply Current (Quiescent)</td>
<td>( I_{\text{IN}} )</td>
<td>( V_{\text{EN}} = 2\text{V}, V_{\text{FB}} = 0.65\text{V} )</td>
<td>400</td>
<td></td>
<td></td>
<td>( \mu\text{A} )</td>
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<td>Switch Leakage</td>
<td>( \text{SW}_{\text{LKG}} )</td>
<td>( V_{\text{EN}} = 0\text{V}, V_{\text{SW}} = 0\text{V} ) or ( 12\text{V} )</td>
<td>0</td>
<td>1</td>
<td></td>
<td>( \mu\text{A} )</td>
</tr>
<tr>
<td>Current Limit</td>
<td>( I_{\text{LIMIT}} )</td>
<td>( t_{\text{ON}} &gt; 200\text{ns} )</td>
<td>8</td>
<td>10</td>
<td></td>
<td>( \text{A} )</td>
</tr>
<tr>
<td>One-Shot On Time</td>
<td>( t_{\text{ON}} )</td>
<td>( R_{\text{FREQ}} = 200\text{k}\Omega, V_{\text{OUT}} = 1.2\text{V} )</td>
<td>200</td>
<td></td>
<td></td>
<td>( \text{ns} )</td>
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<tr>
<td>Minimum Off Time</td>
<td>( t_{\text{OFF}} )</td>
<td>( R_{\text{FREQ}} = 200\text{k}\Omega )</td>
<td>100</td>
<td></td>
<td></td>
<td>( \text{ns} )</td>
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<tr>
<td>Fold-back Off Time(5)</td>
<td>( t_{\text{FB}} )</td>
<td>( \text{ILIM} = 1 )</td>
<td>1.2</td>
<td></td>
<td></td>
<td>( \mu\text{s} )</td>
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<tr>
<td>OCP hold-off time(5)</td>
<td>( t_{\text{OC}} )</td>
<td>( \text{ILIM} = 1 )</td>
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<td>( \mu\text{s} )</td>
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<tr>
<td>Feedback Voltage</td>
<td>( V_{\text{FB}} )</td>
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<td>594</td>
<td>600</td>
<td>606</td>
<td>( \text{mV} )</td>
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<tr>
<td>Feedback Current</td>
<td>( I_{\text{FB}} )</td>
<td>( V_{\text{FB}} = 600\text{mV} )</td>
<td>10</td>
<td>100</td>
<td></td>
<td>( \text{nA} )</td>
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<tr>
<td>Soft Start Charging Current</td>
<td>( I_{\text{SS}} )</td>
<td>( V_{\text{SS}} = 0\text{V} )</td>
<td>10</td>
<td></td>
<td></td>
<td>( \mu\text{A} )</td>
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<tr>
<td>Soft Stop Charging Current</td>
<td>( I_{\text{SS}} )</td>
<td>( V_{\text{SS}} = 0.6\text{V} )</td>
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<td></td>
<td></td>
<td>( \mu\text{A} )</td>
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<tr>
<td>EN Input Low Voltage</td>
<td>( V_{\text{IL}} )  ( V_{\text{EN}} )</td>
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<td>0.4</td>
<td></td>
<td></td>
<td>( \text{V} )</td>
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<tr>
<td>EN Input High Voltage</td>
<td>( V_{\text{IH}} )  ( V_{\text{EN}} )</td>
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<td>2</td>
<td></td>
<td></td>
<td>( \text{V} )</td>
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<tr>
<td>EN Input Current</td>
<td>( I_{\text{EN}} )  ( V_{\text{EN}} )</td>
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<td>1.5</td>
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<td>( \mu\text{A} )</td>
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<td>OVP Feedback Threshold</td>
<td>( V_{\text{FB-UV}} )</td>
<td></td>
<td>0.8</td>
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<td></td>
<td>( \text{V} )</td>
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<tr>
<td>UVP Feedback Threshold(6)</td>
<td>( V_{\text{FB-OV}} )</td>
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<td>0.4</td>
<td></td>
<td></td>
<td>( \text{V} )</td>
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<tr>
<td>VID Inputs Low Voltage</td>
<td>( V_{\text{IL}} )  ( V_{\text{VID}} )</td>
<td></td>
<td>0.4</td>
<td></td>
<td></td>
<td>( \text{V} )</td>
</tr>
<tr>
<td>VID Inputs High Voltage</td>
<td>( V_{\text{IH}} )  ( V_{\text{VID}} )</td>
<td></td>
<td>2</td>
<td></td>
<td></td>
<td>( \text{V} )</td>
</tr>
<tr>
<td>VID Inputs Current</td>
<td>( I_{\text{VID}} )</td>
<td></td>
<td>0</td>
<td></td>
<td></td>
<td>( \mu\text{A} )</td>
</tr>
<tr>
<td>Equivalent FB Slew Rate During VID On-The-Fly(5)</td>
<td>( SR_{\text{FB}} )</td>
<td></td>
<td>( \pm 20 )</td>
<td></td>
<td></td>
<td>( \text{mV/\mu s} )</td>
</tr>
<tr>
<td>VID Switch On Resistance(5)</td>
<td>( V_{\text{IDS-ON}} )</td>
<td></td>
<td>100</td>
<td></td>
<td></td>
<td>( \Omega )</td>
</tr>
<tr>
<td>Power Good Rising Threshold</td>
<td>( P_{G_{\text{VH-Hi}}} )</td>
<td></td>
<td>0.9</td>
<td>( V_{\text{FB}} )</td>
<td></td>
<td></td>
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<tr>
<td>Power Good Falling Threshold</td>
<td>( P_{G_{\text{VH-Lo}}} )</td>
<td></td>
<td>0.85</td>
<td>( V_{\text{FB}} )</td>
<td></td>
<td></td>
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<tr>
<td>Power Good Delay</td>
<td>( P_{G_{\text{t}}} )</td>
<td></td>
<td>0.5</td>
<td></td>
<td></td>
<td>( \text{ms} )</td>
</tr>
<tr>
<td>Power Good Sink Current Capability</td>
<td>( V_{\text{PG}} )</td>
<td>( \text{Sink} ) ( 4\text{mA} )</td>
<td>0.4</td>
<td></td>
<td></td>
<td>( \text{V} )</td>
</tr>
<tr>
<td>Power Good Leakage Current</td>
<td>( I_{\text{PG LEAK}} )</td>
<td>( V_{\text{PG}} = 3.3\text{V} )</td>
<td>10</td>
<td></td>
<td></td>
<td>( \text{nA} )</td>
</tr>
<tr>
<td>Standby Mode Delay Time(5)</td>
<td>( t_{\text{STANDBY}} )</td>
<td></td>
<td>12</td>
<td></td>
<td></td>
<td>( \mu\text{s} )</td>
</tr>
<tr>
<td>( V_{\text{IN}} ) Under Voltage Lockout Threshold Rising</td>
<td>( \text{INU}<em>{V</em>{\text{th}}} )</td>
<td></td>
<td>4</td>
<td></td>
<td></td>
<td>( \text{V} )</td>
</tr>
<tr>
<td>( V_{\text{IN}} ) Under Voltage Lockout Threshold Hysteresis</td>
<td>( \text{INU}_{\text{HY}} )</td>
<td></td>
<td>800</td>
<td></td>
<td></td>
<td>( \text{mV} )</td>
</tr>
<tr>
<td>Thermal Shutdown(5)</td>
<td>( T_{\text{SD}} )</td>
<td></td>
<td>150</td>
<td></td>
<td></td>
<td>( ^\circ\text{C} )</td>
</tr>
</tbody>
</table>

**Note:**

5) Not tested. Not guaranteed.
# PIN FUNCTIONS

<table>
<thead>
<tr>
<th>QFN17 Pin #</th>
<th>Name</th>
<th>Description</th>
</tr>
</thead>
<tbody>
<tr>
<td>1,2</td>
<td>SW</td>
<td>Switch Output. Connect using wide PCB traces.</td>
</tr>
<tr>
<td>3</td>
<td>BST</td>
<td>Bootstrap. Requires a capacitor between SW and BST to form a floating supply across the high-side switch driver.</td>
</tr>
<tr>
<td>4</td>
<td>PG</td>
<td>Power Good. Output is an open drain and is high if the output voltage exceeds 90% of the nominal voltage. There is a delay from $FB \geq 90% \times V_{ref}$ to PG goes high.</td>
</tr>
<tr>
<td>5</td>
<td>EN</td>
<td>EN=1 to enable. For automatic start-up, connect to VIN with a 100kΩ resistor.</td>
</tr>
<tr>
<td>6,7</td>
<td>VID1, VID2</td>
<td>VID inputs. Control signals for the output-voltage scaling. Acts as the control signals for the internal VID switches. Usually uses an external resistor in parallel with the low-side FB resistor. Changing the VID ON/OFF state changes the FB divider scaling and result in different output voltages.</td>
</tr>
<tr>
<td>8</td>
<td>VCC</td>
<td>Internal LDO output. The power supply of the internal control circuits. Decouple with 1μF capacitor.</td>
</tr>
<tr>
<td>9,10</td>
<td>GND</td>
<td>System Ground. The reference ground of the regulated output voltage. Layout requires extra care.</td>
</tr>
<tr>
<td>11</td>
<td>IN</td>
<td>Supply Voltage. Operates from a 4.5V-to-28V input rail. Requires C1 to decouple the input rail. Connect using wide PCB traces.</td>
</tr>
<tr>
<td>12</td>
<td>AGND</td>
<td>Analog Ground.</td>
</tr>
<tr>
<td>13</td>
<td>FB</td>
<td>Feedback. Connect to the tap of an external resistor divider from the output to GND to set the output voltage.</td>
</tr>
<tr>
<td>14,15</td>
<td>RFB2, RFB1</td>
<td>Drain of the internal VID switches. Typically uses an external resistor in parallel with the low-side FB resistor along with the internal VID switch to change the ON/OFF state of the VID switching to change the FB divider scaling and result in different output voltages.</td>
</tr>
<tr>
<td>16</td>
<td>SS</td>
<td>Soft-Start. Connect an external capacitor to program the soft-start time for the switch-mode regulator.</td>
</tr>
<tr>
<td>17</td>
<td>FREQ</td>
<td>Frequency Set during CCM. The input voltage and the frequency-set resistor between the IN and FREQ pin determines the ON period. For best results, use an ON period longer than 200ns. Decouple with a 1nF capacitor.</td>
</tr>
</tbody>
</table>
TYPICAL PERFORMANCE CHARACTERISTICS

$V_{IN}=12V$, $V_{OUT}=1.05V$, $L=1\mu H$, $T_A=+25^\circ C$, unless otherwise noted.

**Efficiency**

- $F_{SW}=540kHz$
- $F_{SW}=300kHz&540kHz$
- $V_{OUT}=5V$, $F_{SW}=550kHz$

**Line Regulation**

- $I_{OUT}=3A$
- $I_{OUT}=0A$
- $I_{OUT}=6A$

**Load Regulation**

- $V_{IN}=21V$
- $V_{IN}=12V$
- $V_{IN}=5V$

**Case Temperature Rise vs. Output Current**

**Frequency vs. Temperature**

- $I_{OUT}=6A$

**Frequency vs. $V_{IN}$**

- $I_{OUT}=6A$

**Frequency vs. Load Current**

- $I_{OUT}=6A$
TYPICAL PERFORMANCE CHARACTERISTICS (continued)

$V_{\text{IN}}=12\text{V}$, $V_{\text{OUT}}=1.05\text{V}$, $L=1\mu\text{H}$, $T_A=+25^\circ\text{C}$, unless otherwise noted.

**Input & Output Ripple**

- **$I_{\text{OUT}} = 0\text{A}$**
- **$I_{\text{OUT}} = 0.5\text{A}$**
- **$I_{\text{OUT}} = 6\text{A}$**

**Power Good Through $V_{\text{IN}}$ Start-Up**

- **$I_{\text{OUT}} = 6\text{A}$**

**Power Good Through $V_{\text{IN}}$ Shutdown**

- **$I_{\text{OUT}} = 6\text{A}$**

**Start-Up Through $V_{\text{IN}}$**

- **$I_{\text{OUT}} = 6\text{A}$**

**Shutdown Through $V_{\text{IN}}$**

- **$I_{\text{OUT}} = 0\text{A}$**

- **$I_{\text{OUT}} = 6\text{A}$**

$V_{\text{IN}}(\text{AC})$ 50mV/div.
$V_{\text{IN}}(\text{AC})$ 20mV/div.
$V_{\text{IN}}(\text{AC})$ 20mV/div.
$V_{\text{SW}}$ 10V/div.
$V_{\text{SW}}$ 100mV/div.
$V_{\text{OUT}}(\text{AC})$ 20mV/div.
$V_{\text{OUT}}(\text{AC})$ 10mV/div.
$V_{\text{OUT}}(\text{AC})$ 10mV/div.
$V_{\text{SW}}$ 2A/div.
$I_L$ 2A/div.
$I_L$ 5A/div.
$I_L$ 1A/div.
$I_L$ 5A/div.
$V_{\text{IN}}$ 5V/div.
$V_{\text{IN}}$ 5V/div.
$V_{\text{IN}}$ 5V/div.
$V_{\text{IN}}$ 5V/div.
$V_{\text{IN}}$ 5V/div.
$V_{\text{IN}}$ 5V/div.
$V_{\text{OUT}}$ 500mV/div.
$V_{\text{OUT}}$ 500mV/div.
$V_{\text{OUT}}$ 500mV/div.
$V_{\text{OUT}}$ 500mV/div.
$V_{\text{OUT}}$ 500mV/div.
$V_{\text{OUT}}$ 1V/div.
$V_{\text{OUT}}$ 1V/div.
$V_{\text{OUT}}$ 1V/div.
$V_{\text{OUT}}$ 1V/div.
$V_{\text{OUT}}$ 1V/div.
$V_{\text{SW}}$ 10V/div.
$V_{\text{SW}}$ 10V/div.
$V_{\text{SW}}$ 10V/div.
$V_{\text{SW}}$ 10V/div.
$V_{\text{SW}}$ 10V/div.
$V_{\text{IN}}$ 10V/div.
$V_{\text{IN}}$ 10V/div.
$V_{\text{IN}}$ 10V/div.
$V_{\text{IN}}$ 10V/div.
$V_{\text{IN}}$ 10V/div.
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$V_{\text{IN}}$ 10V/div.
$V_{\text{IN}}$ 10V/div.
$V_{\text{IN}}$ 10V/div.
$V_{\text{IN}}$ 10V/div.
$V_{\text{IN}}$ 10V/div.
$V_{\text{IN}}$ 10V/div.
TYPICAL PERFORMANCE CHARACTERISTICS (continued)

**VIN=12V, VOUT=1.05V, L=1µH, TA=+25°C, unless otherwise noted.**

**Start-Up Through EN**

- **IOUT = 0A**
- **IOUT = 6A**
- **IOUT = 0A**

**Shutdown Through EN**

- **IOUT = 6A**
- **IOUT = 6A**
- **IOUT = 0A**

**Short Circuit Protection**

- **NB650, Latch-Off Version**

**OCP Protection**

- **NB650, Latch-Off Version**

**Transient**

- **IOUT = 0.6A-5.4A@2.5A/µs, FSW = 530kHz, COUT = 3x22µF**

**VID On-the-fly**

- **IOUT = 0.3A**
- **FVID1 = 1kHz, FVID2 = 0.5kHz, VOUT = 1.05V/1.1V/1.15V/1.2V**

**VID On-the-fly**

- **IOUT = 6A**
- **FVID1 = 1kHz, FVID2 = 0.5kHz, VOUT = 1.05V/1.1V/1.15V/1.2V**
Figure 1: Functional Block Diagram
OPERATION

PWM Operation

The NB650/NB650H is a fully-integrated, synchronous, rectified, step-down, switch-mode converter with dynamic output voltage control. It offers a very compact solution to achieve a 6A continuous output current over a wide input supply range, with excellent load and line regulation. The NB650/NB650H operates at high efficiency over a wide output current load range.

Constant-on-time (COT) provides a fast transient response and easy loop stabilization. At the beginning of each cycle, the high-side MOSFET (HS-FET) turns on when the feedback voltage (VFB) falls below the reference voltage (VREF), which indicates an insufficient output voltage. The input voltage and the frequency-set resistor determine the ON as follows:

\[ t_{\text{ON}}(\text{ns}) = \frac{9.6 \times R_{\text{FREQ}}(\text{k}\Omega)}{V_{\text{IN}}(\text{V}) - 0.4} + t_{\text{DELAY1}}(\text{ns}) \]  

(1)

Where \( t_{\text{DELAY1}} \) is the 20ns delay of a comparator in the tON module.

For best results, select \( t_{\text{ON}} \geq 120\text{ns}. \)

After the ON period elapses, the HS-FET turns off to enter the OFF state. The part turns ON again when VFB drops below VREF. By repeating this operation, the converter regulates the output voltage. The integrated low-side MOSFET (LS-FET) turns on when the HS-FET is OFF to minimize conduction loss. There is a dead short between input and GND (shoot-through) if both HS-FET and LS-FET turn on at the same time. An internally-generated dead-time (DT) between HS-FET OFF and LS-FET ON or LS-FET OFF and HS-FET OFF avoids shoot-through.

Heavy-Load Operation

As shown in Figure 2, the HS-FET and LS-FET repeatedly turn on/off when the output current is high, and the inductor current never goes to zero. It’s called continuous-conduction-mode (CCM) operation. In CCM operation, the switching frequency (fSW) is fairly constant.

Light-Load Operation

When the load current decreases, the NB650/NB650H automatically reduces the switching frequency to maintain high efficiency. Figure 3 shows the light-load operation. VFB does not reach VREF when the inductor current approaches zero. As the output current drops from heavy-load condition, the inductor current also decreases and eventually approaches zero. The LS-FET driver enters a tri-state (high-Z) whenever the inductor current reaches zero. A current modulator takes control of the LS-FET and limits the inductor current to less than 600μA to slowly discharge the output capacitors to GND through LS-FET as well as R1 and R2A, R2B and R2C. The HS-FET does not turn ON as frequently as in heavy-load condition. As a result, the efficiency at light-load condition increases greatly. This operation mode is also called skip mode.

As the output current increases from the light-load condition, the time period within which the current modulator regulates becomes shorter. As the part exits light-load mode, the HS-FET turns on more frequently to increase the switching frequency. The output current reaches critical when the current modulator time is zero. The
following equation determines the critical level of the output current:

\[ I_{OUT} = \frac{(V_{IN} - V_{OUT}) \times V_{OUT}}{2 \times L \times f_{SW} \times V_{IN}} \]  

When the output current exceeds the critical level, light load mode turns into PWM mode, and the switching frequency stays fairly constant over the output current range.

**Switching Frequency**  
The NB650/NB650H uses constant-on-time (COT) control, and has no dedicated internal oscillator. The input voltage is feed-forwarded to the on-time one-shot timer through the resistor \( R_{FREQ} \). The duty ratio is kept as \( V_{OUT}/V_{IN} \). Hence, the switching frequency is fairly constant over the input voltage range. The switching frequency can be set as follows:

\[ f_{SW} (kHz) = \left[ \frac{9.6 \times R_{FREQ} (k\Omega)}{V_{IN} (V) - 0.4} + t_{DELAY1} (ns) \right] \times 10^6 \]  

Where \( t_{DELAY2} \) is another comparator delay of about 40ns.

**Frequency vs. \( R_{FREQ} \)**  
![Graph showing frequency vs. \( R_{FREQ} \)]

**Jitter and FB Ramp Slope**  
Figure 5 and Figure 6 show jitter in both PWM and skip modes. When there is noise in the \( V_{FB} \) downward slope, the ON time of HS-FET deviates from its intended level and produces jitter. There is a relationship between a system’s stability and the steepness of the \( V_{FB} \) ripple’s downward slope: The steepness of the \( V_{FB} \) ripple’s slope dominates in noise immunity. The magnitude of the \( V_{FB} \) ripple doesn’t directly affect the noise immunity.

![Figure 5: Jitter in PWM Mode]

**Ramp with Large ESR Cap**  
When using POSCAPs or other types of capacitors with larger ESR as output capacitors, the ESR ripple dominates the output ripple, and the slope on the FB is ESR-related. Figure 7 shows an equivalent circuit in PWM mode with the HS-FET off and without an external ramp circuit. The application section includes design steps for large ESR capacitors.

![Figure 7: Equivalent circuit showing ESR related slope]

**NB650/NB650H is optimized to operate at high switching frequencies at high efficiency. Higher switching frequencies allow for smaller LC filter components to reduce system PCB space.**
To realize the stability without the use of an external ramp, select an ESR value as follows:

\[ R_{ESR} \geq \frac{t_{SW} + 0.7 \times \pi}{2 C_{OUT}} \]  

(4)

Where \( t_{SW} \) is the switching period.

**Ramp with Small ESR Capacitor**

The ESR ripple when using ceramic output capacitors is not high enough to stabilize the system and requires an external compensation ramp. The application section includes a description of designing with small ESR capacitors.

And R2 is the equivalent resistor from FB to GND that varies with VID input, the ramp on the \( V_{FB} \) can then be estimated as:

\[ V_{RAMP} = \frac{V_{IN} - V_{O}}{R4 \times C4} \times \frac{R1}{R4 \times R2 + R9} \]  

(7)

Usually R9 is set to 0Ω, then equation 7 can be simplified as:

\[ V_{RAMP} = \frac{(V_{IN} - V_{O}) \times \tau_{ON}}{R4 \times C4} \]  

(8)

The downward slope of the \( V_{FB} \) ripple then follows:

\[ V_{SLOPE1} = \frac{-V_{RAMP}}{t_{off}} = \frac{-V_{OUT}}{R4 \times C4} \]  

(9)

As shown in equation 8, if there is instability in PWM mode, we can reduce either R4 or C4. If C4 can not be reduced further due to limitations from equation 5, then we can only reduce R4. For a stable PWM operation, the \( V_{SLOPE1} \) should be designed as follows.

\[ -V_{slope1} \geq \frac{t_{SW} + t_{ON} \times R_{ESR} C_{OUT}}{2 \times L \times C_{OUT} \times V_{OUT} + \frac{10^{-3}}{t_{SW} - t_{on}}} \]  

(10)

Where \( I_{O} \) is the load current.

In skip mode, the downward slope of the \( V_{FB} \) ripple is almost the same with or without the external ramp. Figure 9 shows the simplified circuit of the skip mode when both HS-FET and LS-FET are off.

And R2 is the equivalent resistor from FB to GND that varies with VID input, the ramp on the \( V_{FB} \) can then be estimated as:

\[ V_{RAMP} = \frac{V_{IN} - V_{O}}{R4 \times C4} \times \frac{R1}{R4 \times R2 + R9} \]  

(7)

Usually R9 is set to 0Ω, then equation 7 can be simplified as:

\[ V_{RAMP} = \frac{(V_{IN} - V_{O}) \times \tau_{ON}}{R4 \times C4} \]  

(8)

The downward slope of the \( V_{FB} \) ripple then follows:

\[ V_{SLOPE1} = \frac{-V_{RAMP}}{t_{off}} = \frac{-V_{OUT}}{R4 \times C4} \]  

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As shown in equation 8, if there is instability in PWM mode, we can reduce either R4 or C4. If C4 can not be reduced further due to limitations from equation 5, then we can only reduce R4. For a stable PWM operation, the \( V_{SLOPE1} \) should be designed as follows.

\[ -V_{slope1} \geq \frac{t_{SW} + t_{ON} \times R_{ESR} C_{OUT}}{2 \times L \times C_{OUT} \times V_{OUT} + \frac{10^{-3}}{t_{SW} - t_{on}}} \]  

(10)

Where \( I_{O} \) is the load current.
Where \( R_O \) is the equivalent load resistor.

As described in Figure 6, \( V_{SLOPE2} \) in skip mode is smaller than \( V_{SLOPE1} \) in PWM mode, so the jitter in the skip mode is larger. For less jitter during ultra-light–load conditions, select smaller \( V_{FB} \) resistors, though at the cost of light-load efficiency.

**VID Input**

Typically, \( R1 \) and \( R2 \) set the output voltage with \( V_{FB}=0.6V \). \( R2 \), in this case, is a combination of \( R2A, R2B, \) and \( R2C \) depends on the VID, which is active low. The NB650/NB650H can dynamically track VID codes as they change. As a result, the converter output voltage can change without the need to reset either the controller or the value of \( R1 \) and \( R2A \). As shown in Figure 1, \( R2B \) and \( R2C \) are parallel with \( R2A \). The equivalent value of \( R2 \) can change due to different VID codes. One can get four \( V_{OUT} \) values depending on the VID codes with the details in the application information. The VID logic and equivalent \( R2s \) are shown in Table 1.

<table>
<thead>
<tr>
<th>VID2</th>
<th>VID1</th>
<th>( R2 )</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>1</td>
<td>( R2 = R_{2A} )</td>
</tr>
<tr>
<td>1</td>
<td>0</td>
<td>( R2 = R_{2A} // R_{2B} )</td>
</tr>
<tr>
<td>0</td>
<td>1</td>
<td>( R2 = R_{2A} // R_{2C} )</td>
</tr>
<tr>
<td>0</td>
<td>0</td>
<td>( R2 = R_{2A} // R_{2B} // R_{2C} )</td>
</tr>
</tbody>
</table>

**Enable Control**

The NB650/NB650H has a dedicated Enable control pin (EN). Pulling this pin high or low enables or disables the IC. Tie EN to \( V_{IN} \) through a resistor for automatic start-up.

**Soft Start/Stop**

The NB650/NB650H employs a soft-start/stop (SS) mechanism to ensure smooth output during power-up and power shutdown. When the EN pin goes high, an internal current source (10\( \mu \)A) charges up the SS capacitor. The SS capacitor voltage then acts as the \( V_{REF} \) voltage to the PWM comparator. The output voltage smoothly ramps up with the SS voltage. Once the SS voltage reaches the same level as the \( V_{REF} \) voltage, it continues ramping up while the \( V_{REF} \) voltage becomes the reference to the PWM comparator. At this point, the soft-start finishes and it enters steady-state operation.

When the EN pin goes low, a 10\( \mu \)A internal current source discharges the SS capacitor. Once the SS voltage reaches the \( V_{REF} \) voltage, acts as the reference to the PWM comparator.

The output voltage decreases smoothly with the SS voltage until it reaches zero level. Determine the SS capacitor as follows:

\[
C_{SS}(nF) = \frac{t_{SS}(ms) \times I_{SS}(\mu A)}{V_{REF}(V)}
\]  

(12)

If the output capacitors have large capacitance values, avoid setting a short SS time. Use a minimum value of 4.7nF if the output capacitance value exceeds 330\( \mu \)F.

**Power Good**

The NB650/NB650H has power-good (PG) output. The PG pin is the open drain of a MOSFET. Connect to \( V_{CC} \) or another voltage source through a resistor (e.g. 100k\( \Omega \)). The MOSFET turns ON after the application of the input voltage so that the PG pin is pulled to GND before the SS is ready. After the FB voltage reaches 90% of the reference voltage, the PG pin is pulled high after a delay.

The PG delay is determined as follows:

\[
t_{PG}(ms) = \frac{4 \times t_{SS}(ms)}{9}
\]

(13)

When the FB voltage drops to 90% of the reference voltage, the PG pin is pulled low.

**Over-Current Protection and Short-Circuit Protection**

The NB650/NB650H has cycle-by-cycle over-current limit control. The inductor current is monitored during the ON state. Once the inductor current hits the current limit, the HS-FET turns off. At the same time, the over-current protection (OCP) timer starts. The OCP timer is set as 50\( \mu \)s. If the current limit is hit for every cycle within that 50\( \mu \)s period, then OCP will trigger.

When the output is shorted to ground, the device hits its current limit and the FB voltage is less than 0.4V. The device treats this as a dead-short...
on the output and triggers OCP immediately. This is short circuit protection (SCP).

Under OCP/SCP condition, NB650 will latch off. The converter needs power cycle to restart. NB650H will try to recover from OCP/SCP fault with hiccup mode. That means in OCP/SCP protection, the NB650H will disable the output power stage, discharge soft-start capacitor and then automatically try to start again. If the overcurrent condition still holds after soft-start ends, the NB650H repeats this operation cycle till overcurrent fault is removed and output rises back to regulation level.

Over/Under-Voltage Protection
The NB650/NB650H monitors the output voltage through the FB voltage to detect overvoltage and under voltage on the output. When the FB voltage exceeds 0.8V, the over-voltage protection (OVP) triggers. Once OVP triggers, the LS-FET is always on while the HS-FET is always off. The device needs to power cycle to power up again. Under-voltage protection (UVP) triggers when the FB voltage is below 0.4V. Usually, UVP accompanies hitting the current limit, which results in SCP.

UVLO Protection
The NB650/NB650H has under-voltage lockout (UVLO) protection. When $V_{IN}$ exceeds the UVLO-rising threshold voltage, the NB650/NB650H powers up. It shuts off when $V_{IN}$ falls below the UVLO-falling threshold voltage. This is non-latch protection.

Thermal Shutdown
The NB650/NB650H employs thermal shutdown by internally monitoring the temperature of the junction. If the junction temperature exceeds the threshold value (typically 150°C), the converter shuts off. This is non-latch protection. There is about 25°C hysteresis. Once the junction temperature drops to around 125°C, it initiates a soft-start.
APPLICATION INFORMATION

Setting the Output Voltage-Large ESR Caps

A resistor divider from the output voltage to the FB pin sets the output voltage. Changing the VID codes for the NB650/NB650H accomplishes the same thing.

When there is no external ramp, the output voltages are set by feedback resistors R1 and R2A, R2B and R2C. First, choose R1 within 5kΩ-to-100kΩ to ensure stable operation. VOUT1, VOUT2, VOUT3 and VOUT4 are the voltages at different VID codes, arranged from low to high. Then determine R2A, R2B and R2C as follows:

\[
R2A = \frac{V_{REF}}{V_{OUT1} - \frac{1}{2} \Delta V_{OUT} - V_{REF}} \times R1
\]
\[
R2B = \frac{1}{V_{OUT2} - \frac{1}{2} \Delta V_{OUT2} - V_{REF}} \times \frac{1}{R1} - \frac{1}{R2A}
\]
\[
R2C = \frac{1}{V_{OUT3} - \frac{1}{2} \Delta V_{OUT3} - V_{REF}} \times \frac{1}{R1} - \frac{1}{R2A}
\]

VOUT4 can be calculated as:

\[
V_{OUT4} = \frac{V_{REF} \times (R1 + R2A // R2B // R2C)}{R2A // R2B // R2C} + \frac{1}{2} \Delta V_{OUT4}
\]

Where \( \Delta V_{OUTx} \) is the output ripple determined by equation 30.

Setting the Output Voltage-Small ESR Caps

Choose R1 within 5kΩ-to-100kΩ. The value of R2 then is determined as follows:

\[
R2A = \frac{V_{FB(AVG)}}{(\frac{1}{R1} + \frac{1}{R4 + R9})} \times (V_{OUT1} - V_{FB(AVG)})
\]
\[
R2B = \frac{1}{V_{OUT2} - V_{FB(AVG)}} \times \frac{1}{(\frac{1}{R1} + \frac{1}{R4 + R9})} - \frac{1}{R2A}
\]
\[
R2C = \frac{1}{V_{OUT3} - V_{FB(AVG)}} \times \frac{1}{(\frac{1}{R1} + \frac{1}{R4 + R9})} - \frac{1}{R2A}
\]

And VOUT4 also can be calculated with equation 17.

The \( V_{FB(AVG)} \) is the average value on FB. \( V_{FB(AVG)} \) varies with the \( V_{IN} \), \( V_{O} \), and load condition; its value in skip mode is lower than in PWM mode, which means the load regulation is strictly related to the \( V_{FB(AVG)} \). Also the line regulation is related to the \( V_{FB(AVG)} \); use a lower V RAMP that meets the conditions of equation 10 for better load or line regulation.

For PWM operation, estimate \( V_{FB(AVG)} \) from the following equation:

\[
V_{FB(AVG)} = V_{REF} + \frac{1}{2} V_{RAMP} \times \frac{R1 // R2}{R1 // R2 + R9}
\]

Usually, R9 is set to 0Ω, and it can also be set following equation 22 for better noise immunity. Set the value to \(<(1/5)\times R1 // R2\) to minimize its influence on \( V_{RAMP} \).

\[
R9 \leq \frac{1}{2 \pi \times C4 \times 2f_{SW}}
\]

Using equations 18 through 20 to calculate the output voltage can be complicated. Furthermore, as \( V_{RAMP} \) changes due to changes in \( V_{OUT} \) and \( V_{IN} \), \( V_{FB} \) also varies. To improve the output voltage accuracy and simplify the R2A, R2B and R2C calculations, add a DC-blocking capacitor (Cdc) to filter the DC influence from R4 and R9. Figure 11 shows a simplified circuit with external ramp compensation and a DC-blocking capacitor. The addition of this capacitor simplifies the R2A, R2B and R2C calculations, as per equations 23-25.
Select $C_{DC}>10\times C_4$ for better DC blocking, but select a value less than 0.47µF when considering start-up performance. For larger $C_{DC}$ values for better FB noise immunity, combine with reduced $R_1$ and $R_2$ to limit the $C_{DC}$ to a reasonable value without affecting system start-up. Note that even with $C_{DC}$, the load and line regulation are still related to $V_{RAMP}$.

\[
R_{2A} = \frac{V_{REF} + \frac{1}{2} V_{RAMP}}{\frac{1}{R_1} \times (V_{OUT1} - V_{REF} - \frac{1}{2} V_{RAMP})} \tag{23}
\]

\[
R_{2B} = \frac{1}{\frac{1}{R_1} \times (V_{OUT2} - V_{REF} - \frac{1}{2} V_{RAMP}) - \frac{1}{R_2A}} \tag{24}
\]

\[
R_{2C} = \frac{1}{\frac{1}{R_1} \times (V_{OUT3} - V_{REF} - \frac{1}{2} V_{RAMP}) - \frac{1}{R_2A}} \tag{25}
\]

The worst-case condition occurs at:

\[
I_{CIN} = \frac{I_{OUT}}{2} \tag{27}
\]

For simplification, choose an input capacitor whose RMS current rating is greater than half of the maximum load current.

The input capacitance value determines the input voltage ripple of the converter. If the system requires a specific input voltage ripple, choose the input capacitor that meets the specification.

\[
\Delta V_{IN} = \frac{I_{OUT}}{f_{SW} \times C_{IN}} \times \frac{V_{OUT}}{V_{IN}} \times (1 - \frac{V_{OUT}}{V_{IN}}) \tag{28}
\]

\[
\Delta V_{IN} = \frac{1}{4} \times \frac{I_{OUT}}{f_{SW} \times C_{IN}} \tag{29}
\]

Output Capacitor

The output capacitor maintains the DC output voltage. Use ceramic or POSCAP capacitors. The output voltage ripple can be estimated as:

\[
\Delta V_{OUT} = \frac{V_{OUT}}{f_{SW} \times L} \times (1 - \frac{V_{OUT}}{V_{IN}}) \times \left( R_{ESR} + \frac{1}{8 \times f_{SW} \times C_{OUT}} \right) \tag{30}
\]

Where $R_{ESR}$ is the equivalent series resistance (ESR) of the output capacitor.

For ceramic capacitors, the capacitance dominates the impedance at the switching frequency, and causes the majority of the output voltage ripple. For simplification, the output voltage ripple can be estimated as:

\[
\Delta V_{OUT} = \frac{V_{OUT}}{8 \times f_{SW} \times L \times C_{OUT}} \times (1 - \frac{V_{OUT}}{V_{IN}}) \tag{31}
\]

The output voltage ripple caused by ESR is very small, and therefore requires an external ramp to stabilize the system. The external ramp can be generated through resistor $R_4$ and capacitor $C_4$ following equations 5, 9 and 10.
ramp is not needed. A minimum ESR value of 12mΩ is required to ensure stable operation of the converter. For simplification, the output ripple can be approximated as:

\[ \Delta V_{\text{OUT}} = \frac{V_{\text{OUT}}}{f_{\text{SW}} \times L} \times (1 - \frac{V_{\text{OUT}}}{V_{\text{IN}}}) \times R_{\text{ESR}} \]  (32)

Inductor

The inductor supplies constant current to the output load while being driven by the switching input voltage. A larger value inductor results in less ripple current, which results in lower output ripple voltage. However, a larger value inductor is physically larger, has a higher series resistance, and/or lower saturation current. To determine the inductor value, allow the inductor peak-to-peak ripple current to reach approximately 30% to 40% of the maximum switch current limit. Make sure that the peak inductor current is below the maximum switch current limit. The inductance value can be calculated as:

\[ L = \frac{V_{\text{OUT}}}{f_{\text{SW}} \times \Delta I_L} \times (1 - \frac{V_{\text{OUT}}}{V_{\text{IN}}}) \]  (33)

Where \( \Delta I_L \) is the peak-to-peak inductor ripple current.

Choose an inductor that will not saturate under the maximum inductor peak current. The peak inductor current can be calculated as:

\[ I_{\text{LP}} = I_{\text{OUT}} + \frac{V_{\text{OUT}}}{2f_{\text{SW}} \times L} \times (1 - \frac{V_{\text{OUT}}}{V_{\text{IN}}}) \]  (34)
TYPICAL APPLICATION

Figure 12: Typical Application Circuit with No External Ramp
Vin = 12V, Vout = 1.05/1.15/1.20V, Iout = 6A, fsw = 550kHz

Figure 13: Typical Application with Low-ESR Ceramic Capacitor
Vin = 12V, Vout = 1.05/1.10/1.15/1.20V, Iout = 6A, fsw = 550kHz
Figure 14: Typical Application Circuit with Low-ESR Ceramic Capacitor and DC-Blocking Capacitor
$V_{IN} = 12V$, $V_{OUT} = 1.05/1.10/1.15/1.20V$, $I_{OUT} = 6A$, $f_{SW} = 550kHz$

Figure 15: Typical Application Circuit
$V_{IN} = 19V$, $V_{OUT} = 0.65/0.75/0.80/0.90V$, $I_{OUT} = 6A$
LAYOUT RECOMMENDATIONS

1. Place the high current paths (GND, IN, and SW) as close to the device as possible with direct, short, and wide traces.
2. Use a 0.1μF input decoupling capacitor to connect the IN and GND pins. Put the input decoupling capacitor and input capacitors as close to the IN and GND pins as possible.
3. Put the VCC decoupling capacitor as close to the VCC and GND pins as possible.
4. Keep the switching node SW short and away from the feedback network.
5. Place the external feedback resistors next to the FB pin. Make sure that there is no via on the FB trace.
6. Keep the BST voltage path (BST, C_{BST}, and SW) as short as possible.
7. Connect the bottom IN and SW pads to large copper areas to achieve better thermal performance.
8. Use a four-layer layout to achieve better thermal performance.
PACKAGE INFORMATION

QFN17 (3 x 4mm)

NOTE:
1) ALL DIMENSIONS ARE IN MILLIMETERS.
2) EXPOSED PAD SIZE DOES NOT INCLUDE MOLD FLASH.
3) LEAD COPLANARITY SHALL BE 0.10 MILLIMETER MAX.
4) JEDEC REFERENCE IS MO-220.
5) DRAWING IS NOT TO SCALE.

RECOMMENDED LAND PATTERN
Authorized Distributor

Click to View Pricing, Inventory, Delivery & Lifecycle Information:

Monolithic Power Systems (MPS):

NB650GL-Z  NB650GL-P